# **APPENDIX E**

# QRA KAPUNI GAS TREATMENT PLANT - WORLEY







**TODD ENERGY LTD** 

# Kapuni Gas Treatment Plant Quantitative Risk Assessment Report

610115-RPT-R0003 July 2022

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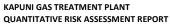
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# **EXECUTIVE SUMMARY**

#### Introduction

Worley New Zealand Limited (Worley) has been commissioned by Todd Energy (Todd) to perform a Quantitative Risk Assessment (QRA) for the Kapuni Gas Treatment Plant (KGTP).

#### Objectives

The main objective of this study is to develop risk contours to assess land use compatibility in accordance with the NSW Hazardous Industry Planning Advisory Paper No. 4 (HIPAP 4) "Risk Criteria for Land Use Planning".

#### Methods

The study uses an internationally accepted QRA approach that involves identification of hazards, assessment of the frequency of potential events, assessment of the consequences of potential events, risk computation and comparison of risk results with Todd's risk acceptance criteria and NSW HIPAP 4 individual fatality risk criteria. The risk computation is carried out using DNV risk modelling software package Safeti version 8.22.

The assessment considers risks from KGTP for the following cases:

- Base Case all facilities currently in operation;
- Sensitivity Case 1 all facilities currently in operation with reduced ESDV success rate of 98% instead
  of 100%; and
- Sensitivity Case 2 all facilities currently in operations including standby and mothballed facilities which might be brought back to operation in the future.

This QRA specifically evaluates onsite process/ flammable and toxic risks, but excludes risks from neighbouring facilities, non-flammable risks due to natural environmental hazards and occupational hazards.

#### Results

Risk contours for the Base Case are presented in Figure 1.







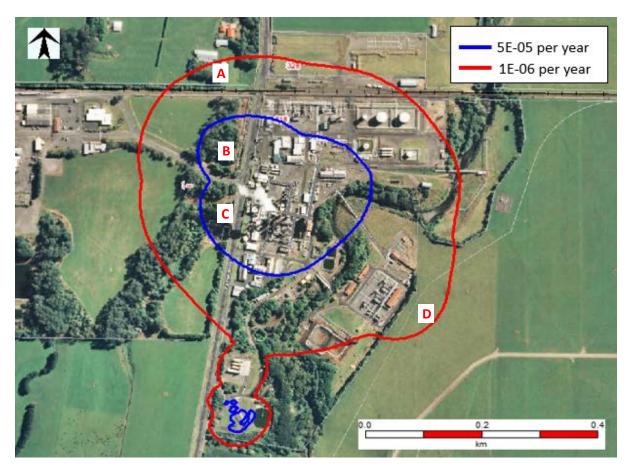


Figure 1: Base Case LSIR Contours at KGTP

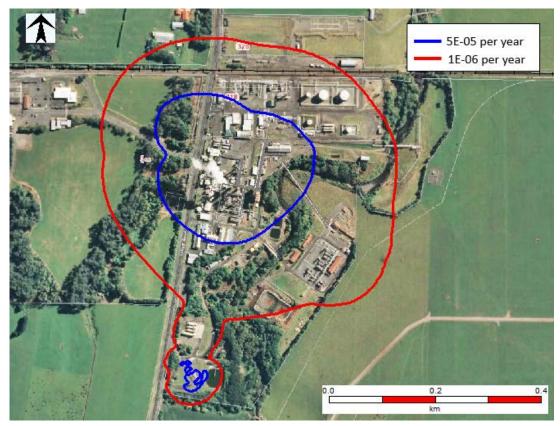
The following conclusions have been made for the Base Case assessment:

- The 5E-05 per year contour extends into the KPS site to the north but remains within the Todd Energy site boundary;
- The 5E-05 per year contour extends across Palmer Road and into the bushes at the west boundary of the Ballance site;
- The 1E-06 per year contour extends onto the property of the neighbour to the northwest (approximately 180m NW of KGTP northern boundary) but does not extend as far as the dwelling and farm buildings;
- The main risk contributors to the shed area (location A) are ammonia toxic events from 71 mm leaks from the Liquid Receivers (KGT80\_AMM\_04\_L\_71mm) and Ammonia Condensers (KGT80\_AMM\_03\_L\_71mm) within the CO2 Recovery Unit (at approximately 15°C and 15 barg); and
- The main risk contributors to the Ballance site bushes (locations B and C) are ammonia toxic events from 22 mm leaks from the Liquid Receivers (KGT80\_AMM\_04\_L\_22mm) and Ammonia Condensers (KGT80\_AMM\_03\_L\_22mm) within the CO2 Recovery Unit (at approximately 15°C and 15 barg).
- The main risk contributors to the rural land area to the east of the plant (location D) are Product Gas jet fire events from 85 mm leaks from the Gas Storage Compressor (D4-0401) to Coalescer (KGT13\_PGS\_16\_V\_85mm), and the Gas Storage Compressor (KGT13\_PGS\_15\_V\_85mm) within the Product Gas Lines and Compressors unit (at approximately 15°C and 40 barg).





Risk contours for the Sensitivity Case 1 are presented in Figure 2.



#### Figure 2: Sensitivity Case 1 LSIR Contours at KGTP

The 5E-05 per year and 1E-06 per year risk contours for Sensitivity Case 1 are similar to the Base Case risk contours. The assessment conclusions made against HIPAP 4 for Base Case are applicable to Sensitivity Case 1 as well. This is mainly due to:

- The ESDV failure probability change is only 2%, therefore the frequencies of hazardous events (fire explosion or toxic) associated with increased consequence distances (if any, from the additional inventory due to isolation failure cases) are not expected to be apparent in the risk contours; and
- In most modelling cases, especially gas releases, it is expected that the consequence effects would have reached the steady state condition before the inventory depletes. Hence the additional inventory may lead to a prolonged fire event, but not increase the magnitude of the consequence.





Risk contours for the Sensitivity Case 2 are presented in Figure 3.

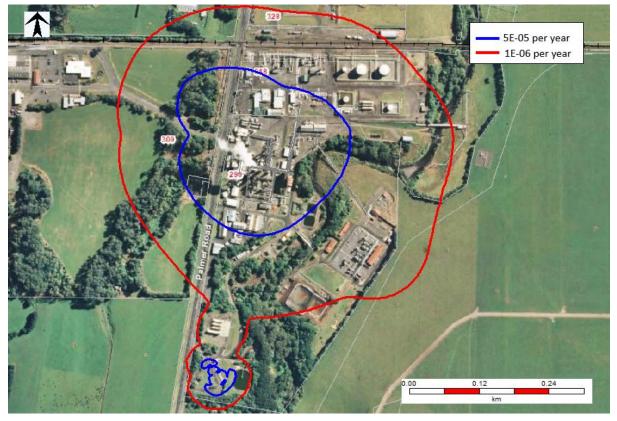


Figure 3: Sensitivity Case 2 LSIR Contours at KGTP

The risk contours of 5E-05 per year and 1E-06 per year for Sensitivity Case 2 are slightly larger, when compared to Base Case. This is particularly apparent at the LPG/NGL loading area at the southern edge of the KGTP site, which is due to the increased in loading frequencies for both the NGL and LPG loading scenarios. The increase in 5E-05 per year and 1E-06 per year contours do not change the assessment conclusions made against HIPAP 4 for Base Case are applicable to Sensitivity Case 2 as well.

Although there is additional equipment and inventories considered in Sensitivity Case 2, the increase in risk levels are not significant. This is most likely due to:

- The additional nodes/sections considered in Sensitivity Case 2 only formed a small part of the overall KGTP hazardous nodes/sections. There is approximately 18 % increase in total release frequency for Sensitivity Case 2 as compared to the Base Case, with 50% of the increase being from the "1-3 mm" leak category; and
- In most modelling cases, especially gas releases, it is expected that the consequence effects would have reached the steady state condition before the inventory depletes. Hence the additional inventory due to the higher throughput in Sensitivity Case 2 may lead to a prolonged fire event, but not increase the magnitude of the consequence.





# **1** ABBREVIATIONS

API	American Petroleum Institute
BLEVE	Boiling Liquid Expanding Vapour Explosion
CO <sub>2</sub>	Carbon Dioxide
DNV	Det Norske Veritas
DTL	Dangerous Toxic Load
ESDV	Emergency Shutdown Valve
FBR	Full Bore Rupture
FGL	First Gas Limited
GCPS	Global Congress on Process Safety
HCRD	Hydrocarbon Release Database
HIPAP4	NSW Hazardous Industry Planning Advisory Paper No. 4
НМВ	Heat and Material Balance
IOGP	International Association of Oil and Gas Producers
IRPA	Individual Risk Per Annum
KGTP	Kapuni Gas Treatment Plant
KPS	Kapuni Production Station
LFL	Lower Flammable Limit
LPG	Liquefied Petroleum Gas
LSIR	Location Specific Individual Risk
MEM	Multi-Energy Method
NGL	Natural Gasoline
NH <sub>3</sub>	Ammonia
NIWA	National Institute of Water and Atmospheric Research Ltd
NZ	New Zealand
P&ID	Piping & Instrumentation Diagram
PFD	Probability of Failure on Demand
PHAST	Process Hazard Analysis Software Tool
SDV	Shutdown Valve
SLOT	Specified Level of Toxicity
SLOD	Significant Likelihood of Death
QRA	Quantitative Risk Assessment
RADD	Risk Assessment Database Directory
STDC	South Taranaki District Council
Todd	Todd Energy





VCE	Vapour Cloud Explosion
Worley	Worley New Zealand Limited





# 2 INTRODUCTION

# 2.1 Background

A Quantitative Risk Assessment (QRA) was completed by Worley New Zealand Limited (Worley) for Kapuni Gas Treatment Plant (KGTP) in 2020 as requested by Todd Energy (Todd).

An Assumptions Register has been prepared and agreed with Todd [Ref. 1] prior to commencing the QRA to ensure all modelling inputs used represent the current processes and operating conditions of KGTP and assumptions made are reasonable.

This report presents the QRA methodology, modelling inputs, assumptions and risk results.

# 2.2 Objectives

The main objective of the study is to develop risk contours to assess land use compatibility in accordance with the NSW Hazardous Industry Planning Advisory Paper No. 4 (HIPAP 4) "Risk Criteria for Land Use Planning" [Ref. 8].

# 2.3 Scope

Facilities considered in the QRA include:

- CO<sub>2</sub> Removal Unit (Benfield);
- Dehydration and Dew Point Control Unit;
- Propane Refrigeration System;
- Liquefied Petroleum Gas (LPG) Production Unit;
- Storage tanks for LPG & Loadout Facility;
- Storage tank for Natural Gasoline (NGL) & Loadout Facility;
- Product Lines and Compressors;
- Cogeneration Area;
- Utilities;
- CO<sub>2</sub> Recovery Unit; and
- CO<sub>2</sub> Storage tanks & Loadout Facility.

#### 2.4 Exclusions

The following facilities and scope of work are excluded from the QRA:

- Utilities such as instrument air and utility water as they do not contain any hydrocarbon inventory;
- The flare and blowdown;
- The impact from Ballance Agri-Nutrients and Kapuni Production Station (KPS) to KGTP. The cumulative risk considering both KGTP and KPS is discussed briefly in Section 9;
- Risk other than hydrocarbon/ process (e.g. transportation/ seismic/ volcanic risks);
- Societal Risk (F-N Curve); and
- Occupied building risk assessment.





# 2.5 QRA Study Cases

QUANTITATIVE RISK ASSESSMENT REPORT

The QRA study includes base case and sensitivity cases assessment to study the impact of certain assumptions and/or plant operating capacity on the risk results. The QRA Base Case includes the assessment of current KGTP operation with a set of agreed modelling assumptions detailed in Section 4.2.

The two sensitivity cases considered in the KGTP QRA are:

- Sensitivity Case 1: 98% ESDV Success Probability; and
- Sensitivity Case 2: Future Operations.

The details of Base Case, Sensitive Case 1 and Sensitivity Case 2 are summarised in Table 2-1.

QRA Case	Details	Potential Impact
Base Case	<ul> <li>Current plant operation with 2 Benfield nominal throughput (12 Sm<sup>3</sup>/s), includes all Operating units summarised in Table 3-2</li> <li>Assumed ESDV system has 100% isolation success probability</li> </ul>	-
Sensitivity Case 1 (98% ESDV Success Probability)	<ul> <li>Current plant operation with 2 Benfield nominal throughput (12 Sm<sup>3</sup>/s), includes all Operating units summarised in Table 3-2</li> <li>Assumed ESDV system has 98% success probability</li> </ul>	• Increased release inventories during ESDV failure, i.e. 2% of the time. The volume for each isolatable section is added with the next biggest connecting isolation inventory
Sensitivity Case 2 (Future Operation)	<ul> <li>Maximum throughput operation (29 Sm<sup>3</sup>/s) for future operation after the Kapuni development project, includes all Operating, Mothballed and Standby units summarised in Table 3-2</li> <li>Assumed ESDV system has 100% isolation success probability (noting that the 100% and 98% scenarios give very similar results)</li> </ul>	<ul> <li>Additional equipment considered in the QRA model</li> <li>Increased in inventory for each isolatable section due to increase in throughput</li> <li>Increased in total leak frequency</li> </ul>

Table 2-1: KGTP QRA Base Case, Sensitivity Case 1, Sensitivity Case 2 Comparison





# 3 FACILITY AND PROCESS OVERVIEW

# 3.1 Facility Overview

QUANTITATIVE RISK ASSESSMENT REPORT

Kapuni is an onshore gas and condensate field located in South Taranaki, approximately 50 km south of New Plymouth and 14 km northwest of Hawera. Throughout the Kapuni gas field, there are feeder well-sites which deliver raw Kapuni gas to Kapuni Production Station (KPS) and KGTP. The well sites, KPS and KGTP are owned and operated by Todd. Todd recover hydrocarbon condensate from the raw gas at KPS. The remaining raw gas is delivered via pipeline from KPS to KGTP.

KGTP is located directly to the south of KPS, with a fence separating the two facilities. Ballance Agri-Nutrients plant is located to the west of the KGTP. The locations of these sites land area are shown in Figure 3-1:



Figure 3-1: Map Showing Locations of KPS, KGTP and Ballance Sites

Raw Kapuni gas has a very low heating value due to it containing about 40-46 mol% Carbon Dioxide (CO<sub>2</sub>). Consequently, this gas needs to be treated at KGTP so that the natural gas meets the New Zealand (NZ) specification for reticulated natural gas and can, therefore, go into the NZ open access gas transmission network owned by First Gas Limited (FGL).

Overview site plans of KGTP are shown in Figure 3-2 to Figure 3-4, and Table 3-1 shows the description of each area.

Area	Description			
1	CO₂ Removal			
2	Dehydration and Dewpoint Control			
3	Refrigeration			
4 LPG Production				
5 Product Lines and Compressors (West)				
6	Product Lines and Compressors (East)			

#### Table 3-1: KGTP Area Description





Area	Description			
7	LPG Storage			
8	LPG Loadout			
9	Product Gas Storage Compressors (East)			
10	Flare (East)			
11	Flare (West)			
12	Steam Boilers			
13	CO <sub>2</sub> Recovery			
14	Alkali Storage			
15	LTS Road Bridge			
16	LTS Pipe Bridge			
17	Methanol Storage			





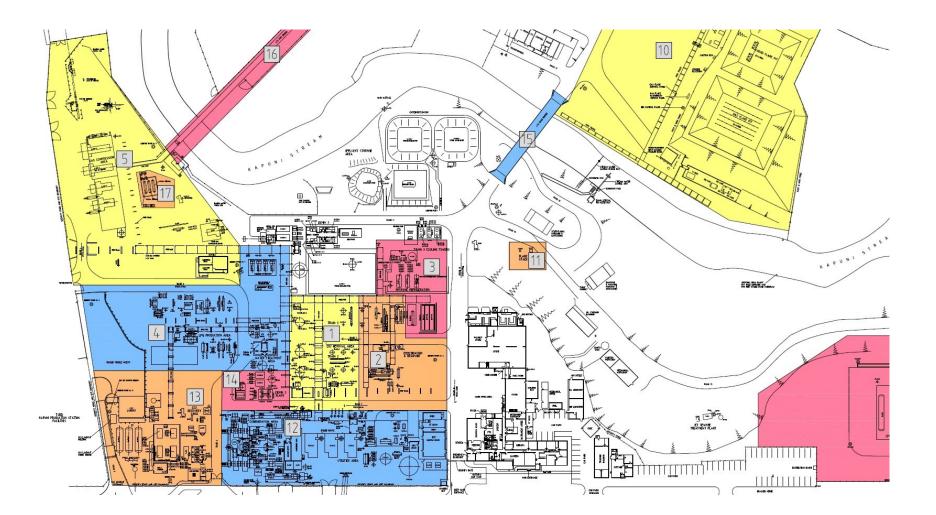


Figure 3-2: Kapuni Gas Treatment Plant Plot Plan (Main Process Area)





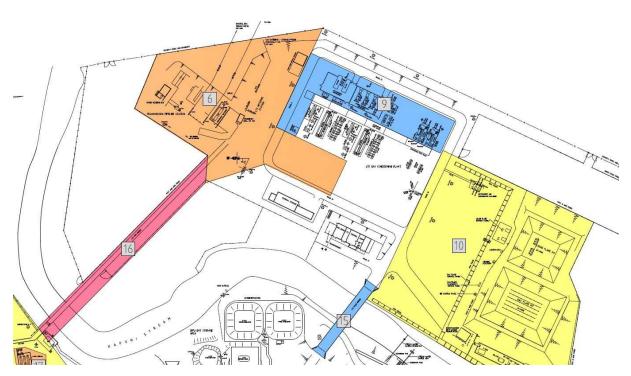


Figure 3-3: Kapuni Gas Treatment Plant Plot Plan (Product Gas Compression Unit and Flare Pits)

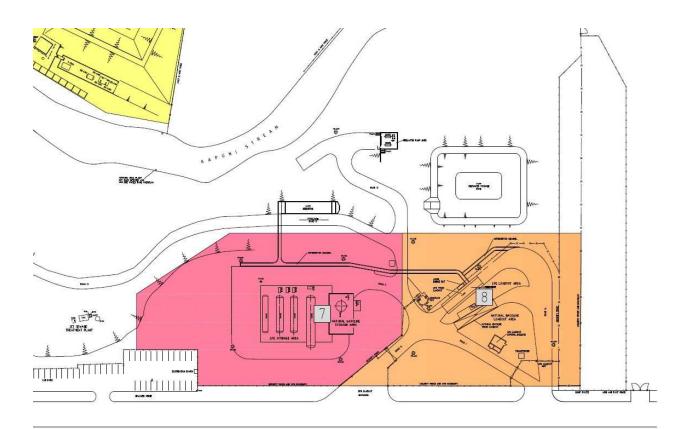


Figure 3-4: Kapuni Gas Treatment Plant Plot Plan (LPG Storage and Loadout Area)





# 3.2 Process Overview

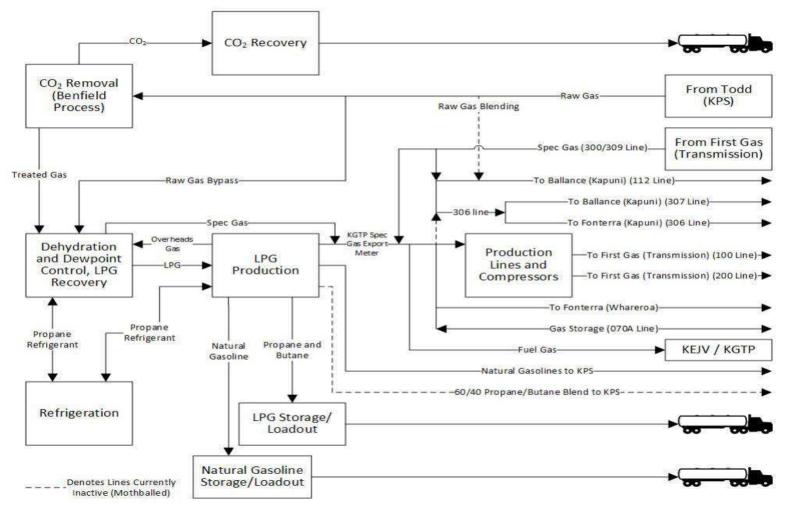
The generalised gas treatment process in KGTP involves the following steps:

- a) Removal of the bulk of the CO<sub>2</sub> via a recirculating Benfield hot potassium carbonate process so that the gas meets the acceptable specifications for energy content.
- b) Removal of water by contact with methanol and then chilling using propane refrigerant to meet the water content and hydrocarbon dewpoint specifications.
- c) Removal of a large proportion of the heavier hydrocarbon components in the above chilling stage, followed by separation to produce Liquefied Petroleum Gas (LPG) and Natural Gasoline (NGL) for export/sale.
- d) Compression and metering of treated spec gas to transfer into the transmission network. Note that the Product Gas Compressor system is a First Gas asset but can be controlled from KGTP.
- e) CO<sub>2</sub> collected from Benfield Process is processed into liquid CO<sub>2</sub>, using an ammonia refrigeration system and transferred to storage tanks for export/sale.

The KGTP process overview is shown in Figure 3-5.













# 3.3 Plant and/or Equipment Operational Status

Not all plant and equipment in the KGTP site are currently in operation. The four plant and equipment status categories defined by Todd are as follow:

- Operating: All plant and / or equipment that are currently in operation to achieve an outcome for the business.
- Standby: All plant and / or equipment that are ready to start when the operating plant and / or equipment unit stops.
- Mothballed: All plant and / or equipment that are unlikely to be used for achieving any business outcome in the near future. They are positively isolated from all upstream and downstream process systems. Blinds, spades or spacers are installed at all the points of disconnection from live process systems. All systems are electrically isolated and earthed. The plant and / or equipment is preserved to maintain it in a satisfactory condition.
- Abandoned: All plant and / or equipment that are unlikely to be used for achieving any business
  outcome in the foreseeable future. They are positively isolated and physically disconnected from all
  upstream and downstream process systems with a visible air gap present to prove positive isolation
  but maintain physical position on site. Blinds are installed at all the points of disconnection from live
  process systems. All systems are electrically isolated / disconnected as appropriate. Plant or
  equipment is not maintained or preserved.

The operational status of process plants / units in KGTP are summarised in Table 3-2.

Plant/U	nit	Operational Status	Considered in QRA?	
CO <sub>2</sub> Removal Unit	Train 1, 2	Operating	Yes	
(Benfield)	Train 3	Mothballed Note1	Yes (Sensitivity case 2) Note 1	
Dehydration and Dew Point	No. 2 Chilling System	Operating	Yes	
Control Unit	No. 1 Chilling System	Standby Note2	Yes (Sensitivity case 2) Note 2	
Propane Refrigeration System	ı	Operating	Yes	
LPG Production Unit	Train 1	Standby Note2	Yes (Sensitivity case 2) Note 2	
LPG Production Unit	Train 2	Operating	Yes	
LPG Storage & Loadout Facilit	τy	Operating	Yes	
• 60/40 Condensing	Tank	Mothballed Note 6	Yes (Sensitivity case 2) Note 6	
Natural Gasoline Storage & Lo	oadout Facility	Operating	Yes	
Product Lines and Compresso	ors	Operating	Yes	
<ul> <li>Stab Gas Compress</li> <li>CNG Compressor</li> <li>No.4 Product Gas C</li> </ul>		Abandoned Note 3	No	
Gas Gathering Facility		Operating	Yes	
Cogeneration Area		Operating	Yes	
CO <sub>2</sub> Recovery Unit		Operating	Yes	
Utilities		Operating	Yes	

Table 3-2 : KGTP Plants/Units Operational Status





Plant/Unit	Operational Status	Considered in QRA?
<ul> <li>Boilers (B-901-1/2/3)</li> <li>De-aerator (E-901-1)</li> </ul>	Mothballed Note 4	Yes (Sensitivity case 2) Note 4
Demin Plants 1&2	Abandoned Note 3	No
LTS Conditioning Unit	Abandoned Note 5	No Note5

Notes:

- 1. Benfield train 3 is mothballed and considered in QRA as Sensitivity case 2.
- 2. One out of two trains of the Dehydration and Dew Point Control Unit and the LPG Production Unit are currently on standby and considered in QRA as Sensitivity case 2.
- 3. Equipment is abandoned and will never be recommissioned, therefore not considered in QRA.
- 4. Boilers and de-aerator are mothballed, and the fuel gas lines are blinded off. One boiler is not in the condition that could be easily restarted but two can be brought back online fairly easy. Therefore, only two boilers are considered in QRA as Sensitivity case 2.
- 5. The LTS gas conditioning unit is in an abandoned condition which would require significant remedial work prior to recommissioning, therefore not considered in the study. However, a few live product gas lines and Gas Storage Compressors (D4-0401/0402) in this area, are considered in QRA.
- 6. 60/40 LPG line is mothballed and is considered in QRA as Sensitivity Case 2.

The QRA study considers current KGTP operation as Base Case. Risk levels considering equipment to be use for future production are considered in the Sensitivity Case 2 assessment.





# 4 STUDY METHODOLOGY AND ASSUMPTIONS

The methodology followed for completing the QRA is aligned with good industry practice and the Todd Energy Fire and Explosion Analysis and Quantitative Risk Assessment Methodology Guideline [Ref. 2]. The generic process, specified in the Worley's Onshore QRA Method Statement [Ref. 3], is illustrated in Figure 4-1 with the minor modification in that this study does not include the provision of risk mitigation measure recommendations.

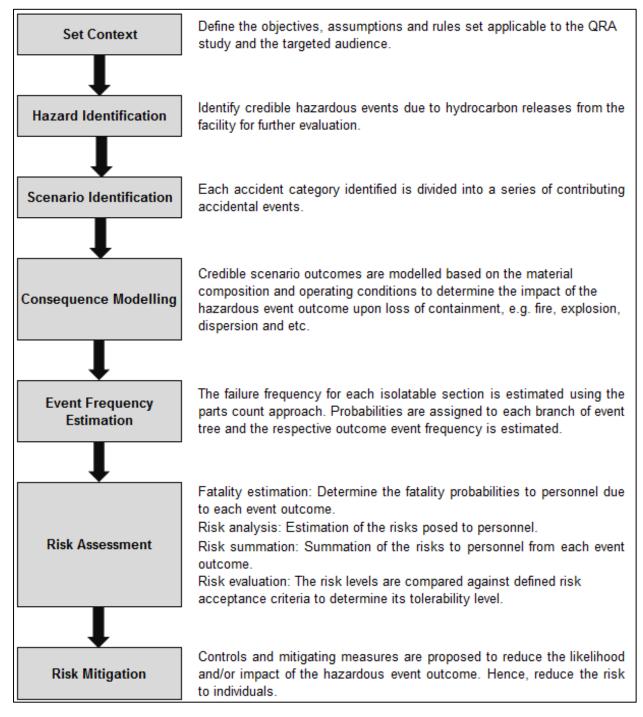


Figure 4-1: QRA Methodology





# 4.1 Assessment Tool

DNV Safeti Software version 8.22 [Ref. 6] is used to build the QRA model. Safeti is an integrated consequence and risk modelling package developed by DNV Software aimed at the onshore petrochemical and chemical process industry for assessing process plant risks via comprehensive QRA. It is designed to perform all the analytical, data processing and results presentation elements of a QRA within a structured framework.

# 4.2 QRA Assumptions

An Assumptions Register [Ref. 1] was generated which outlines the basis of all assumptions and the input bases inherent in the QRA study. Key assumptions are shown in the following subsections for reference.

# 4.2.1 Atmospheric Conditions

Meteorological conditions impact the outcomes of release modelling, including downwind flammable and toxic vapour cloud dispersion distance (influenced by atmospheric stability and wind speed), rate of pool vaporisation (ambient temperature), and atmospheric attenuation of radiant heat (temperature and relative humidity).

The following conditions are used as basis in the QRA modelling.

#### Wind Speed and Direction

Wind speed and direction data are taken from NIWA's CliFlo database [Ref. 19] for the Hawera Automatic Weather Station to represent the atmospheric conditions at KGTP. Data for 5-year period from January 2008 to December 2012 are taken, with wind speed and direction measurements taken every hour. The wind rose is shown in Figure 4-2.

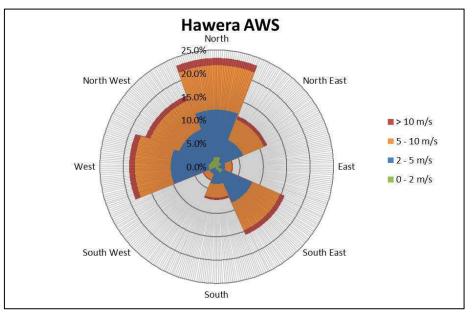


Figure 4-2: Hawera AWS Windrose

The following combinations of wind speed and atmospheric stability is used in the QRA model to represent the typical wind speed conditions around the plant area:

- 2/F wind speed of 2 m/s with Pasquill Stability class F stable, night with moderate clouds and light/moderate wind
- 5/D wind speed of 5 m/s with Pasquill Stability class D neutral, little sun and high wind or overcast/windy night





 10/D – wind speed of 10 m/s with Pasquill Stability class D – neutral, little sun and high wind or overcast/windy night

For the modelling, wind speed reference height (the height at which the wind impacts a release) is set at 1 m (i.e. so as to match the release height). The Power Law wind profile is applied, where the wind speed varies with height according to power-law profile.

By consideration of the Pasquill Stability class relationship with day and night and wind speeds, the wind data for use in the QRA model is calculated as shown in Table 4-1.

Wind Speed / Pasquill Stability	North	North East	East	South East	South	South West	West	North West	Total
0 - 2 m/s / F	2.1%	1.1%	0.3%	1.4%	0.6%	0.3%	1.7%	1.5%	9.0%
2 - 5 m/s / D	10.1%	5.1%	1.5%	6.9%	3.1%	1.4%	8.2%	7.2%	43.5%
5 - 10 m/s / D	11.1%	5.6%	1.7%	7.5%	3.4%	1.5%	8.9%	7.9%	47.5%
Total	23.3%	11.8%	3.5%	15.9%	7.1%	3.2%	18.7%	16.5%	100.0%

Table 4-1: Hawera AWS Wind Data

#### Ambient Temperature and Relative Humidity

The following ambient temperature and relative humidity are used in the QRA:

- Ambient temperature: 14°C
- Relative humidity: 83%

#### Solar Radiation

The allowance for solar radiation has been excluded from the calculations.

#### Topography

Safeti cannot take into account the effects of the local undulating topography for the gas dispersion. The surface roughness of 0.1 m is applied to represent an area of "low crops, occasional large obstacles".

#### 4.2.2 General Leak Frequency

The leak frequencies for process equipment in general are taken from the International Association of Oil and Gas Producers (IOGP) Risk Assessment Data Directory (RADD) Process Release Frequency [Ref. 12]. Where IOGP data does not cover such as storage vessels, TNO Purple book failure data [Ref. 10] was used. The details are provided in the Assumptions Register [Ref. 1].

#### 4.2.3 Release Hole Sizes

For every component failure, there is a range of credible hole sizes ranging from pinhole leak to full bore rupture. In general, the representative hole sizes used in the QRA is as shown in Table 4-2.

Selected representative holes sizes were chosen using the geometric mean of the smallest and largest hole size in each group. For example, the representative hole size for the range 10 - 50 mm is calculated as  $(10 \times 50)0.5 = 22$  mm. The use of geometric mean is also aligned with the recommendation in the latest OGP Process Release Frequency [Ref. 12].



QUANTITATIVE RISK ASSESSMENT REPORT



#### Table 4-2: Hole Size Distribution

OGP Hole Size Group (mm)	Representative Hole Size (mm)
1 - 3	2
3 - 10	6
10 - 50	22
50 - 150	85
> 150	Range geometric mean

22 mm is used as the maximum hole size for small bore fittings. The maximum hole size for a flange is also limited to 22 mm as a release from a flange is normally limited to a segment of a gasket between bolts [Ref. 2].

It is noted for equipment referencing TNO Purple Book [Ref. 10] failure data, actual hole sizes following the failure data is used as there are no sufficient leak size distribution data in Purple Book to calculate the geometric mean.

# 4.2.4 Leak Frequency Modification Factor

Several leak frequency modification factors are applied to the release frequency database as per the Assumption Register [Ref. 1] and Todd Energy's Methodology Guideline [Ref. 2].

Type of Re	Reduction in frequencies	
Piping Release Frequency	Process Piping	-
	Inter-unit Piping	90%
Rupture Release Frequency	ture Release Frequency Full bore rupture	

Table 4-3: Leak Frequency Modification Factor

For KGTP, process (on skid) piping are considered for pipework which connect equipment within the unit boundary while inter-unit piping is considered for piping which connects different units within the KGTP site.

# 4.2.5 Isolation Success Probability

The Emergency Shutdown (ESD) systems are intended to shut down and isolate the process inventories to reduce damage or risk of escalation. When activated, emergency shutdown valves (ESDVs) divide the process system into a number of isolatable sections, with each potential leak source associated with a particular isolatable inventory.

In this KGTP QRA, 100% ESDV success probability is assumed for the Base Case inventory consideration.

# 4.2.6 Ignition Probabilities

For KGTP QRA, the Energy Institute (EI) ignition probability model referenced in OGP Ignition Probabilities [Ref. 14] is used for the estimation of overall ignition probability of loss of containment scenarios.

For this QRA, the following ignition scenarios are used [Ref. 14]:

 Scenario 8 – Large Plant Gas LPG (Gas of LPG release from large onshore plant) – Releases of flammable gases, vapour or liquids significantly above their normal (NAP) boiling point from large onshore outdoor plants (plant area above 1200 m<sup>2</sup>, site area above 35,000 m<sup>2</sup>).





- Scenario 9 Large Plant Liquid (Liquid release from large onshore plant) Releases of flammable liquids that do not have any significant flash fraction (10% or less) if released from large onshore outdoor plants (plant area above 1200 m<sup>2</sup>, site area above 35,000 m<sup>2</sup>) and which are not bunded or otherwise contained.
- Scenario 13 Tank Liquid 100 m x 100 m Bund (Liquid release from onshore tank farm where spill is limited by small or medium sized bund) Releases of flammable liquids that do not have any significant flash fraction (10% or less) if released from onshore outdoor storage area 'tank farm' (e.g. spill in a large tank bund containing four or fewer tanks, or any other bund less than 25,000 m<sup>2</sup> area).

The graphs of ignition probabilities as a function of mass release rate are shown in Figure 4-3.

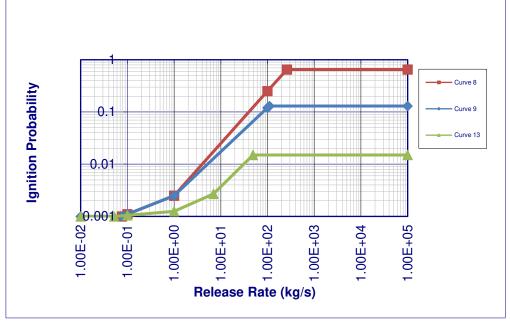


Figure 4-3 Ignition Probability

# **Early and Delayed Ignition Probabilities**

The graph presented in Figure 4-3 represents the total ignition probability. An overall distribution for early to delayed ignition ratio of 30:70 to 50:50 split is considered reasonable. The timing of ignition is used as a means to predict the nature of the ignited event. Early ignition is taken to indicate a jet fire or pool fire depending on the material released. Delayed ignition is taken to indicate that the ignition would initially result in a flash fire or explosion.

For this study, a 30:70 split for early to delayed ignition probability is used. Given the maturity of the hazardous area and ignition control measures in place on KGTP site, it can be assumed that 70% of releases will not find an ignition source in the immediate area of the release and therefore will have a delayed ignition.

#### **Explosion Probabilities**

For this QRA, the generic explosion probabilities shown in Table 4-4 is used [Ref. 15].

Release Rate Category	Release Rate (kg/s)	Explosion Probability given ignition
Minor	<1 (0.5 nominal)	0.04
Major	1-50	0.12
Massive	>50 (100 nominal)	0.3





# 4.2.7 Congested Areas

Flammable vapour cloud accumulation at congested area(s) is a prerequisite to initiate a Vapour Cloud Explosion (VCE).

KGTP is generally open with good ventilation expected throughout the year. However, some areas around the process plants can be quite congested due to the size and arrangement of process equipment/vessels/piping. These areas are identified as congested areas and shown in Figure 4-4.

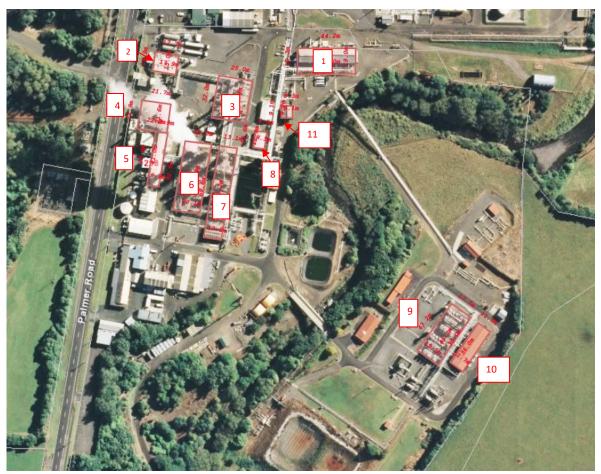


Figure 4-4: KGTP Congested Area

The estimated volume of each congested area is given in Table 4-5.

The VCE impacts are estimated using "Multi Energy Model" in Phast/Safeti, where the explosion overpressure is modelled based on blast strength of each congested area. The blast strength class assumed for each congested area is summarised in Table 4-5. Details and basis of the "Multi Energy Model" congested area parameters are provided in Assumptions Register [Ref. 1].

No.	Description	Volume (m <sup>3</sup> )	Blast Strength Class
Congested Area 1	Gas Compression Area Compressor Shed	5,852	5
Congested Area 2	CO <sub>2</sub> Recovery Area Compressor Shed	1,350	5
Congested Area 3	LPG Production Process Area	2,400	5
Congested Area 4	Cogeneration Process Area	2,904	5

Table 4-5: Volume and Blast Strength	Index of the Congested Areas
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No.	Description	Volume (m <sup>3</sup> )	Blast Strength Class
Congested Area 5	Boiler House	3,321	5
Congested Area 6	Gas Treatment Process Area 1	3,180	5
Congested Area 7	Gas Treatment Process Area 2	2,691	5
Congested Area 8	OVHD Compressor Shed	585	5
Congested Area 9	LTS Conditioning Process Area	2,451	3
Congested Area 10	LTS Gas Conditioning Compressor House	2,592	5
Congested Area 11	Stab Gas Compressor Shed	432	5

It is noted that VCE is performed with a "black box" calculations in the Safeti model. Safeti estimates explosion risk based on percentage fill of the identified congested areas, taking into account of the flammable gas cloud dispersion from all release scenarios within KGTP. The software however does not report the eventual percentage filled in each identified congested area used for the explosion fatality risk modelling.

# 4.2.8 Fatality Criteria

# **Heat Radiation**

The method of calculating the probability of fatality for an individual, given known exposure duration and thermal heat radiation levels, is undertaken by using a Probit function. The Probit function is a general formula which takes the same form, but with various constants used. The Probit used for lethality calculations is taken from the TNO Green Book [Ref. 11]. The Probit function is defined as follows:

Probit = 
$$-36.38 + 2.56 \ln (t \times q^{4/3})$$

Where:

t = exposure duration in seconds

q = thermal radiation level in W/m<sup>2</sup>

Safeti calculates the Probit values during the analysis.

An exposure duration of 20 seconds is used as a base case, although it is noted that personnel are likely to find some form of shielding protection within this time frame.

# Flash Fire

If personnel are within the 100% lower flammable limit (LFL) of the gas plume, 100% fatality is assumed. LFL is the lower end of the concentration range over which the flammable mixture of a gas/ vapour in air can be ignited at a given temperature/ pressure.

A flash fire occurs when a dispersed cloud of flammable gas or vapour and air mixture is ignited within its flammable regions, causing a wall of flame to spread throughout the flammable region and back to the release point. The flame propagates through the cloud in a manner such that negligible or no damaging overpressure is generated. This flash is almost instantaneous as the flame propagates at high speed through the cloud and back to the source.

An assumption of 100% fatality rate within the footprint of the cloud is conservative and does not allow for potential risk reducing considerations such as;

- uneven mixing of gas and air in the cloud resulting in uneven propagation of the flame;
- topography;
- sparsely populated rural land use adjoining the site;





- KAPUNI GAS TREATMENT PLANT QUANTITATIVE RISK ASSESSMENT REPORT
  - availability of shelter;
  - opportunity for escape; and
  - clothing worn by persons exposed to the flash fire.

Thermal radiation outside of the flash fire falls off rapidly and is not sustained due to the instantaneous nature of the event. The potential for fatality outside the flash fire footprint is not considered credible.

# Explosion Overpressure

The "Multi-Energy Explosion" model is used to model the congested area Vapour Cloud Explosion (VCE). The assessment criteria for explosion overpressure effects are based on the explosion effects taken from the HIPAP4 [Ref. 8] as given in Table 4-6.

Explosion Overpressure (kPa)	Effects		
3.5	No fatality and very low probability of injury		
7	Probability of injury is 10%. No fatality		
21	20% chance of fatality to a person in a building		
35	50% chance of fatality for a person in a building and <b>15% chance of fatality for a person in the open</b>		
70	Threshold of lung damage 100% chance of fatality for a person in a building or in the open		

#### Table 4-6: Effects of Explosion Overpressure

Note: The two overpressure levels in bold are considered in the QRA as the fatality probabilities for personnel in the open.

# BLEVE

Boiling Liquid Expanding Vapour Explosion (BLEVE) is an escalation scenario that occurs as a result of prolonged flame impingement on above ground pressurised vessels containing materials such as liquefied petroleum gas (LPG) or lighter end hydrocarbon. BLEVE would result in an explosion overpressure together with a fireball and missile generation over some distance. As the fireball tends to drift upward and to avoid double counting, only the explosion overpressure effects are considered in the QRA. The fatality criteria for BLEVE explosion are referenced from Table 4-6 above.

For KGTP study, BLEVE is considered credible if a pressurised vessel contains at least 4 m3 of volatile hydrocarbon (liquid butane or lighter). The BLEVE scenarios considered in the KGTP QRA study are shown in Table 4-7. These vessels are above ground vessels and no credit is taken for the available firefighting provisions (e.g. deluge).

Table 4-7: Vessels Considered	for BLEVE in KGTP
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Equipment Tag no.	Description	V/H Note 2	Material <sup>Note1</sup>	Equip. Volume (m³)	Liquid Inventory (m³)
D-420-2	De-Ethaniser	V	K402	33.5	16.75
D-420-1	Stabiliser	V	K402	10.3	5.15
D-430-2	De-Propaniser	V	K404	20.9	10.45
D-430-1	De-Propaniser	V	К404	14.3	7.15
F-4003	Propane Storage Vessel	Н	Propane	113	51.32 Note 3
F-4004	Propane Storage Vessel	Н	Propane	230	106.59 Note 3





Equipment Tag no.	Description	V/H Note 2	Material <sup>Note1</sup>	Equip. Volume (m³)	Liquid Inventory (m³)
F-4001	Butane Storage Vessel	Н	Butane	66	51.29 Note 4
F-4002	Butane Storage Vessel	Н	Butane	113	44.45 Note 4
F-315	Propane Refrigerant Surge Drum	Н	Propane	9.2	4.6
D-315-2	Propane Refrigerant Economiser	Н	Propane	17.6	5.3

Notes:

- 1. Material composition is provided in Assumptions Register [Ref. 1].
- 2. V denotes vertical vessel, H denotes horizontal vessel.
- 3. Mass inventory values (26 tonnes, 54 tonnes) were converted to volume respectively using Propane density of 506.6 kg/m<sup>3</sup> at 2 barg, 15°C [Ref. 6].
- 4. Mass inventory values (30 tonnes, 26 tonnes) were converted to volume respectively using Butane density is 585.0 kg/m<sup>3</sup> at 2 barg, 15°C [Ref. 6].

#### **Toxic Effects**

Fatality probabilities when exposed to toxic gas as a function of concentration and exposure duration can be calculated by using a probit function in the form given below:

Probit =  $a + b \ln (C^n \cdot t)$ 

where:

- t = exposure durations in minutes
- C= concentration in ppm
- a, b and n = material specific probit constants

The toxic materials handled onsite include:

- Ammonia;
- Methanol;
- Ethyl Mercaptan (odorant);
- t-Butyl Mercaptan (odorant); and
- Carbon Dioxide.

UK HSE [Ref. 20] gives the following toxic load values for toxic materials as shown in Table 4-8.





# Table 4-8 : UK HSE Dangerous Toxic Load (DTL) for Specified Level of Toxicity (SLOT) and Significant Likelihood of Death (SLOD) Values

Material	n	SLOT DTL (ppm <sup>n.</sup> min)	SLOD DTL (ppm <sup>n.</sup> min)
Ammonia	2	3.78 x 10 <sup>8</sup>	1.03 x 10 <sup>9</sup>
Methanol	1	8.02 x 10 <sup>5</sup>	2.67 x 10 <sup>6</sup>
Ethyl mercaptan	1	1.66 x 10 <sup>5</sup>	6.62 x 10⁵
t-Butyl mercaptan	1	9.9 x 10 <sup>5</sup>	3.96 x 10 <sup>6</sup>
Carbon Dioxide	8	1.5 x 10 <sup>40</sup>	1.5 x 10 <sup>41</sup>

By solving the simultaneous equation, the other constants a and b can be calculated. The probit constants for toxic materials onsite are shown in Table 4-9.

Material	а	b	n
Ammonia	-43.24	2.32	2
Methanol	-23.67	1.94	1
Ethyl mercaptan	-17.58	1.68	1
t-Butyl mercaptan	-20.53	1.68	1
Carbon Dioxide	-90.94	1.01	8

	Table	4-9	÷	Probit	Constants
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# 4.3 Vapour Cloud Explosion and UK HSE Research Report RR1113 Findings

The UK Buncefield Oil Depot explosion and fire in December 2005 is of particular interest for sites with vapour cloud explosion (VCEs) potential. UK HSE Research Report RR1113 (Review of Vapour Cloud Explosion Incidents) [Ref.22] describes post-Buncefield work undertaken by the UK HSE (along with US safety regulators) to consolidate previous research and analysis on vapour cloud development and explosions into a single review of historical incidents.

The review focusses on source terms, cloud development and explosion mechanics for both permanent fuel gases C2-C4 (e.g. LPG) and volatile liquids C4-C6 (e.g. gasoline). The report notes that, once a stable current of cold heavy vapour forms, the subsequent development of LPG and gasoline clouds are similar [Ref.22]. Those operating sites handling LPG should therefore be interested in records of vapour cloud development and VCEs at gasoline sites and vice versa.

There is one gasoline tank (F-4033) at the KGTP site. However, the tank has a volume of 65 m3 and filling rate of approximately 2 m3/hr, which is much lower than the 100 m3/hr "in-scope tank" criteria for Buncefield type overflow scenarios consideration [Ref. 24]. The Buncefield type overflow scenario assessment is therefore not addressed in this report.

The KGTP site handles and stores LPG, and it is acknowledged that the LPG spray releases could potentially form large vapour clouds under nil/ very low wind conditions (< 1.3m/s).

RR1113 notes that under nil / very low wind speed conditions (<1.3 m/s) vapour dispersion will be gravity-driven, and the vapour cloud will continue to grow for as long as the release continues (spreading out in all directions and/or following any downward slopes around the release source).



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These large vapour clouds are almost certain to ignite, and the probability of a severe explosion event (open area VCE) is high, especially for gasoline. However, for LPG incidents, it is suggested that the clouds formed can be very rich or even over the upper flammability limit (UFL) and as such the risk of an open area VCE is most likely less than 50%. RR1113 concluded that additional experimental and modelling work is required determine what kind of LPG spray releases in nil/very low wind conditions could results in clouds within the flammable range.

The report also concludes that although the transition to a severe explosion seems to involve some degree of congestion or confinement as an initiator, the overpressure effects are not limited to areas of congestion or confinement. The report suggests that overpressures in this scenario could be in excess of 2000 mbar, with 100% fatalities throughout the extent of the large flammable cloud at time of ignition.

However, at this point in time, the explosion propagation mechanism through open/uncongested areas is subjected to considerable academic debate, and there are no commonly available methods to reproduce these specific conditions and subsequent high levels of overpressure with current industry standard explosion models (e.g. Multi Energy Method). Furthermore, the UK HSE Vapour Cloud Assessment (VCA) method provided in RR908 / FABIG 12 [Ref.26, 27] addresses gasoline overfill, but does not address LPG releases. As such, the LPG vapour cloud formation under nil/ very low wind conditions have not been quantified in this QRA.

The findings of RR1113 are highlighted in this assessment to reinforce the maintenance of plant integrity as critical risk reduction measures and suggest that the value of mitigation measures such as vapour detection should be reviewed. Site emergency response planning should take into consideration the LPG vertical spray release scenarios under nil / very low wind conditions.





# 5 HAZARD IDENTIFICATION

# 5.1 Hazardous Materials

The material compositions used in the QRA modelling are based on information and confirmation provided by Todd [Ref. 4, 5, 16].

Any stream that will generate different consequences is represented by different sections. For node sections with similar operating conditions or fluid composition that will generate similar consequence results, the stream which results in worst case result is selected as representative to rationalise the number of scenarios performed. This is also to avoid the method of averaging out the inputs of different feed gas streams as it may create a stream with 'brand new' operating conditions, material compositions and flowrates which does not represent the actual release conditions.

The effect of CO in hydrocarbon mixtures on fire hazards is considered to avoid over/under conservatism in the QRA. Research [Ref. 18] has found that CO<sub>2</sub>/methane mixture were ignitable up to a CO<sub>2</sub> concentration of 60%. Following the research findings, hydrocarbon mixtures with CO<sub>2</sub> concentration of up to 60 vol% are assumed to remain flammable and modelled in the QRA to account for the fire and explosion hazards. CO<sub>2</sub> toxic effects on personnel fatalities are considered in the QRA study as discussed in Section 4.2.7. It is noted that the CO<sub>2</sub> toxic fatality effects are only considered for scenarios with equipment containing pure CO<sub>2</sub>.

As far as is reasonable, the compositions in each stream are simplified (i.e. isomers are summed together). The important characteristic of molecular weight is kept close to the actual value to ensure the release rate is representative.

In addition to the material composition provided in process condition summary [Ref. 4], the following materials and the associated compositions are used in the QRA as well:

- Product gas (89 mol% Methane and 11 mol% Ethane);
- LPG (60 mol% Propane and 40 mol% Butane); and
- Natural Gasoline (50 mol% Pentane and 50 mol% Hexane).

Detailed stream compositions used for each isolatable sections/node were provided in Assumptions Register [Ref. 1].

Diesel and lube oil have high flash points and considered as combustible liquids, thus not further modelled in the QRA study. The flash point of a liquid is the lowest temperature at which a liquid will form a vapour in the air near its surface. For substances with high flash point, presence of major heat sources such as pre-existing fire [Ref. 7] are required to heat the substances above its flash point before it can be ignited in air.

# 5.2 Isolatable Sections

An ESD system can limit the outflow once a loss of containment occurs. When activated, ESDVs divide the process system into a number of isolatable sections, with each potential leak source associated with a particular isolatable inventory. These sections were split further where necessary and the entire contained inventory was considered as available for release.

Node sections highlighted in the Piping & Instrumentation Diagrams (P&IDs) are presented in Appendix 1. Details of the node sections for Base Case and Sensitivity Case 2 are presented in Table 5-1. Inventory calculation for Sensitivity Case 1 are detailed in Section 8.1.1.





# 5.3 Release Scenarios

Release rates were calculated based on the release hole sizes and fluid pressure/ tank head pressure. The height of release from all scenarios is assumed to be at 1 m above ground, although some equipment may be located at the elevation higher than the ground level. It is assumed that 70% of the releases are horizontal and 30% of the releases are vertical.

The release scenarios and the respective operating conditions used in the QRA study are presented in Table 5-1.

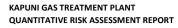




#### Table 5-1: Release Scenarios and Operating Conditions

Node	Description / Boundaries	Stream No. <sup>(Note 1)</sup>	т (° с)	P (barg)	Max Pipe / Hose Diameter (mm) <sup>(Note 2)</sup>	Pipe / Hose Length (m) (Note 3)	Volume of Isolatable Section (m <sup>3</sup> )
	Raw Gas and Maui Gas	Lines					
KGT01_RGS_01_V	Raw Gas header from KPS/KGTP Site Boundary via Inlet Separator (M-507) and Clanton Separator (M-105) to Absorber Towers (D-101-1/2) inlet valves (PV101- 1/2), Cogen Plant Header (XSV-603), LTS Plant Gas Header and bypass to Separator (D-201-4) top line	K101	15	40	500	259	233.0
KGT01_RCS_01_L	Raw Condensate from Cyclone Bank (M-507) bottom to LPG Surge Vapouriser (F-201) inlet (liquid inventory taken up to XSV-516)	К919	15	40	100	218	4.1
KGT01_MAU_01_V	Maui Gas from 300 line & 309 line (XSV-594) adjoining with Product Gas Compressors Inlet header and sending Maui Gas export to AUP/ Ballance & Lactose Plant -306 line (up to XSV-9622)	К502	15	45	500	111	233.0
KGT01_MAU_02_V	Maui Gas export via Dry Gas In-line Filter (M-512) to A/U Plant- 112 line (up to HV-300)	К502	15	45	100	63	233.0
	CO <sub>2</sub> Removal						
KGT02_TGS_01_V	Treated gas from top of $CO_2$ Absorber Tower (D-101-1) via Gas Cooler (E-105-1) and Gas Separator (M-101-1) to FV-102-1 (Benfield Train 1)	K102	42	40	300	15	36.2
KGT03_TGS_04_V	Treated gas from top of $CO_2$ Absorber Tower (D-101-2) via Gas Cooler (E-105-2) and Gas Separator (M-101-2) to FV-102-2 (Benfield Train 2)	К102	42	40	250	15	36.0
	Dehydration and Dewpoir	t Control					
KGT01_TGS_07_V	Treated gas from CO <sub>2</sub> Removal Unit via Decanted Water Stripper (D-201-3) and Wash Water Stripper (D-201-4) to Chilling System	К203	42	40	300	48	233.0
KGT01_TGS_10_V	Treated gas from Strippers via Gas/Gas Heat Exchangers (E-313-1/2) and Gas Chiller (E-313-3) to Low Temperature Separator (M-313) inlet	К203	42	40	300	48	233.0
KGT01_TGS_12_V	Treated gas from Strippers via Gas/Liquid Heat Exchanger (E-303-4) adjoining with Gas Chiller (E-313-3) inlet line	К203	42	40	200	49	233.0
KGT01_PGS_02_V	Product gas from Low Temperature Separator (M-313) and Two-Phase Separator (M-314) via Gas/Gas Heat Exchangers (E-313-1/2) to Product Gas header (PV-337)	К205	12	40	200	15	233.0
KGT04_PGS_07_V	Product gas from top of High Temperature Separator (M-307) to Product Gas header (PV-380)	K205	12	40	80	15	2.4
KGT01_MPG_01_L	Mixed LPG from bottom of Low Temperature Separator (M-313) and Two-Phase Separator (M-314) to FV-357 on outlet line	K204	12	40	80	15	56.3
KGT04_MPG_03_L	Mixed LPG from FV-357 on outlet line of Two-Phase Separator (M-313) via Gas Liquid Heat Exchanger (E-303-4) to High Temperature Separator (M-307) inlet	K204	12	40	100	35	4.0
KGT04_MPG_04_L	Mixed LPG from bottom of High Temperature Separator (M-307) to HT Separator Condensate Pumps (G-301-1/2) suction. (G-301-2 is on stand-by)	К204	12	40	150	15	4.0
KGT04_MPG_05_L	Mixed LPG from HT Separator Condensate Pump (G-301-1) Discharge to Wash Water Coalescer (M-302) inlet	K204	12	40	100	15	4.0
KGT04_MPG_06_L	Mixed LPG from Wash Water Coalescer (M-302) to LPG Production Unit (XSV- 332)	K204	12	40	100	15	4.0
	Product Gas Lines and Con	npressors					
KGT01_PGS_01_V	Product Gas header from Dehydration and Dew Point Unit to Product Gas Compressors Inlet header, domestic supply and sending Product Gas export to KPS and Whareroa (up to KPS/KGTP Site Boundary)	К501	15	40	400	229	233.0
KGT01_PGS_13_V	Product Gas from Product Gas header to blanket Hydrocarbon Separator (M-111) top section	К501	15	40	100	15	233.0
KGT01_PGS_14_V	Product Gas from Product Gas Header (FV-0106) via LTS pipe bridge to XSV- 0109 near Gas Storage Compressors in LTS unit	К505	15	40	200	274	233.0
KGT13_PGS_15_V	Product Gas from XSV-0109 to Gas Storage Compressors (D4-0401/0402) Inlet (D4-0402 is on standby.)	K901	15	40	500	56	23.5
KGT13_PGS_16_V	Product Gas from Gas Storage Compressor (D4-0401) Discharge via Gas Storage Compressor Cooler (D2-0402) to Coalescer (D11-0417) inlet	К901	15	40	150	51	23.5
KGT13_PGS_17_V	Product Gas export from Coalescer (D11-0417) to Gas Storage/ 070 Pipeline (XSV-0112)		15	40	500	51	23.5
KGT01_MGS_01_V	Mixed Gas from Process Gas header and Maui Gas line to suction of Product Gas Compressor (C-903-2/3/5) (C-903-3 is on standby.)	К501	15	40	400	91	233.0
KGT01_MGS_03_V	Mixed Gas from Product Gas Compressor (C-903-2) Discharge	K506	40	70	200	15	233.0
KGT01_MGS_07_V	Mixed Gas from Product Gas Compressor (C-903-5) Discharge	К506	40	70	200	15	233.0
KGT11_MGS_05_V	Mixed Gas discharge header to the flange to the flange with Transmission export line	K506	40	70	350	91	41.3
KGT11_MGS_08_V	Mixed Gas domestic supply to Stores/ Workshop/ Admin. Building	K506	40	70	50	251	41.3
KGT11_MGS_09_V	Mixed Gas export from Product Gas Compressor Discharge header via Oil Coalescer (M-919) to 100/200 Pipelines in Transmission metering area and side uses as purge gas for Odorant Injection Tank (F-553) and instrument gas for XSV-0107	К506	40	70	350	278	41.3







Node	Description / Boundaries		т (° С)	P (barg)	Max Pipe / Hose Diameter (mm) <sup>(Note 2)</sup>	Pipe / Hose Length (m) (Note 3)	Volume of Isolatable Section (m <sup>3</sup> )
	Pigging						
KGT01_PIG_01_V	Pig Receiver - 300 and 309 Pipeline (M-918)	K502	15	45	500	-	233.0
KGT13_PIG_02_V	LTS Pig Launcher (M-917)	К901	15	40	500	-	23.5
KGT11_PIG_03_V	Kapuni North Pig Launcher - 200 Pipeline (M-915)	К506	40	70	200	-	41.3
KGT11_PIG_04_V	Kapuni South Pig Launcher - 100 Pipeline (M-916)	K506	40	70	200	-	41.3
	Utilities and Cogen U	Jnit		1			
KGT01_MPG_21_V	Mixed LPG from top of LPG Surge Vaporiser (F-201) via Rich Fuel Gas Separator (M-201-2) to HRSG burners (B-604-A-1/2/3, B-604-B1/2/3) in Cogen. Unit	К919	88	3.9	100	78	233.0
KGT01_MPG_22_L	Mixed LPG at bottom of LPG Surge Vaporiser (F-201)	K919(L)	88	3.9	50	15	56.3
KGT01_MPG_23_L	Mixed LPG from bottom of Hydrocarbon Separator (M-111) to LPG Surge Vapouriser (F-201) inlet	К919	15	40	50	50	56.3
KGT01_FGA_01_V	Product Gas from Product Gas header via Fuel Gas Heater (E-602) and Fuel Gas KO Pot (M-601) to Fuel Gas Superheater (E-603)	K503	15	40	150	38	233.0
KGT01_FGA_02_V	Fuel Gas from Fuel Gas Superheater (E-603) via Fuel Gas Filters (M-628-A/B) to HRSG A/B Burners (B-604-A-1/2/3, B-604-B1/2/3) (M-628-B is on standby.)	К503	15	40	150	138	233.0
KGT01_PGS_19_V	Product gas from Product Gas header to Ammonia/ CO <sub>2</sub> Compressor Engines (CE-821/822) in CO2 Recovery Unit	K501	15	40	50	154	233.0
KGT01_PGS_21_V	Product gas from Product Gas header to Gas Flare System Burners (D1-4100B)	K501	15	40	100	274	233.0
	LPG Production Facility - Stabilis	er, De-Ethanis	ser				
KGT01_MPG_07_L	Mixed LPG from Dehydration unit (XSV-332) via De-Ethaniser Feed Preheater (E- 420-3) to De-Ethaniser (D-420-2) inlet (LPG Production Train 2)	K401	12	30	100	194	56.3
KGT01_DET_01_V	De-Ethaniser (D-420-2) Top Vapour via De-Ethaniser OVHD Condenser (E-420-2) and De-Ethaniser Reflux Drum (F-420-2) to XSV-411-2 on inlet line to OVHD Compressor Suction Scrubber (M-422) (LPG Production Train 2)	K408	20	30	100	15	233.0
KGT01_PGS_04_V	Product gas from De-Ethaniser(D-420-2) via top of Suction Scrubber (M-422) to OVHD Compressor (C-421-1/2) inlet (LPG Production Train 2) (C-421-2 is on standby.)	K408	20	30	80	110	233.0
KGT01_PGS_05_V	Product gas from De-Ethaniser OVHD Compressor (C-421-1) discharge via De- Ethaniser OVHD Compressor Cooler (E-421-1) to Product gas header and to adjoining Treated Gas line from Strippers (LPG Production Train 2)	K408	20	30	200	143	233.0
KGT01_DEX_01_L	Reflux from De-Ethaniser Reflux Drum (F-420-2) via De-Ethaniser Reflux Pumps (G-420-1/2) to De-Euthaniser (D-420-2) top side (LPG Production Train 2) (G-420-2 is on standby.)	К402	100	30	80	15	56.3
KGT01_DEB_01_L	De-Ethaniser (D-420-2) Bottom Liquid to/from De-Ethaniser Reboiler (E-422-2) and to De-Propaniser Feed Surge Drum (F-420-3) inlet (LPG Production Train 2)	K402	100	30	150	15	56.3
KGT01_MPG_09_L	Mixed LPG from Bottom of De-Propaniser Feed Surge Drum (F-420-3) to De- Propaniser (D-430-1/2) inlet	K402	100	30	150	22	56.3
KGT01_MPG_10_V	Mixed LPG from Top of De-Propaniser Feed Surge Drum (F-420-3) to De- Propaniser (D-430-2) inlet	K402	100	30	100	15	233.0
	LPG Production Facility - De	-Propaniser					
KGT01_DPT_11_V	De-Propaniser (D-430-2) Top Vapour via De-Propaniser Condenser (E-430-2) to De-Propaniser Reflux Drum (F-430-2) (LPG Production Train 2)	K403	20	14	150	15	233.0
KGT01_DPX_11_L	Reflux from De-Propaniser Reflux Drum (F-430-2) via De-Propaniser Reflux Pumps (G-430-3/4) to De-Propaniser (D-430-2) (LPG Production Train 2) (G-430-4 is on stand-by.)	К403	20	14	100	15	56.3
KGT01_PC3_02_L	Product propane from De-Propaniser Reflux Pump (G-430-3) via Propane Product Cooler (E-4001-2) to XSV-417-2 on the export line to Storage (LPG Production Train 2)	К403	20	14	50	15	56.3
KGT01_DPB_11_L	De-Propaniser (D-430-2) Bottom Liquid to/from De-Propaniser Reboiler (E-432- 2) and to De-Butaniser (D-440-1/2) (LPG Production Train 2)	K404	105	14	150	56	56.3
	LPG Production Facility	- De-C4					
KGT01_DBT_11_V	De-Butaniser (D-440-2) Top Vapour via De-Butaniser Condenser (E-440-2) to De- Butaniser Reflux Drum (F-440-2) and to Surge Vaporiser (F-201) (LPG Production Train 2)	K405	20	7	150	168	233.0
KGT01_DBX_11_L	Reflux from De-Propaniser Reflux Drum (F-440-2) via De-Butaniser Reflux Pumps (G-440-3/4) to De-Butaniser (D-440-2) (LPG Production Train 2) (G-440-4 is on standby.)	K405	20	7	80	15	56.3
KGT01_NGL_01_L	Natural Gasoline from bottom of De-Butaniser (D-440-2) and De-Butaniser Reboilers (E-442-1/2) to De-Ethaniser FEED Pre-Heater (E-420-3) inlet (LPG Production Train 2) (E-442-1 is on standby.)	К406	115	7	150	42	56.3
KGT01_NGL_02_L	Natural Gasoline from De-Ethaniser Feed Pre-Heater (E-420-3) via Gasoline Cooler (E-460) to the export lines KPS and Storage (XSV-416 and XSV-481-1)	K407	20	7	150	23	56.3





Node	Description / Boundaries	Stream No. <sup>(Note 1)</sup>	т (° С)	P (barg)	Max Pipe / Hose Diameter (mm) <sup>(Note 2)</sup>	Pipe / Hose Length (m) (Note 3)	Volume of Isolatable Section (m <sup>3</sup> )
	LPG Production Facility - Product E	xport and Loa	dout				
KGT32_NGL_05_L	Natural Gasoline from XSV-416 in LPG Production Unit to KPS (up to KPS/KGTP Site Boundary)	K507	20	7	50	210	0.4
KGT33_NGL_06_L	Natural Gasoline from LPG Production Unit (XSV-481-1) to XSV-4073 on the inlet to NGL Storage Tank (F-4033)	K703	15	7	100	578	4.7
KGT34_NGL_07_L	Natural Gasoline Storage Tank (F-4033)	К706	15	ATM	-	-	65.0
KGT35_NGL_09_L	Natural Gasoline export from Natural Gasoline Storage Tank (F-4033) via Natural Gasoline Load Out Pump (G-4033) to XSV-4068 on the NGL export line	K803	15	2.95	100	15	0.1
KGT36_NGL_10_L	Natural Gasoline from XSV-4068 to NGL Tanker Loading Hose (T-4003) inlet	K803	15	2.95	100	15	0.1
KGT36_NGL_11_L	Natural Gasoline Loadout Hose (T-4003)	K803	15	2.95	100	-	0.1
KGT36_NGL_12_L Note 4	Natural Gasoline Road Tanker	K803	15	2.95	100	-	20 tonnes
KGT37_PC3_05_L	Product Propane export from LPG Production Unit (XSV 417-2) to SDV-4004 on the inlet lines to Propane Storage Vessels (F-4003, F-4004)	К701	15	14	80	-	2.5
KGT39_PC3_07_V	Vapour Section of Propane Storage Vessel (F-4003)	K704	15	7	-	-	61.7
KGT39_PC3_08_L	Liquid Section of Propane Storage Vessel (F-4003)	К704	15	7	-	-	51.3
KGT40_PC3_09_V	Vapour Section of Propane Storage Vessel (F-4004)	К704	15	7	-	-	123.4
KGT40_PC3_10_L	Liquid Section of Propane Storage Vessel (F-4004)	K704	15	7	-	-	106.6
KGT41_PC4_04_L	Product Butane export from LPG Production Unit (XSV-419-2) to SDV-4005 on the inlet lines to Butane Storage Vessels (F-4001, F-4002)	K702	15	7	80	562	2.6
KGT43_PC4_06_V	Vapour Section of Butane Storage Vessel (F-4001)	K705	15	2	-	-	14.7
KGT43_PC4_07_L	Liquid Section of Butane Storage Vessel (F-4001)	К705	15	2	-	-	51.3
KGT44_PC4_08_V	Vapour Section of Butane Storage Vessel (F-4002)	К705	15	2	-	-	68.6
KGT44_PC4_09_L	Liquid Section of Butane Storage Vessel (F-4002)	К705	15	2	-	-	44.5
KGT45_PC3_12_L	Product Propane export from Propane Storage Vessels (F-4003, F-4004) via Propane Loadout Pumps (G-4002/4024) to SDV-4017 on the LPG export line (G-4002 is on standby.)	К801	15	10	200	15	0.5
KGT46_PC4_11_L	Product Butane export from Butane Storage Vessels (F-4001, F-4002) via Butane Loadout Pump (G-4001) to SDV-4016 on the LPG export line	K802	15	5	200	15	0.5
KGT47_LPG_01_L	Product LPG export from SDV-4016/4017 to LPG Loadout Arm (T-4002)	K806	15	7.5	100	15	0.1
KGT47_LPG_02_L	LPG Loadout Arm (T-4002)	K806	15	7.5	80	-	0.1
KGT47_LPG_03_L Note 4	LPG Road Tanker	K806	15	7.5	80	-	20 tonnes
KGT47_LPG_05_L	LPG Loadout Smart Hose to Isotainers	K806	15	7.5	50	-	0.1
KGT47_LPG_06_L Note 4	New LPG Road Tanker (Isotainer)	K806	15	7.5	50	-	12 tonnes
	Propane Refrigeration S	System					
KGT70_REF_01_V	Vapour section of Propane Refrigerant Surge Drum (F-315)	К302	-34	1	100	15	36.4
KGT70_REF_02_L	Propane refrigerant from bottom of Propane Refrigerant Surge Drum (F-315) to Propane Refrigerant Economiser (D-315-2) inlet	K301	15	4	100	15	25.2
KGT70_REF_03_V	Propane refrigerant from Propane Refrigerant Economiser (D-315-2) to Compressors (C-330-1/ C-330-2) inter-stage suction	K301	15	4	150	22	36.4
KGT70_REF_04_L	Propane refrigerant from bottom of Propane Refrigerant Economiser (D-315-2) to each user (E-313-3, E-420-2) (E-303-3 is on standby.)	К301	15	4	200	174	25.2
KGT70_REF_05_L	Propane refrigerant in Gas Chiller (E-313-3)	К302	-34	1	150	15	25.2
KGT70_REF_07_L	Propane refrigerant in De-Ethaniser Reflux Drum (E-420-2)	К302	-34	1	150	15	25.2
KGT70_REF_11_V	Propane refrigerant from each user via Propane Compressor Suction Scrubber (M-333) to Compressors (C-330-1/ 2) suction	K302	-34	1	300	154	36.4
KGT70_REF_14_V	Propane refrigerant from Compressors (C-330-1/2) discharge via Oil Separator (M-330-1/2) to Propane Refrigerant Condensers (E-317-1A/B, E-317-2) inlet	К301	15	4	250	65	36.4
KGT70_REF_15_L	Propane refrigerant from Propane Refrigerant Condensers (E-371-1A/B, E-317- 2) to Propane Refrigerant Surge Drum (F-315) inlet	К301	15	4	200	28	25.2
	Mercaptans and Meth	nanol					
KGT50_EMC_01_L	Ethyl Mercaptan from Transportable Odorant Drums (F-4007-A/ B) via Odorant Injection Pump (G-4011) to LPG Loadout Arm (T-4002) inlet (F-4007-B is on standby.)	К804	15	10	15	15	0.2
KGT50_EMC_02_L	Ethyl Mercaptan Transportable Odorant Drums (F-4007-A/ B)	K805	15	1	-	-	0.2
KGT51_BMC_05_L	t-Butyl Mercaptan Portable Odorant Tank (F-521) to domestic gas supply header	K603	15	8	-	-	0.1
KGT52_BMC_01_L	t-Butyl Mercaptan Odorant Injection Tank (F-553)	K603	15	1	-	-	19.0





Node	Description / Boundaries		Description / Boundaries Stream No. (Note 1) T (° C)	P (barg)	Max Pipe / Hose Diameter (mm) <sup>(Note 2)</sup>	Pipe / Hose Length (m) (Note 3)	Volume of Isolatable Section (m <sup>3</sup> )
KGT52_BMC_02_L	t-Butyl Mercaptan from Odorant from Odorant Injection Tank (F-553) via Odorant Injection Pumps (G-552-A/B) to Transmission export lines (100/200 lines) (G-552-B is on standby.)		15	80	15	15	19.0
KGT52_BMC_03_L	t-Butyl Mercaptan Filling Hose	K603	15	1	50	-	19.0
KGT53_BMC_04_L Note 4	L t-Butyl Mercaptan Road Tanker		15	1	50	-	16 tonnes
KGT55_MOH_01_L	Methanol Storage Tanks (F-502-1/2/4/6)	K918	15	ATM Liquid head (2.7m)	-	-	8.7
KGT55_MOH_02_L	Methanol from Methanol Storage Tanks (F-502-1/2/4/6) via Metering Pumps (G-309-1/2, G-319-1/2) to users (G-309-2, G-319-2 are on standby.)	K917	15	50	25	343	8.7
KGT55_MOH_03_L	Methanol Filling Hose	К918	15	0	40	-	8.7
KGT56_MOH_04_L	Methanol Road Tanker	К918	15	0	40	-	4 tonnes
	CO <sub>2</sub> Recovery - Amm	onia					
KGT80_AMM_01_V	Ammonia gas from Ammonia Compressor (C-888) discharge to Ammonia Condenser (E-895) through Oil Separator (M-892) (Train A)	к908	15	15	150	15	3.3
KGT80_AMM_11_V	Ammonia gas from Ammonia Compressor (C-821) discharge to Ammonia Receiver (F-823) through Oil Separator (M-825) and Ammonia Condenser (E- 825) (Train B)	К908	15	15	150	15	3.3
KGT80_AMM_02_V	Ammonia gas section of Liquid Receivers (F-803/F-823)	К908	15	15	32	15	3.3
 KGT80_AMM_03_L	Ammonia liquid from Ammonia Condensers (E-895/825) to Liquid Receiver (F- 803/F-823)	к908	15	15	100	15	4.9
KGT80_AMM_04_L	Ammonia liquid from Liquid Receivers via Liquid Sub-Coolers (E-826/896) and CO <sub>2</sub> Condenser (E-804) to Oil Receiver (M-828)	к908	15	15	100	21	4.9
KGT80_AMM_07_L	Ammonia liquid from SV-825 and SV-896C via Oil Receiver (M-828) (coil) to CO <sub>2</sub> Chiller (E-803)	к908	15	15	25	38	4.9
KGT80_AMM_08_V	Ammonia gas return from CO <sub>2</sub> Condenser (E-804) and Oil Receiver (M-828) to Ammonia Compressors (C-888/821) suction	к909	-30	0	250	15	3.3
KGT80_AMM_09_V	Ammonia gas return from CO <sub>2</sub> Chiller (E-803) and liquid ammonia vaporising via Liquid Sub-Coolers (E-826/896) to Ammonia Compressors (C-888/821) suction	к909	-30	0	80	48	3.3
	CO <sub>2</sub> Recovery - CC	)2		1			
KGT90_CO2_01_V	$CO_2$ gas from $CO_2$ Compressor (C-802) Discharge via Pulsation Vessel (F-806), Intercooler (E-807) and Interstage Separator (M-830) to After Cooler (E-802) inlet (Train A)	К910	-26.6	15	100	15	45.6
KGT90_CO2_02_V	$CO_2$ gas from $CO_2$ Compressor (C-822) Discharge via Pulsation Vessel (F-826), Intercooler (E-827) and Interstage Separator (M-829) to After Cooler (E-802) (Train B)	К910	-26.6	15	100	15	45.6
KGT90_CO2_03_V	$CO_2$ gas from $CO_2$ After Cooler (E-802) via Aftercooler Separator (M-881) and via $CO_2$ Chiller (E-803) to Chiller Separator (M-882)	К910	-26.6	15	100	31	45.6
KGT90_CO2_07_V	$CO_2$ gas from Chiller Separator (M-882) outlet via $CO_2$ Purifiers(M-807-1/2), $CO_2$ Driers (B-801-1/2) and $CO_2$ Particulate Filters (M-879-1/2) to $CO_2$ Condenser (E- 804) inlet adjoin with $CO_2$ gas lines from Storage Tanks (F-801-1/2/3) (M-807-2, B-801-2 and M-879-2 are on standby.)	К910	-26.6	15	80	89	45.6
KGT90_CO2_08_L	$CO_2$ liquid from $CO_2$ Condenser (E-804) via $CO_2$ Liquid Receiver (F-802) and $CO_2$ Condenser Pump (G-883) to Liquid $CO_2$ Storage Tanks (F-801-1/2/3) inlet	К910	-26.6	15	100	71	223.0
KGT90_CO2_16_V	$CO_2$ gas from Aftercooler Separator (M-881) and Raw Gas Boosters (C-885/823) discharge via Catalyst Carbon Vessels (D-821/ D-801) to $CO_2$ Compressors (C-802/822) suction	К907	15	1	300	180	45.6
KGT90_CO2_18_V	CO <sub>2</sub> gas from Storage Tanks (F-801-1/2/3) to users (Compressor shelters, LPG Storage tanks and LPG Loading facility)		15	0.094	50	796	45.6
KGT90_CO2_19_V	$CO_2$ gas for Regeneration Cycle via Regeneration Heaters (B-802/ B-803), $CO_2$ Purifier (M-807-2), $CO_2$ Drier (B-801-1)	К922	15	0.1	80	15	45.6
KGT90_CO2_09_L	Liquid CO <sub>2</sub> Storage Tank (F-801-1)	К910	-26.6	15	-	-	223.0
KGT90_CO2_10_L	Liquid CO <sub>2</sub> Storage Tank (F-801-2)	К910	-26.6	15	-	-	223.0
KGT90_CO2_11_L	Liquid CO <sub>2</sub> Storage Tank (F-801-3)	К910	-26.6	15	-	-	223.0
KGT90_CO2_12_L	Air Liquide CO <sub>2</sub> Storage Tank (F-811)	К910	-26.6	15	-	-	223.0
KGT90_CO2_24_L	Liquid $CO_2$ from Storage Tanks (F-801-1/2/3) via $CO_2$ loadout pumps (G-821, G-801-1/2) to BOC $CO_2$ Road Tanker Loadout Connections	К906	-26.6	15	100	71	223.0
KGT90_CO2_25_L	Liquid CO <sub>2</sub> from Air Liquid CO <sub>2</sub> Storage Tank (F-811) via G-812 to Air Liquid Road Tanker Loadout Connection	К906	-26.6	15	50	15	223.0
KGT90_CO2_26_V	$CO_2$ gas to Storage Tanks (F-801-1/2/3) from BOC $CO_2$ Road Tanker Revert Connections	К906	-26.6	15	50	23	45.6
KGT90_CO2_27_V	CO <sub>2</sub> gas to from Air Liquid CO <sub>2</sub> Storage Tank (F-811) from Air Liquid Road Tanker Revert Connection	K906	-26.6	15	25	15	45.6



QUANTITATIVE RISK ASSESSMENT REPORT



Node	Description / Boundaries	Stream No. <sup>(Note 1)</sup>	т (° С)	P (barg)	Max Pipe / Hose Diameter (mm) <sup>(Note 2)</sup>	Pipe / Hose Length (m) (Note 3)	Volume of Isolatable Section (m <sup>3</sup> )
KGT90_CO2_28_L	Vector CO <sub>2</sub> Loadout connection	К906	-26.6	15	50	-	223.0
KGT90_CO2_29_V	BOC CO <sub>2</sub> Road Tanker Revert connections	К906	-26.6	15	25	-	45.6
KGT90_CO2_30_L	BOC CO <sub>2</sub> Road Tanker Loadout Connection	К906	-26.6	15	80	-	223.0
KGT90_CO2_31_V	Air Liquide Road Tanker Revert connection	К906	-26.6	15	25	-	45.6
KGT90_CO2_32_L	Air Liquide Road Tanker Loading connection	К906	-26.6	15	50	-	223.0
KGT90_CO2_33_L Note 4	Vector CO <sub>2</sub> Road Tanker	К906	-26.6	15	50	-	18 tonnes
KGT90_CO2_34_L Note 4	BOC CO <sub>2</sub> Road Tanker	К906	-26.6	15	80	-	18 tonnes
KGT90_CO2_35_L Note 4	Air Liquide Road Tanker	К906	-26.6	15	50	-	18 tonnes

Notes:

- 1. Stream compositions are provided in Assumptions Register [Ref. 1].
- 2. The maximum pipe/hose diameters of each node are determined using the P&IDs.
- 3. The piping lengths are measured from the KGTP layout drawings using scale [Ref. 17]. A safety factor 1.25 has been applied to all lengths measured from the map to account for bends and elevations which could not be determined from the 2D map. See Appendix 3 for the main estimated piping lengths.
- 4. Road tankers BLEVE have been excluded in the assessment since several control measures are provided for road tankers in KGTP site as listed below. This is in line with the following TNO Purple Book [Ref. 10] recommendation where it stated "In general, the external impact LOCs for road tanker accidents do not have to be considered in an establishment if measures have been taken to reduce road accidents, like speed limits." The KGTP site specific measures are:
  - Only one LPG/ NGL loadout occurs at a time. Other vehicles are precluded from entering the area via the site access system.
  - Site speed limit
  - Deluge cage over LPG loadout area





# 6 FREQUENCY ANALYSIS

### 6.1 Release Frequency Assessment

Following the nodes sectionalisation, parts (equipment) count on each release scenario is conducted based on Piping & Instrumentation Diagrams (P&IDs) to estimate the release frequency. The summary of estimated release frequencies for each KGTP unit for the Base Case are presented in Table 6-1. The detail breakdown of release frequencies for each node sections are provided in Appendix 4.

	Base Case Release Frequencies (per year) Note 1								
Node Section	1 - 3 mm	3 - 10 mm	10 - 50 mm	50 - 150 mm	> 150 mm	Total	% Contrib.		
Raw Gas and Maui Gas Lines	1.50E-02	6.58E-03	3.50E-03	6.07E-04	1.03E-04	2.58E-02	2.9%		
CO <sub>2</sub> Removal	6.12E-03	2.82E-03	1.56E-03	3.83E-04	3.57E-05	1.09E-02	1.2%		
Dehydration and Dewpoint Control	2.56E-02	1.10E-02	5.66E-03	1.06E-03	2.54E-04	4.36E-02	4.9%		
Product Gas Lines and Compressors	6.28E-02	2.75E-02	1.39E-02	2.96E-03	4.61E-04	1.08E-01	12.0%		
Pigging	3.58E-06	1.85E-06	1.03E-06	2.55E-07	1.16E-07	6.83E-06	<0.01%		
Utilities and Cogen Unit	4.82E-02	1.97E-02	8.94E-03	1.86E-03	7.00E-05	7.88E-02	8.8%		
LPG Production Facility - Stabiliser, De-C2	2.89E-02	1.23E-02	5.99E-03	1.67E-03	3.58E-05	4.89E-02	5.5%		
LPG Production Facility - De-C3	1.47E-02	5.92E-03	2.82E-03	6.34E-04	1.90E-05	2.41E-02	2.7%		
LPG Production Facility - De-C4	2.09E-02	8.35E-03	3.88E-03	8.22E-04	1.62E-05	3.40E-02	3.8%		
LPG Production Facility - Product Export and Loadout	2.33E-02	6.71E-02	3.40E-03	6.87E-04	5.94E-03	1.00E-01	11.2%		
Propane Refrigeration System	3.78E-02	1.63E-02	7.60E-03	1.60E-03	3.15E-04	6.36E-02	7.1%		
Mercaptans and Methanol	1.95E-02	1.65E-02	3.85E-03	2.05E-03	8.51E-04	4.28E-02	4.8%		
CO <sub>2</sub> Recovery - Ammonia	7.07E-02	2.81E-02	1.14E-02	2.90E-03	2.50E-04	1.13E-01	12.6%		
CO <sub>2</sub> Recovery - CO <sub>2</sub>	7.98E-02	9.66E-02	1.54E-02	4.18E-03	6.80E-03	2.03E-01	22.6%		
Total	4.53E-01	3.19E-01	8.79E-02	2.14E-02	1.51E-02	8.97E-01	100.0%		
% Contribution	50.5%	35.6%	9.8%	2.4%	1.7%	100.0%	-		

Table 6-1: Releas	Frequencies Summary	for KGTP Units
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Notes:

1. Release frequencies estimated have considered the operating factor of equipment.

The total release frequencies for the Base Case scenarios within KGTP are approximately 0.9 per annum, or equivalent one leak every 1.1 years. Approximately 51% of the leak frequencies are contributed from the "1-3 mm" hole sizes range.





# 6.2 Ignition and Explosion Probabilities

The split between immediate ignition, delayed ignition and explosion probabilities for the node sections are presented in Appendix 5.





# 7 RISK ANALYSIS

This section presents QRA risk results, presented in the form of Location Specific Individual Risk (LSIR) contours. Major risk contributors at selected points on the KGTP are discussed as well.

# 7.1 Location Specific Individual Risk (LSIR)

### 7.1.1 Criteria

LSIR is defined as the risk of fatality at a point in space to a hypothetical individual at a location for 365 days per year, 24 hours a day, unprotected and unable to escape.

As there are no standard risk criteria which have been developed for the New Zealand context, the individual risk has been assessed against the suggested risk criteria in the NSW HIPAP No. 4 "Risk Criteria for Land Use Planning" [Ref. 8], as shown in Table 7-1.

Land Use	Risk Criteria Adopted (per annum)	Interpretation for QRA
Hospitals, schools, childcare facilities, old age housing	0.5E-06 (or 5E-07) (1 in 2 million)	5E-07 risk contour should not extend to these areas
Residential, hotels, motels, tourist resorts	1E-06 (1 in 1 million)	1E-06 risk contour should not extend to these areas
Commercial developments including retail centres, offices and entertainment centres	5E-06 (1 in 200,000)	5E-06 risk contour should not extend to these areas
Sporting complexes and active open space	10E-06 (or 1E-05) (1 in 100,000)	1E-05 risk contour should not extend to these areas
Industrial	50E-06 (or 5E-05) (1 in 20,000)	5E-05 risk contour should, as a target, be contained within the boundaries of the industrial site where applicable

Table	7-1:	Individual	Fatalitv	Risk	Criteria
	· -·				0

KGTP is situated in an area classified as "Rural Industrial" under the Operative South Taranaki District Plan [Ref. 23]. The KPS plant is located immediately adjacent to the north while the Ballance plant is located north-west of the KGTP site, as presented in Figure 3-1. It should be noted that the KGTP, KPS and Ballance sites have been classified as a single 'Rural Industrial Zone' on the STDC Operative District Plan.

There are no sporting complexes, hospitals or commercial developments in the area surrounding KGTP. The closest identified offsite parties are a dwelling and a farm shed (approximately 220 metres and 180 metres, respectively from the northwest boundary of KGTP), in addition to the KPS and Ballance plants. Therefore, only the "Industrial" (i.e. the 5E-05/ year risk) and "Residential" (the 1E-06 /year risk) are considered in the QRA study.

### 7.1.2 Base Case Risk Contours

Figure 7-1 presents the Base Case overall LSIR contours at KGTP. The LSIR for fire and explosion events as well as toxic events are presented in Figure 7-2 and Figure 7-3, respectively.





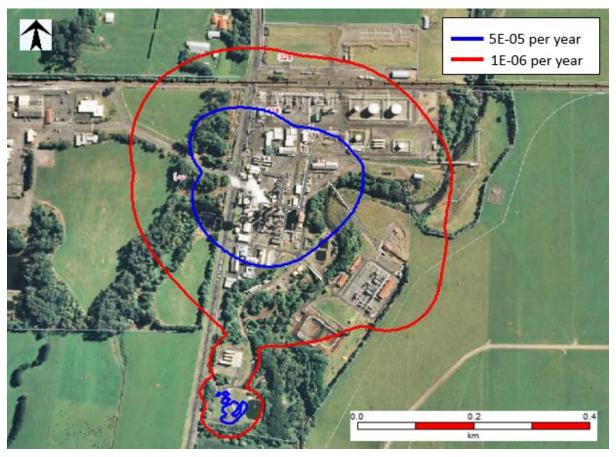


Figure 7-1: Base Case LSIR Contours at KGTP – All Events





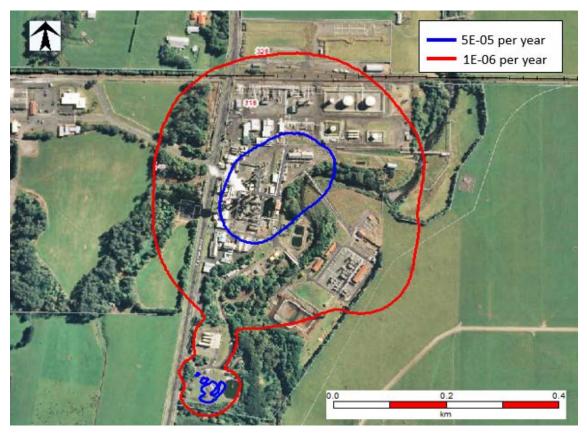


Figure 7-2: Base Case LSIR Contours at KGTP – Fire and Explosion Events





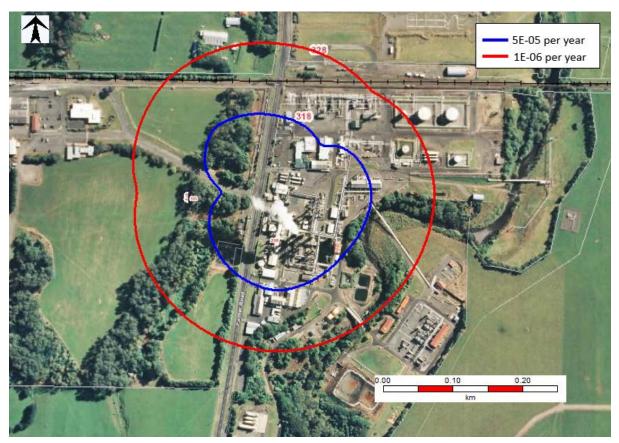


Figure 7-3: Base Case LSIR Contours at KGTP – Toxic Events

Overall risk levels are plotted between 5E-05 and 1E-06 per year, to allow for comparison against the NSW HIPAP 4 [Ref. 8] risk criteria documented in Table 7-2.

Overall LSIR	Risk Contour	Risk Criteria	Result Observation
5E-05 / year	Blue	Industrial 5E-05 / year risk contour should, as a target, be contained within the boundaries of the industrial site where applicable.	<ol> <li>5E-05 per year contour extends into the KPS site to the north but remains within the Todd Energy site boundary.</li> <li>The 5E-05 per year contour extends across Palmer Road and into the bushes at the west boundary of the Ballance site.</li> <li>The 5E-05 per year contour offsite impact is</li> </ol>
			mainly attributed to toxic events.
1E-06 / year	Red	Residential 1E-06 / year risk contour should not extend to residential, hotels, motels, tourist resorts	The 1E-06 per year contour extends onto the property of the closest neighbour north west of KGTP site but does not extend as far as the dwelling and farm buildings.

Table 7-2: Comparison with Fatality Risk Criteria (Base Case Overall LSIR)

The major risk contributors are identified and analysed in Section 7.2.





## 7.2 Major Risk Contributors

The major risk contributors are extracted from the risk model at selected risk points (indicated as the red dots) of interest, as shown in Figure 7-4.



Figure 7-4: Major Risk Contributors Points

### 7.2.1 Base Case Risk Contributor Analysis

The major risk contributing scenarios towards the risk points of interests for base case are presented in Table 7-3.

Risk Points	Release Source	Description	LSIR (per year)	Percentage of Risk Contribution (%)
A - Shed Area	KGT80_AMM_04_L_ 71mm	Ammonia liquid from Liquid Receivers via Liquid Sub-Coolers (E-826/896) and $CO_2$ Condenser (E- 804) to Oil Receiver (M-828)	5.21E-07	43.1%
	KGT80_AMM_03_L_ 71mm	Ammonia liquid from Ammonia Condensers (E- 895/825) to Liquid Receiver (F-803/F-823)	4.21E-07	34.8%
B - Ballance Site 1	KGT80_AMM_04_L_ 22mm	Ammonia liquid from Liquid Receivers via Liquid Sub-Coolers (E-826/896) and CO <sub>2</sub> Condenser (E- 804) to Oil Receiver (M-828)	2.97E-05	34.5%
	KGT80_AMM_03_L_ 22mm	Ammonia liquid from Ammonia Condensers (E- 895/825) to Liquid Receiver (F-803/F-823)	2.22E-05	25.8%

Table 7-3: Major Risk Contributors to Selected Locations for Base Case Assessment





Risk Points	Release Source	Description	LSIR (per year)	Percentage of Risk Contribution (%)
C -Ballance Site 2	KGT80_AMM_04_L_ 22mm	Ammonia liquid from Liquid Receivers via Liquid Sub-Coolers (E-826/896) and $CO_2$ Condenser (E-804) to Oil Receiver (M-828)	3.75E-05	35.5%
	KGT80_AMM_03_L_ 22mm	Ammonia liquid from Ammonia Condensers (E- 895/825) to Liquid Receiver (F-803/F-823)	2.47E-05	23.3%
D - KGTP Site East	KGT13_PGS_16_V_ 85mm	Product Gas from Gas Storage Compressor (D4- 0401) Discharge via Gas Storage Compressor Cooler (D2-0402) to Coalescer (D11-0417) Inlet	6.65E-07	33.5%
	KGT13_PGS_15_V_ 85mm	Product Gas to Gas Storage Compressors (D4- 0401/0402) Inlet	3.87E-07	19.5%
E – LPG Area	KGT01_TGS_10_V_ 212mm	Treated gas from Strippers via Gas/Gas Heat Exchangers (E-313-1/2) and Gas Chiller (E-313-3) to Low Temperature Separator (M-313) inlet	2.64E-07	23.5%
	KGT01_PGS_01_V_ 245mm	Product Gas header from Dehydration and Dew Point Unit to Product Gas Compressors Inlet header, domestic supply and sending Product Gas export to KPS and Whareroa (up to KPS/KGTP Site Boundary)	1.23E-07	11.0%

Based on the major risk contributors above, it can be shown that the shed area and Ballance site risk ranking points are mainly impacted by the ammonia release scenarios, in line with the LSIR toxic risk contours shown in Figure 7-3. The KGTP site east risk point is mainly impacted by the Gas Storage Compressor inlet and discharge line.

# 7.3 LPG Risk Analysis

The LPG storage and loadout facilities contribution to the overall plant risk for the base case are assessed in this section [Ref. 28]. The 1E-06 per year LSIR contour generated from only the LPG storage and loadout area is shown in Figure 7-5.







Figure 7-5: 1E-06 per year Risk Contour Contributed by the LPG Storage & Loadout Area Scenarios only

The major risk contributors to the LPG area (point E) have been identified at Section 7.2 above. The LPG storage and loadout equipment does not feature in the lists as they do not contribute significantly to the overall risk. This is largely due to the low failure frequencies from the LPG equipment and the relatively small inventories compared to the main process area. Each LPG vessel only contributes to about 1% of the risk at point E.

The main vessels, pipework and equipment from the LPG storage and loadout area that contribute to this risk contour are summarized in Table 7-4.

Description / Boundaries	Volume of Isolatable Section (m <sup>3</sup> )
Natural Gasoline Storage Tank (F-4033)	65.0
Natural Gasoline Loadout Facilities (including Load Out Pump (G-4033), Loadout Hose (T-4003))	0.1
Natural Gasoline Road Tanker	20 tonnes
Vapour Section of Propane Storage Vessel (F-4003)	61.7
Liquid Section of Propane Storage Vessel (F-4003)	51.3
Vapour Section of Propane Storage Vessel (F-4004)	123.4
Liquid Section of Propane Storage Vessel (F-4004)	106.6
Vapour Section of Butane Storage Vessel (F-4001)	14.7
Liquid Section of Butane Storage Vessel (F-4001)	51.3
Vapour Section of Butane Storage Vessel (F-4002)	68.6
Liquid Section of Butane Storage Vessel (F-4002)	44.5
Propane and Butane Loadout Pumps (G-4002/4024, G-4001)	0.5

Table 7-4: LPG Storage and Loadout Area Associated Scenarios





Description / Boundaries	Volume of Isolatable Section (m <sup>3</sup> )
LPG Loadout Arm (T-4002)	0.1
LPG Road Tanker	20 tonnes
LPG Loadout (Smart Hose to Isotainers)	0.1
New LPG Road Tanker (Isotainer)	12 tonnes
Ethyl Mercaptan Odorant Injection Pump (G-4011)	0.2
Ethyl Mercaptan Transportable Odorant Drums (F-4007-A/ B)	0.2

The loadout frequencies assumed for the loadout equipment at the LPG area are summarised in Table 7-5.

Description		Loading/Unloading	Load out Frequency (loadings/year)	Filling Time (hours/loading)
NGL Tankers		Hose	715 (20 T/Load)	2 hours
150	Tankers	Arm	1452 (20 T/Load)	2 hours
LPG	Isotainers	Hose	1.2 hours	
Ethyl MercaptanTransportable Odorant Drums (F-4007-A/B) contain Ethyl Mercaptan for odorising the LPG. 2 x 200L drums are swapped out approximately 12 times per year.				

#### Table 7-5: Loadout Frequencies





# 8 SENSITIVITY CASES

The two sensitivities cases considered in the KGTP QRA study, as detailed in Section 2.5 are:

- Sensitivity Case 1: 98% ESDV Success Probability; and
- Sensitivity Case 2: Future Operation.

This section presents results of the QRA sensitivity cases.

### 8.1 Case 1. ESDV Success Probability of 98%

The ESD systems are intended shutdown and isolate the process inventories to reduce damage or risk of escalation. In the event an ESDV failed to close, the expected outcome is additional flow or inventory from the process system adding to the release.

In the QRA Base Case assessment, the probability of successful detection and isolation is assumed to be 100%. However, it is acknowledged that there is potential for detection and isolation to fail. The Probability of Failure on Demand (PFD) of the ESDV can be referenced from industry sources as follow:

- 0.001 0.01 per demand depending on the types of the ESD system (TNO Purple Book [Ref. 10]); and
- In the order of magnitude of 10<sup>-2</sup> per demand (CMPT Quantitative Risk Assessment for offshore installation [Ref. 21]).

For the purpose of the Sensitive Case 1 assessment, ESDV success probability is assumed to be 98%, and the corresponding ESDV failure probability is 2%.

### 8.1.1 Isolatable Inventories for ESDV Failure Consideration

In Sensitivity Case 1, the inventory from the next connecting isolatable section (or the largest inventory if connecting with multiple isolatable sections) are added to the inventory from each isolatable section for the ESDV failure. The connecting isolatable sections have been identified from the P&IDs and are given in Table 8-1.

Isolatable Section	Description (m <sup>3</sup> ) Isola		Connecting Isolatable Section	Volume of Connecting Isolatable Section <sup>Note 1</sup> (m <sup>3</sup> )		Total Volume (m³)		
		Vapour	Liquid		Vapour	Liquid	Vapour	Liquid
KGT01	Raw gas and Maui gas lines, Dehydration and dewpoint unit, LPG production unit, Product gas lines, Utilities	233.0	56.3	KGT11 – Vapour; KGT04 - Liquid	41.3	4.0	274.2	60.3
KGT02	CO <sub>2</sub> removal (Train 1)	36.2	-	KGT01	233.0	-	269.2	-
KGT03	CO <sub>2</sub> removal (Train 2)	36.0	-	KGT01	233.0	-	269.0	-
KGT04	Mixed LPG - High Temperature Separator (M-307) and Wash Water Coalescer (M-302)	2.4	4.0	KGT01	233.0	56.3	235.4	60.3
KGT11	Mixed gas export from Product Gas Compressors (C-903-2/3/5) discharge	41.3	-	KGT01	233.0	-	274.2	-

Table 8-1: Identification of the Connecting Isolatable Sections and Inventories





Isolatable Section	Description	Volume of Isolatable Section (m <sup>3</sup> )		Connecting Isolatable Section	Conne	e Section	Total Volume (m³)	
		Vapour	Liquid		Vapour	Liquid	Vapour	Liquid
	header to 100/200 Pipelines							
KGT13	Product gas export from Gas Storage Compressors (D4-0401/0402) to Gas Storage/070 Pipeline	23.5	-	KGT01	233.0	-	256.5	-
KGT32	NGL export from LPG production unit to KGTP/KPS boundary	-	0.4	KGT01	-	56.3	-	56.8
KGT33	NGL export from LPG production unit to Storage	-	4.7	KGT34	-	65.0	-	69.7
KGT34	NGL Storage Tank (F- 4033)	-	65.0	KGT33	-	4.7	-	69.7
KGT35	NGL Loadout Pump (G- 4033)	-	0.1	KGT34	-	65.0	-	65.1
KGT36	NGL Loadout System	-	0.1	KGT35		0.1	-	0.2
KGT37	Propane export from LPG production unit to Storage	-	2.5	KGT01	-	56.3	-	58.9
KGT39	Propane Storage Vessel (F-4003)	61.7	51.3	KGT37	-	2.5	61.7	53.9
KGT40	Propane Storage Vessel (F-4004)	123.4	106.6	KGT37	-	2.5	123.4	109.1
KGT41	Butane export from LPG production unit to Storage	-	2.6	KGT01	-	56.3	-	58.9
KGT43	Butane Storage Vessel (F- 4001)	14.7	51.3	KGT41	-	2.6	14.7	53.8
KGT44	Butane Storage Vessel (F- 4002)	68.6	44.5	KGT41	-	2.6	68.6	47.0
KGT45	Product Propane Loadout System	-	0.5	KGT40	-	106.6	-	107.1
KGT46	Product Butane Loadout System	-	0.5	KGT43	-	51.3	-	51.8
KGT47	Product LPG Loadout System	-	0.1	KGT45	-	0.5	-	0.6
KGT50	Odorant (Ethyl mercaptan) Injection System for LPG loadout	-	0.2	-	-	-	-	0.2
KGT51	Odorant (t-Butyl mercaptan) Injection System for Domestic	-	0.1	-	-	-	-	0.1





Isolatable Section	Description	Volum Isolatable (m	Section	Connecting Isolatable Section	Volume of Connecting Isolatable Section <sup>Note 1</sup> (m <sup>3</sup> )		Total Volume (m³)	
		Vapour	Liquid		Vapour	Liquid	Vapour	Liquid
KGT52	Odorant (t-Butyl mercaptan) Injection System for Gas Export Line	-	19.0	-	-	-	-	19.0
KGT55	Methanol Injection System	-	6.5	-	-	-	-	6.5
KGT70	Propane Refrigeration System	36.4	25.2	-	-	-	36.4	25.2
KGT80	CO2 Removal Unit – Ammonia System	3.3	4.9	-	-	-	3.3	4.9
KGT90	CO2 Removal Unit – Ammonia System	45.6	223.0	-	-	-	45.6	223.0

Notes:

1. For modelling purposes, only the inventory within the same phase are added, e.g. KGT02 contains vapour phase only, and is connected to KGT01 which contains both vapour and liquid phase, only the vapour inventory from KGT01 is added to KGT02.

# 8.1.2 Sensitivity Case 1 Release Frequencies

There are no changes in estimated release frequencies for the node sections in Sensitivity Case 1. Release frequencies assessment presented in Section 6.1 is applicable to Sensitivity Case 1.





## 8.1.3 Sensitivity Case 1 Risk Contours

Figure 8-1 presents the LSIR contour for KGTP Sensitivity Case 1.

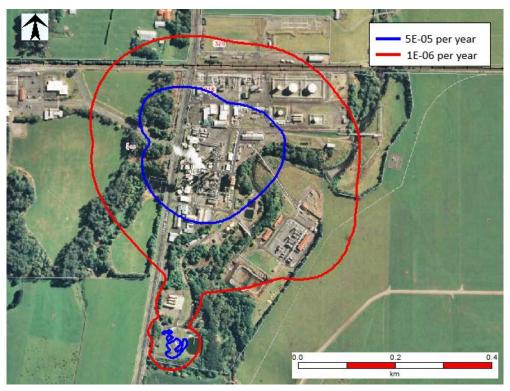


Figure 8-1: Sensitivity Case 1 LSIR Contours at KGTP

The 5E-05 per year and 1E-06 per year risk contours for Sensitivity Case 1 are shown to be similar to the Base Case risk contours (Figure 7-1). It can be concluded that the outcome of assessment against HIPAP 4 for Sensitivity Case 1 is same as that captured in the Base Case. Conclusions made in Table 7-2 are applicable for Sensitivity Case 1 as well.

The insignificant differences in risk contours for Sensitivity Case 1 when compared to Base Case is most likely due to:

- In most modelling cases, especially gas releases, it is expected that the consequence effects would have reached the steady state condition before the inventory depletes. Hence the additional inventory may lead to a prolonged fire event, but not increase the magnitude of the consequence; and
- The ESDV failure probability change is only 2%, therefore the frequencies of hazardous events (fire explosion or toxic) associated with increased consequences (if any) are not expected to be apparent in the risk contours.

## 8.2 Case 2. Future Operating Case

KGTP future operation at maximum throughput operation (29 Sm3/s) is considered in the QRA as Sensitivity Case 2.

### 8.2.1 Sensitivity Case 2 Release Scenarios

The additional release scenarios considered for the Sensitivity Case 2 assessment and the corresponding operating conditions are presented in Table 8-2. The volume of some isolatable sections for existing (Base Case) scenarios are increased due to maximum throughput consideration in Sensitivity Case 2.





## Table 8-2: Release Scenarios and Operating Conditions (Sensitivity 2)

Node	Description / Boundaries	Stream No.	T (degC)	P (barg)	Max Pipe / Hose Diameter (mm)	Pipe / Hose Length (m)	Volume of Isolatable Section (m <sup>3</sup> )
	CO <sub>2</sub> Removal		1				
KGT05_RGS_07_V	Raw gas from Raw Gas header from HV-105-3 via Gas/Gas Heat Exchanger (E-101-3/2) to $CO_2$ absorber tower (D-101-3) inlet (Benfield Train 3)	K101	15	40	300	15	33.0
KGT05_TGS_16_V	Treated gas from top of $CO_2$ absorber tower (D-101-3) via Gas/Gas Heat Exchanger (E-101-3/2) and Gas Separator (M-101-3) adjoining with the inlet line to Strippers (D-201-3/4) in Dehydration and Dewpoint Control Unit (Benfield Train 3)	K102	42	40	300	15	33.0
	Dehydration and Dewpoin	t Control					
KGT01_TGS_11_V	Treated gas from Strippers via Gas/Gas Heat Exchangers (E-303-1/2) and Gas Chiller (E-303-3) to 3 Phase Low Temperature Separator (M-306) inlet (No.1 Chilling System)	К203	42	40	200	43	271.6
KGT01_PGS_03_V	Product gas from top of 3 Phase Low Temperature Separator (M-306) via Gas/Gas Heat Exchanger (E-303-1/2) to PV-338 adjoining with Product Gas header (No.1 Chilling System)	K205	12	40	150	15	271.6
KGT01_MPG_02_L	Mixed LPG from bottom of 3 Phase Low Temperature Separator (M-306) to FV- 381 on the line adjoining with inlet of Gas/Liquid Heat Exchanger (E-303-4) (No.1 Chilling System)	К204	12	40	100	15	56.3
	Utilities and Cogen L	Jnit					
KGT01_PGS_22_V	Product gas to Boilers (B-901-1/2)	K501	15	40	150	50	271.6
	LPG Production Facility - Stabilise	er, De-Ethani	ser	1			
KGT01_MPG_13_L	Mixed LPG from XSV-332 on outlet line of Wash Water Coalescer (M-302) in Dehydration unit to Stabiliser (D-420-1) inlet (LPG Production Train 1)	К401	12	30	150	144	56.3
KGT01_STT_01_V	Stabiliser (D-420-1) Top Vapour via Stabiliser OVHD Scrubber (M-420) to XSV- 420 on inlet line to Suction Scrubber (M-421) (LPG Production Train 1)	К408	20	30	80	15	271.6
KGT01_PGS_10_V	Product gas from top of Stabiliser OVHD Scrubber (M-421) to Stabiliser OVHD Compressor (C-420-1/2) suction (LPG Production Train 1) (C-420-1 is on standby)	K408	20	30	100	90	271.6
KGT01_PGS_11_V	Product gas from Stabiliser OVHD Compressor (C-420-2) discharge via Stabiliser OVHD Compressor Cooler (E-420-5) to Product gas header (LPG Production Train 1)	K408	20	30	100	15	271.6
KGT01_STB_01_L	Stabiliser (D-420-1) Bottom Liquid to/from Stabiliser Reboiler (E-422-1) and to De-Propaniser Feed Surge Drum (F-420-3) inlet (LPG Production Train 1)	К402	100	30	150	15	56.3
	LPG Production Facility - De-	Propaniser					
KGT01_DPT_01_V	De-Propaniser (D-430-1) Top Vapour via De-Propaniser Condenser (E-430-1) to De-Propaniser Reflux Drum (F-430-1) (LPG Production Train 1)	К403	20	14	150	15	271.6
KGT01_DPX_01_L	Reflux from De-Propaniser Reflux Drum (F-430-1) via De-Propaniser Reflux Pumps (G-430-1/2) to De-Propaniser (D-430-1) (LPG Production Train 1) (G-430-2 is on stand-by.)	K403	20	14	100	15	56.3
KGT01_PC3_01_L	Product propane from De-Propaniser Reflux Pump (G-430-1) via Propane Product Cooler (E-4001-1) adjoining with export line to storages (LPG Production Train 1)	К403	20	14	50	22	56.3
KGT01_DPB_01_L	De-Propaniser (D-430-1) Bottom Liquid to/from De-Propaniser Reboiler (E-432- 1) and to De-Butaniser (D-440-1/2) (LPG Production Train 1)	К404	105	14	150	44	56.3
	LPG Production Facility	- De-C4					
KGT01_DBT_01_V	De-Butaniser (D-440-1) Top Vapour via De-Butaniser Condenser (E-440-1) to De- Butaniser Reflux Drum (F-440-1) (LPG Production Train 1)	К405	20	7	100	15	271.6
KGT01_DBX_01_L	Reflux from De-Butaniser Reflux Drum (F-440-1) via De-Butaniser Reflux Pumps (G-440-1/2) to De-Butaniser (D-440-1) (LPG Production Train 1) (G-440-2 is on standby)	К405	20	7	80	15	56.3
KGT01_DBB_01_L	De-Butaniser (D-440-1) Bottom Liquid to /from De-Butaniser Reboiler (E-442-1) (LPG Production Train 1)	К406	115	7	150	15	56.3
KGT01_PC4_12_L	Product Butane from HV-450-1/2 on Debutaniser Reflux Pumps Discharge via Butane Cooler (E-450) adjoining with Product Propane at 60/40 Condensing Tank (M-430) inlet	K405	20	7	80	41	56.3
KGT01_PC3_13_L	Product Propane from Propane Product Coolers (E-4001-1/2) adjoining with Product Butane at 60/40 Condensing Tank (M-430) inlet	К403	20	14	50	15	56.3
KGT01_LPG_04_L	LPG product 60/40 via 60/40 Condensing Tank (M-430) to XSV-434 on KPS export line	K808	20	10.5	50	232	56.3
	Propane Refrigeration S	System					
KGT70_REF_06_L	Propane refrigerant Gas Chiller (E-303-3)	K302	-34	1	150	64	25.2
	CO <sub>2</sub> Recovery - CO	2					





The modified isolatable section volume used in the Sensitivity Case 2 modelling are summarised in Table 8-3.

Isolatable Section	Description		isolatable Base Case	Volume of Isolatable Section (m <sup>3</sup> ) Sensitivity Case 2		
		Vapour	Liquid	Vapour	Liquid	
KGT01	Raw gas and Maui gas lines, Dehydration and dewpoint unit, LPG production unit, Product gas lines, Utilities	233.0	56.3	271.6	84.8	
KGT05	CO <sub>2</sub> removal (Train 3)	0 Note 1	0 Note 1	33.0	0	
KGT70	Propane Refrigeration System	36.4	25.2	36.4	28.4	
KGT90	CO2 Removal Unit – Ammonia System	45.6	223.0	48.5	223.0	

Table 8-3: Modified Volume of Isolatable Sections

Note 1: Only considered for Sensitivity Case 2 (for future operation).

## 8.2.2 Sensitivity Case 2 Leak Frequencies

The estimated release frequencies summary of each KGTP unit considered in Sensitivity Case 2 are presented in Table 8-4. The detail breakdown of release frequencies for each node sections are provided in Appendix 4.

	Sensitivity 2 Release Frequencies (per year) Note 1							
Node Section	1 - 3 mm (2 mm)	3 - 10 mm (6 mm)	10 - 50 mm (22 mm)	50 - 150 mm (85 mm)	> 150 mm (Rupture)	Total	% Contributi on	
Raw Gas and Maui Gas Lines	1.50E-02	6.58E-03	3.50E-03	6.07E-04	1.03E-04	2.58E-02	2.4%	
CO <sub>2</sub> Removal	1.28E-02	5.82E-03	3.20E-03	6.10E-04	1.17E-04	2.25E-02	2.1%	
Dehydration and Dewpoint Control	3.30E-02	1.45E-02	7.54E-03	1.71E-03	2.69E-04	5.70E-02	5.4%	
Product Gas Lines and Compressors	6.28E-02	2.75E-02	1.39E-02	2.96E-03	4.61E-04	1.08E-01	10.2%	
Pigging	3.58E-06	1.85E-06	1.03E-06	2.55E-07	1.16E-07	6.83E-06	<0.1%	
Utilities and Cogen Unit	5.30E-02	2.18E-02	9.99E-03	2.03E-03	9.45E-05	8.70E-02	8.2%	
LPG Production Facility - Stabiliser, De-C2	4.99E-02	2.16E-02	1.06E-02	2.81E-03	5.84E-05	8.49E-02	8.0%	
LPG Production Facility - De-C3	3.13E-02	1.26E-02	6.06E-03	1.23E-03	3.30E-05	5.13E-02	4.8%	
LPG Production Facility - De-C4	3.96E-02	1.59E-02	7.52E-03	1.63E-03	2.86E-05	6.47E-02	6.1%	
LPG Production Facility - Product Export and Loadout	2.33E-02	9.14E-02	3.40E-03	6.87E-04	8.37E-03	1.27E-01	12.0%	

Table 8-4: Release Frequencies Summary for KGTP Units (Sensitivity 2)





	Sensitivity 2 Release Frequencies (per year) Note 1							
Node Section	1 - 3 mm (2 mm)	3 - 10 mm (6 mm)	10 - 50 mm (22 mm)	50 - 150 mm (85 mm)	> 150 mm (Rupture)	Total	% Contributi on	
Propane Refrigeration System	3.99E-02	1.73E-02	8.06E-03	1.73E-03	3.22E-04	6.73E-02	6.3%	
Mercaptans and Methanol	1.95E-02	2.01E-02	3.85E-03	2.05E-03	1.21E-03	4.68E-02	4.4%	
CO <sub>2</sub> Recovery - Ammonia	7.07E-02	2.81E-02	1.14E-02	2.90E-03	2.50E-04	1.13E-01	10.7%	
CO <sub>2</sub> Recovery - CO <sub>2</sub>	8.06E-02	9.70E-02	1.56E-02	4.22E-03	6.81E-03	2.04E-01	19.3%	
Total	5.31E-01	3.80E-01	1.05E-01	2.52E-02	1.81E-02	1.06E+00	100.0%	
% Contribution	50.2%	35.9%	9.9%	2.4%	1.7%	100.0%	-	

Notes:

1. Release frequencies estimated has considered the operating factor of equipment.

The Sensitivity Case 2 scenarios have higher total release frequencies of 1.1 per annum, equivalent to one leak every 0.9 year. There is approximately 6% increase in total release frequencies for Sensitivity Case 2. This can be attributed to Sensitivity Case 2 considered additional equipment in operation. Similarly, to the Base Case, 50% of the leak frequencies are contributed from the "1 - 3 mm" hole sizes range.





## 8.2.3 Sensitivity Case 2 Risk Contours

Figure 8-2 presents the LSIR contour for Sensitivity Case 2.

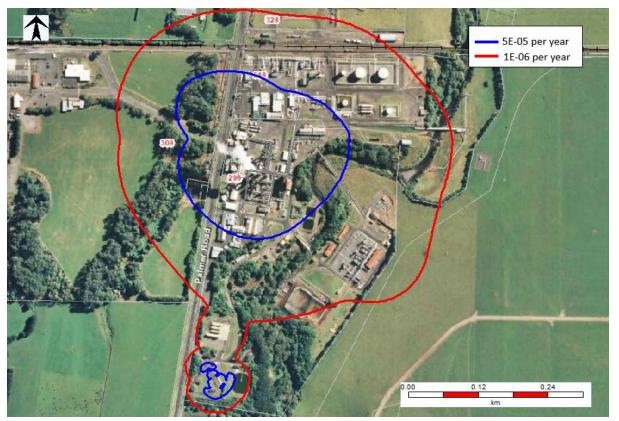


Figure 8-2: Sensitivity Case 2 LSIR Contours at KGTP

When compared to the Base Case, it can be seen that the Sensitivity Case 2 risk contours of 5E-05 per year and 1E-06 per year are slightly larger. This is particularly apparent at the LPG/NGL loading area, which is due to an increased in loading frequencies for both the NGL and LPG scenarios. The slight increase in 5E-05 per year and 1E-06 per year contours however does not change the assessment conclusions made against HIPAP 4 criteria. Conclusions made in Table 7-2 are applicable to Sensitivity Case 2 as well. Although there are additional equipment and inventories considered in Sensitivity Case 2, the increase in risk levels are not significant. This is most likely due to:

- The additional nodes/sections considered in Sensitivity Case 2 only formed a small part of the overall KGTP hazardous nodes/sections. There is approximately 18% increase in total release frequency for Sensitivity Case 2 as compared to the Base Case, with 50% of the increase is from the "1-3 mm" leak category; and
- In most modelling cases, especially gas releases, it is expected that the consequence effects would have reached the steady state condition before the inventory depletes. Hence the additional inventory may lead to a prolonged fire event, but not increase the magnitude of the consequence.





# 8.2.4 Sensitivity Case 2 Risk Contributor Analysis

The major risk contributing scenarios towards the risk points of interests for Sensitivity Case 2 (which has the worst case risk results) are presented in Table 8-5.

Risk Points	Release Source	Description	LSIR (per year)	Percentage of Risk Contribution
A - Shed	KGT80_AMM_04_L_ 71mm	Ammonia liquid from Liquid Receivers via Liquid Sub-Coolers (E-826/896) and $CO_2$ Condenser (E-804) to Oil Receiver (M-828)	5.22E-07	41.6%
	KGT80_AMM_03_L_ 71mm	Ammonia liquid from Ammonia Condensers (E- 895/825) to Liquid Receiver (F-803/F-823)	4.22E-07	33.6%
B - Ballance Site 1	KGT80_AMM_04_L_ 22mm	Ammonia liquid from Liquid Receivers via Liquid Sub-Coolers (E-826/896) and $CO_2$ Condenser (E-804) to Oil Receiver (M-828)	2.97E-05	34.1%
	KGT80_AMM_03_L_ 22mm	Ammonia liquid from Ammonia Condensers (E- 895/825) to Liquid Receiver (F-803/F-823)	2.22E-05	25.5%
C - Ballance Site 2	KGT80_AMM_04_L_ 22mm	Ammonia liquid from Liquid Receivers via Liquid Sub-Coolers (E-826/896) and $CO_2$ Condenser (E-804) to Oil Receiver (M-828)	3.75E-05	34.7%
	KGT80_AMM_03_L_ 22mm	Ammonia liquid from Ammonia Condensers (E- 895/825) to Liquid Receiver (F-803/F-823)	2.47E-05	22.8%
D - KGTP Site East	KGT13_PGS_16_V_ 85mm	Product Gas from Gas Storage Compressor (D4- 0401) Discharge via Gas Storage Compressor Cooler (D2-0402) to Coalescer (D11-0417) inlet	6.65E-07	32.9%
	KGT13_PGS_15_V_ 85mm	Product Gas to Gas Storage Compressors (D4- 0401/0402) Inlet (D4-0402 is on standby)	3.87E-07	19.1%
E- LPG Area	KGT01_TGS_10_V_ 212mm	Treated gas from Strippers via Gas/Gas Heat Exchangers (E-313-1/2) and Gas Chiller (E-313-3) to Low Temperature Separator (M-313) inlet	2.84E-07	20.4%
	KGT01_PGS_01_V_ 245mm	Product Gas header from Dehydration and Dew Point Unit to Product Gas Compressors Inlet header, domestic supply and sending Product Gas export to KPS and Whareroa (up to KPS/KGTP Site Boundary)	1.32E-07	9.5%

Table 8-5: Major Risk Contributors to Selected Locations for Sensitivity Case 2 Assessment

The major risk contributors for Sensitivity Case 2 are consistent with the major risk contributors for Base Case, with just slight differences on the fraction of risk contribution.





# 9 POTENTIAL CUMULATIVE RISK FROM KPS AND KGTP

The KPS plant, which is located to the north of the KGTP plant, is also under Todd's ownership / control. Risk from KPS was assessed and presented in the KPS QRA report [Ref. 29]. That report was commissioned for the South Taranaki District Plan Environment Court process.

Consistent assumptions and methodologies have been adopted for both QRAs, which followed the Todd Energy QRA Methodology Guideline [Ref. 2]. The KPS base case LSIR contour is shown in Figure 9-1.

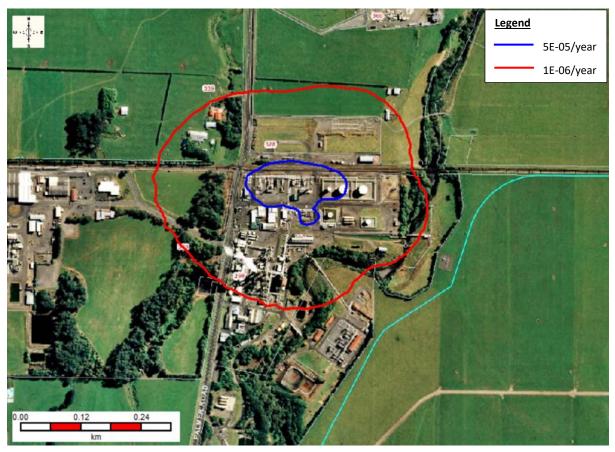


Figure 9-1: KPS LSIR Contour

The KPS QRA was completed using DNV Safeti software version 6.7 (formerly known as Phast Risk). Newer versions of the software have since been released, and one of the improvements made allows more accurate modelling of vapour dispersion distances, especially for large releases. The older version (e.g. Phast Risk 6.7) generally produced more conservative dispersion distances.

The plant has also been modified since the KPS QRA was finalised and accepted by the South Taranaki District Council in July 2020. The stabilizer replacement project, including additional isolation valves to reduce the inventory for some isolatable sections. This was considered in the KPS QRA (as sensitivity case 3) and has led to further risk reduction.

The KPS model was then upgraded to Safeti version 8.22 and combined with the KGTP Safeti model to generate the integrated QRA model. Releases from both plants and the interaction between them (e.g. a flammable vapour cloud from one plant entering the congested area at another plant) were taken into consideration when run as a single model to produce the cumulative risk.

The cumulative risk contours considering risks from both KPS and KGTP are presented in Figure 9-2.





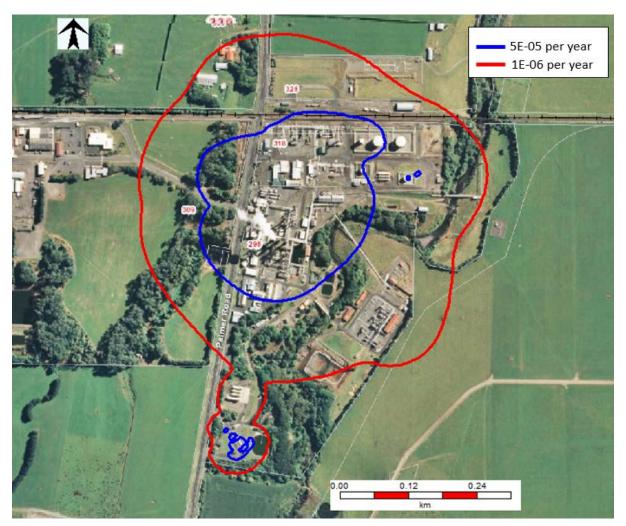


Figure 9-2: KPS and KGTP Integrated LSIR Contours

The risk contour for the cumulative risk does not extend further offsite in any direction, than the individual plant contours. This shows that there are no noticeable potential synergistic or cumulative offsite risks from Todd owned and operated plant. The risk assessment against the HIPAP4 criteria is as presented in Table 9-1.

Table 9-1: Risk Assessment Against HIPAP4 Criteria for the Cumu	lative Risk
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Overall LSIR	Risk Contour	Risk Criteria	Observations
5E-05 / year	Blue	Industrial 5E-05 / year risk contour should, as a target, be contained within the boundaries of the industrial site where applicable.	<ol> <li>The 5E-05 per year risk contour remains mostly within the Todd Energy site boundary, with the exception at the west boundary.</li> <li>The 5E-05 per year contour extends across Palmer Road and into the bushes at the west boundary of the Ballance site.</li> </ol>
1Е-06 / year	Red	Residential 1E-06 / year risk contour should not extend to residential, hotels, motels, tourist resorts	<ol> <li>The 1E-06 per year risk contour extends onto the dwelling and farm building in the immediate vicinity of KPS to the northwest.</li> </ol>





# 10 CONCLUSIONS

QUANTITATIVE RISK ASSESSMENT REPORT

A quantitative risk assessment (QRA) was carried out to assess the risk levels at Kapuni Gas Treatment Plant (KGTP) due to fire, explosion and toxic hazards.

The assessment considers risks from KGTP for the following cases:

- Base Case all facilities currently in operation;
- Sensitivity Case 1 all facilities currently in operation with reduced ESDV success rate of 98% instead of 100%; and
- Sensitivity Case 2 all facilities currently in operations including standby and mothballed facilities which might be brought back to operation in the future.

The overall risk levels are compared to the NSW HIPAP 4 [Ref. 8] risk criteria. The main findings of the QRA for all 3 cases are summarised in Table 10-1.

Case	Main Findings
Base Case	1. The 5E-05 per year contour extends into the KPS site to the north but remains within the Todd Energy site boundary.
	<ol> <li>The 5E-05 per year contour extends across Palmer Road and into the bushes at the west boundary of the Ballance site.</li> </ol>
	3. The 1E-06 per year contour extends onto the property of the neighbour to the northwest (approximately 180m NW of KGTP northern boundary) but does not extend as far as the dwelling and farm buildings.
	4. The main risk contributors to the shed area are ammonia toxic events from the 71 mm leaks from the Liquid Receivers (KGT80_AMM_04_L_71mm) and Ammonia Condensers (KGT80_AMM_03_L_71mm) within the CO2 Recovery Unit at approximately 15°C and 15 barg.
	<ol> <li>The main risk contributors to the Ballance site bushes are ammonia toxic events from the 22 mm leaks from the Liquid Receivers (KGT80_AMM_04_L_22mm) and Ammonia Condensers (KGT80_AMM_03_L_22mm) within the CO2 Recovery Unit at approximately 15°C and 15 barg.</li> </ol>
	6. The main risk contributors to the rural land area to the east of the plant are Product Gas jet fire events from the 85 mm leaks from the Product Gas from the Gas Storage Compressor (D4-0401) to Coalescer (KGT13_PGS_16_V_85mm), and Product Gas feeding to the Gas Storage Compressor (KGT13_PGS_15_V_85mm) within the Product Gas Lines and Compressors unit (at approximately 15°C and 40 barg).





Case	Main Findings
Sensitivity Case 1 – ESDV Success Probability of 98%	1. There are no significant changes to the risk contours with modification of the ESDV success probability. The assessment made against the HIPAP 4 criteria remains the same as per the base case.
	2. The similar risk contours finding is due to:
	<ul> <li>The ESDV failure probability change is only 2%, therefore the frequencies of hazardous events (fire explosion or toxic) associated with increased consequences (if any) are not expected to be apparent in the risk contours; and</li> </ul>
	<ul> <li>In most modelling cases, especially gas releases, it is expected that the consequence effects would have reached the steady state condition before the inventory depletes. Hence the additional inventory may lead to a prolonged fire event, but not increase the magnitude of the consequence.</li> </ul>
Sensitivity Case 2 – Future Operations	<ol> <li>The risk contours for Sensitivity Case 2 risk contours is slightly larger when compared to the Base Case risk contours, however the contour increase is relatively small. The assessment made against the HIPAP 4 criteria remains the same as per the base case.</li> </ol>
	2. The slight increase in risk contours is due to:
	<ul> <li>The additional nodes/sections considered in Sensitivity Case 2 only formed a small part of the overall KGTP hazardous nodes/sections. There is approximately 18% increase in total release frequency for Sensitivity Case 2 as compared to the Base Case, with 50% of the increase is from the "1-3 mm" leak category; and</li> </ul>
	<ul> <li>In most modelling cases, especially gas releases, it is expected that the consequence effects would have reached the steady state condition before the inventory depletes. Hence the additional inventory may lead to a prolonged fire event, but not increase the magnitude of the consequence.</li> </ul>





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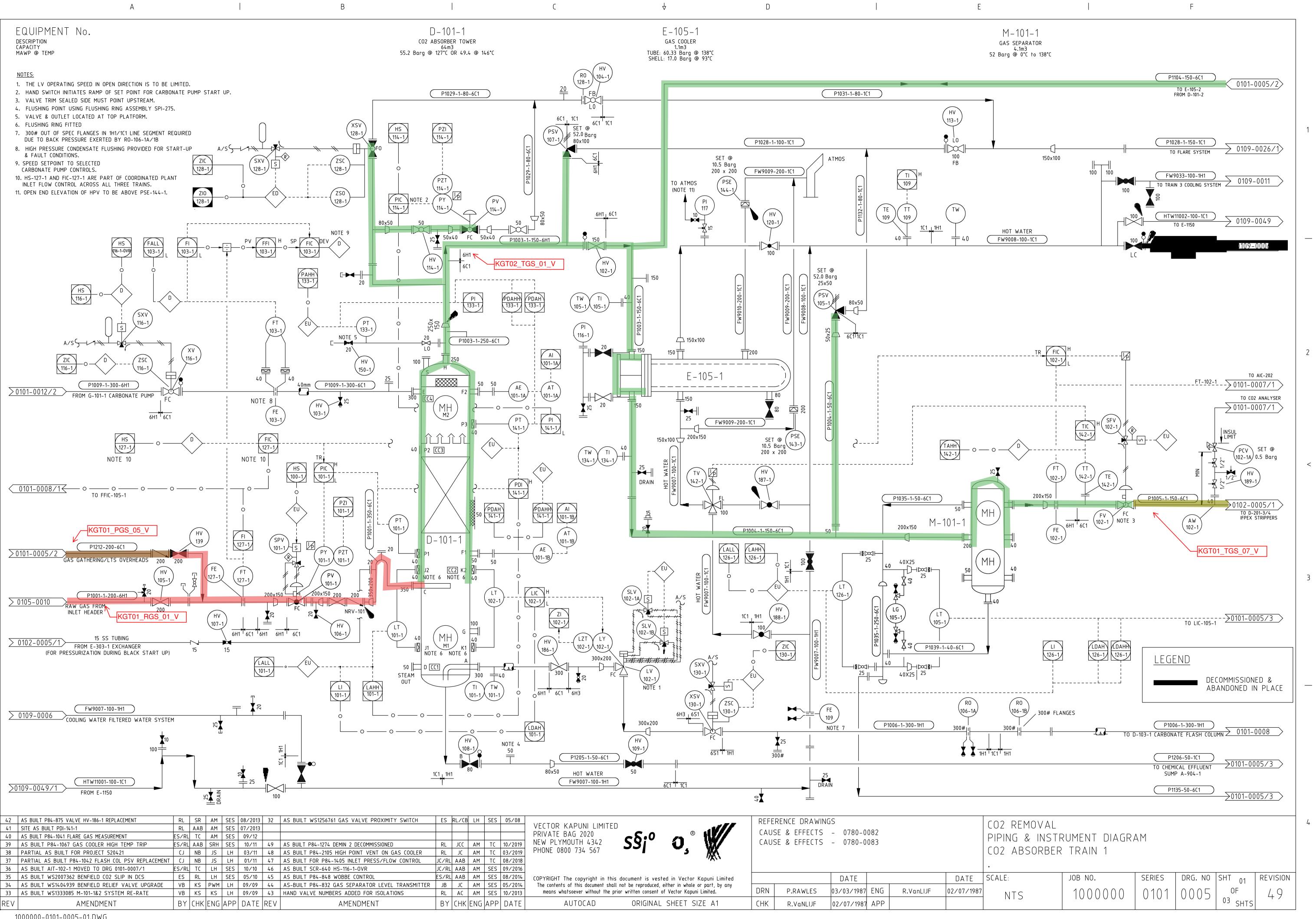


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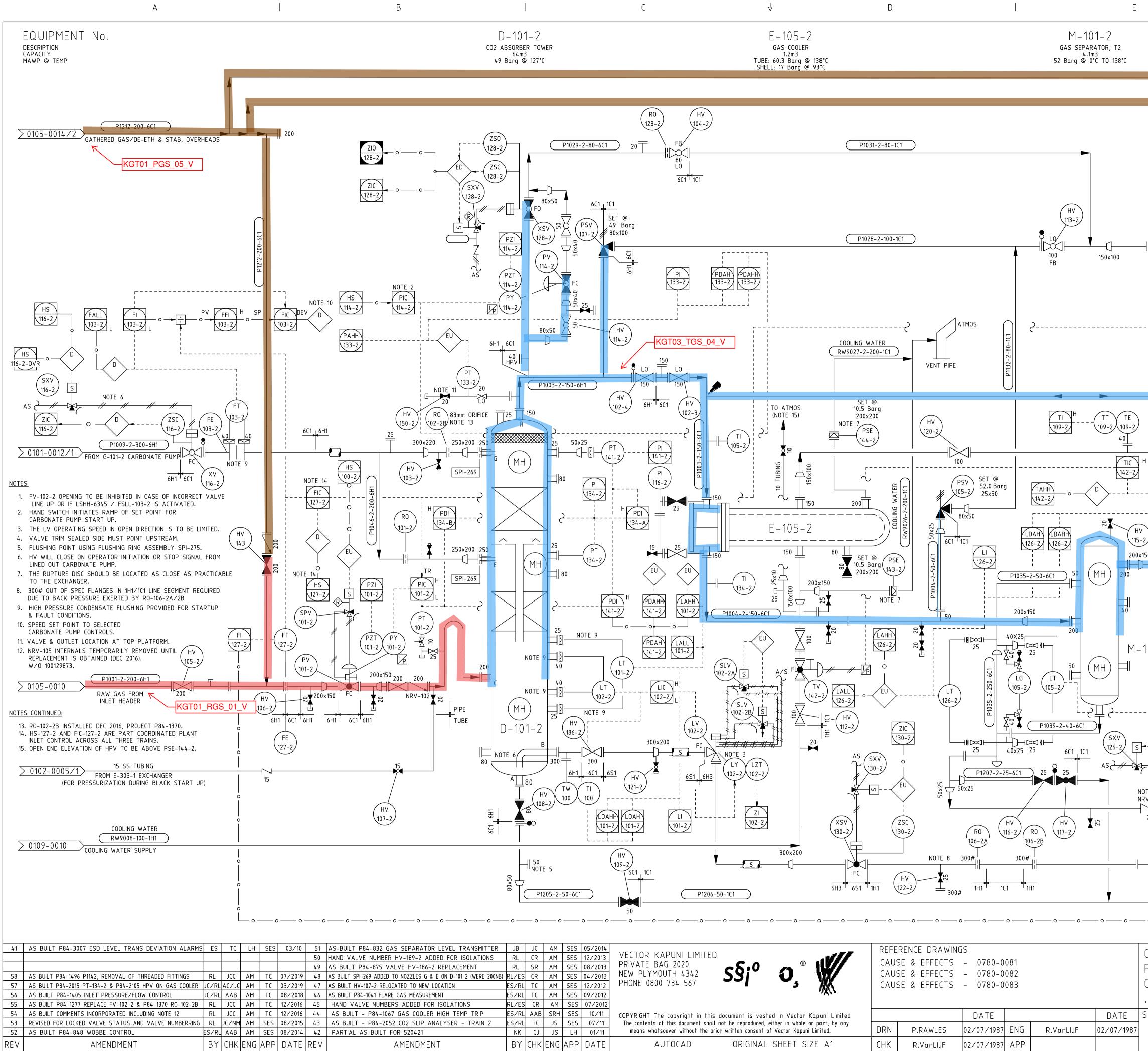


Appendix 1. Sectionalised P&IDs



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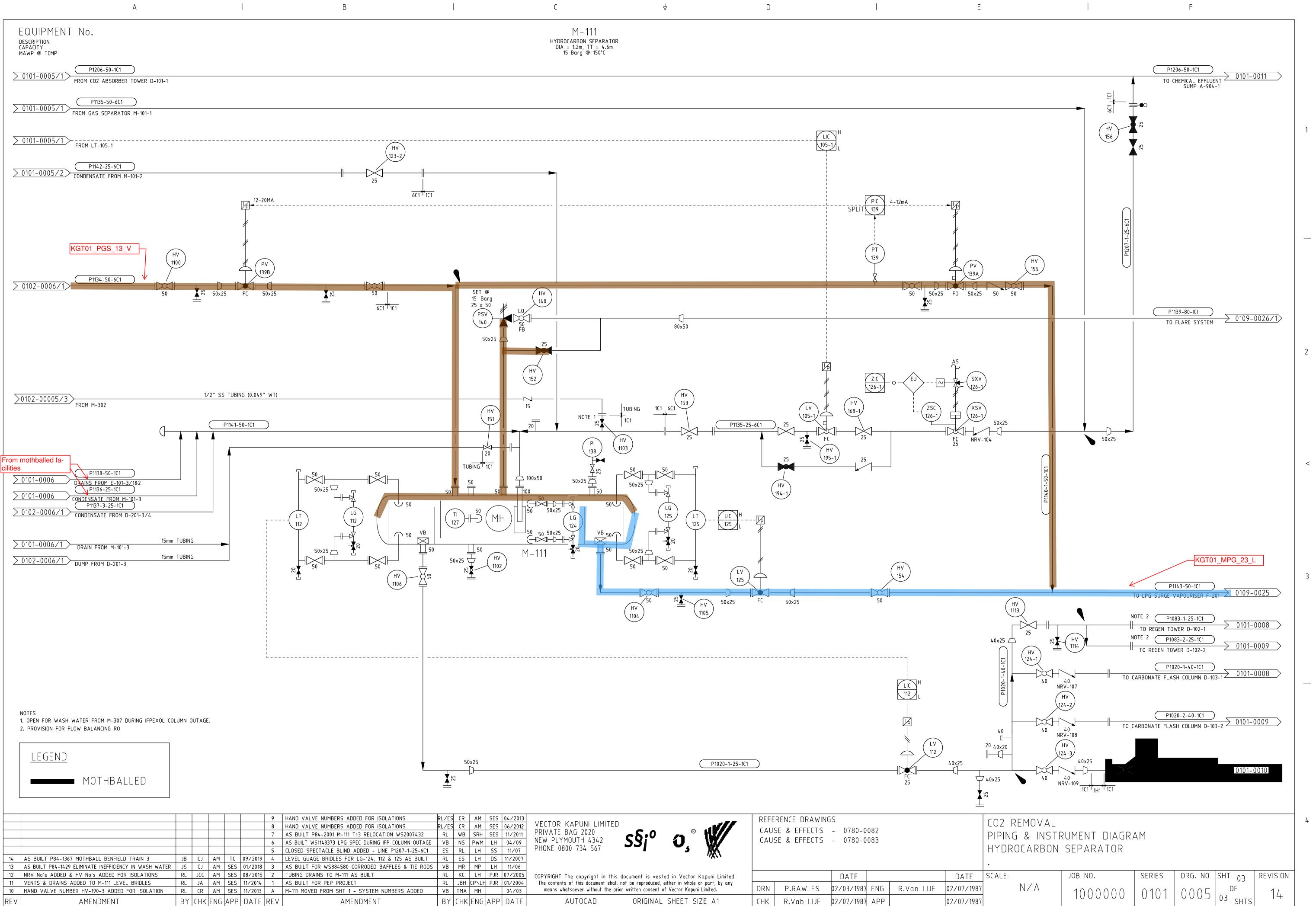
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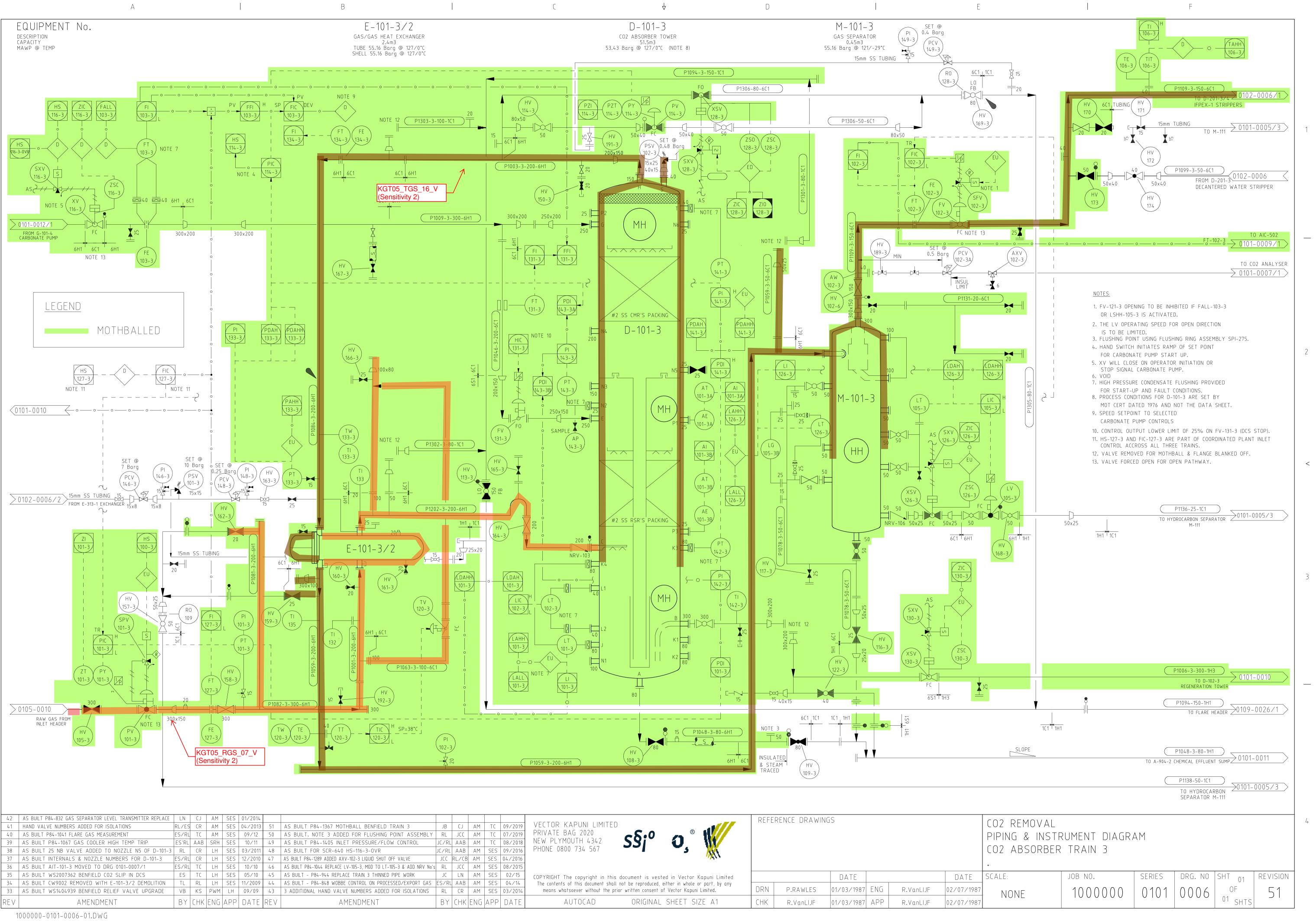
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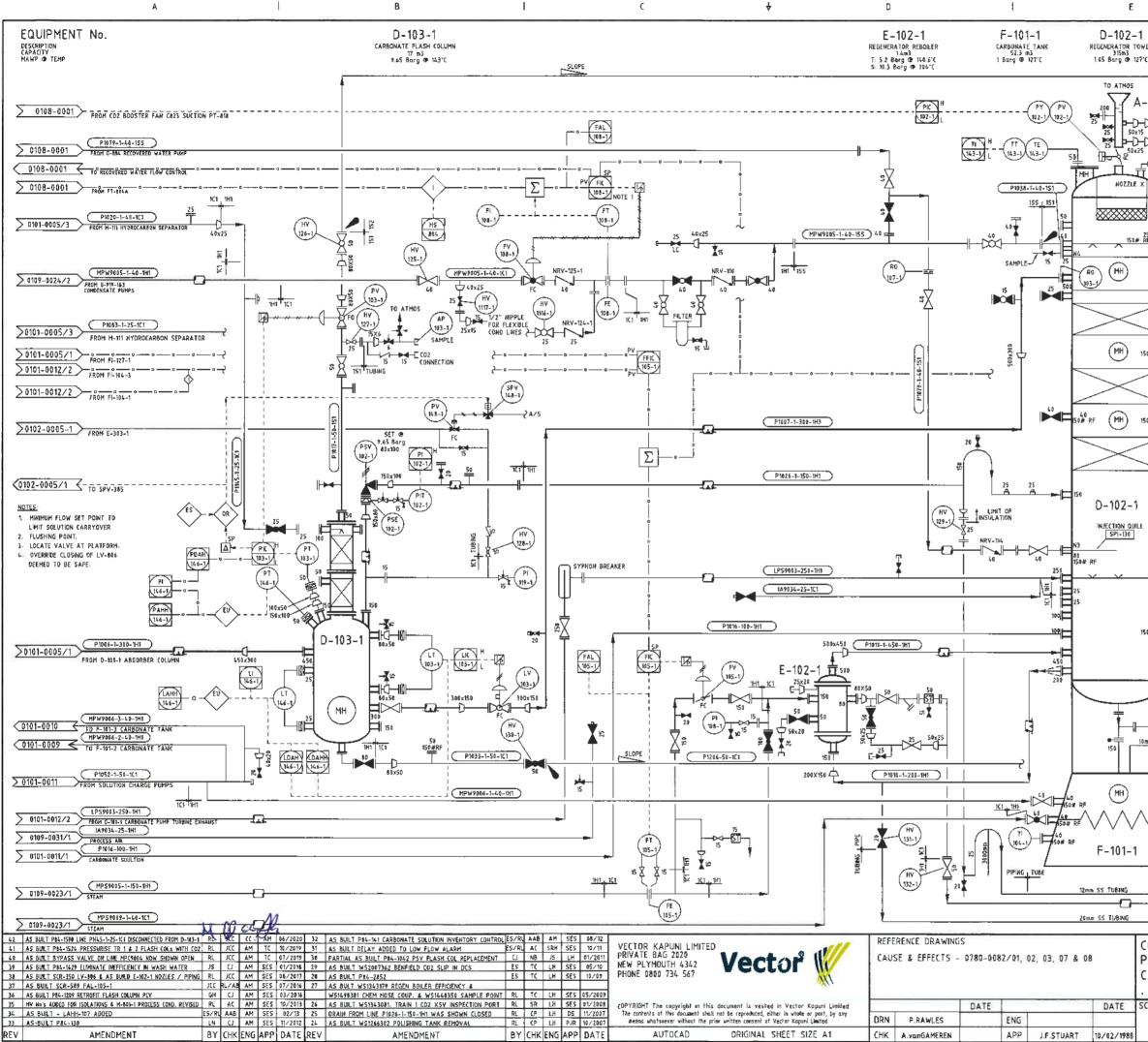
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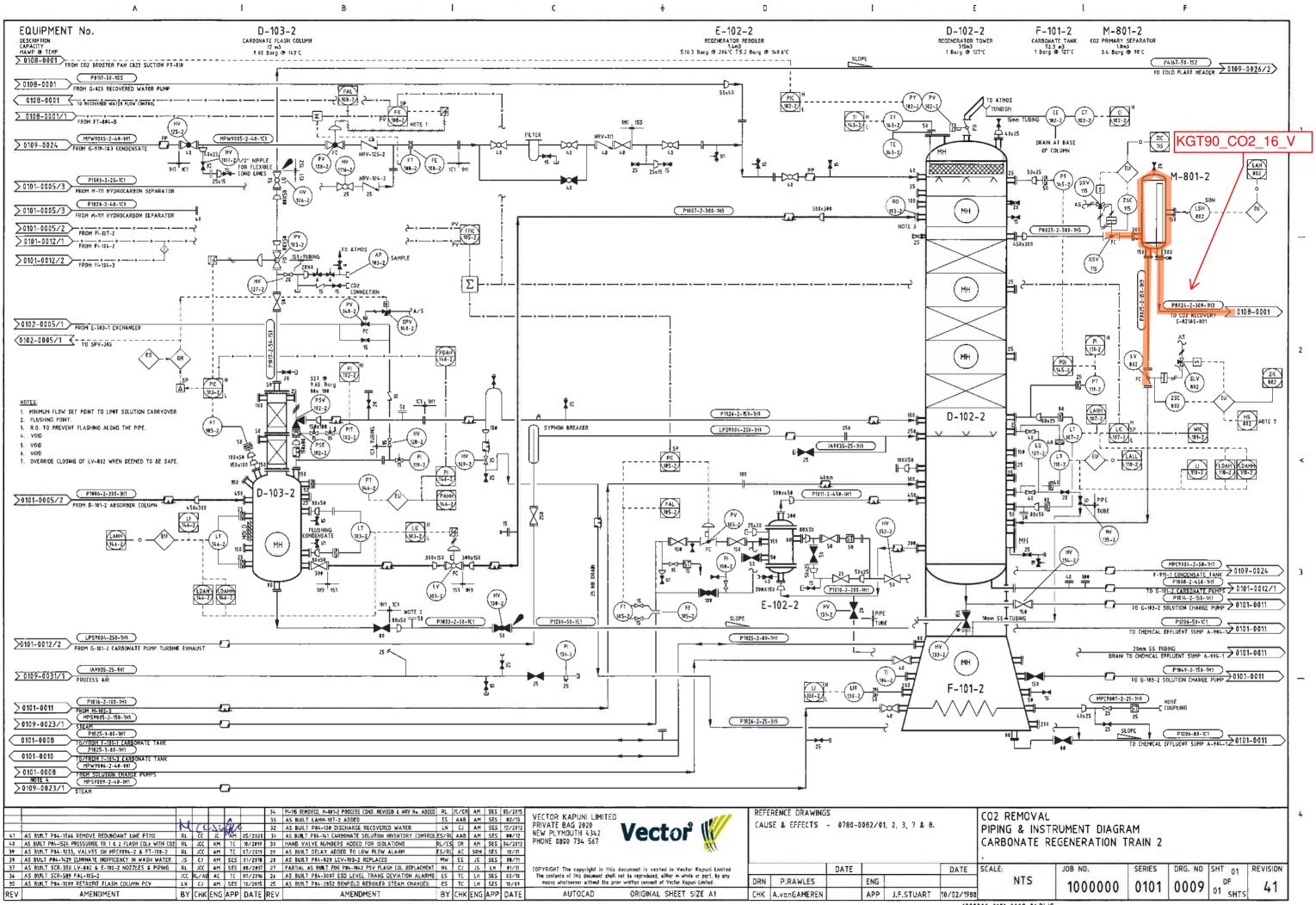


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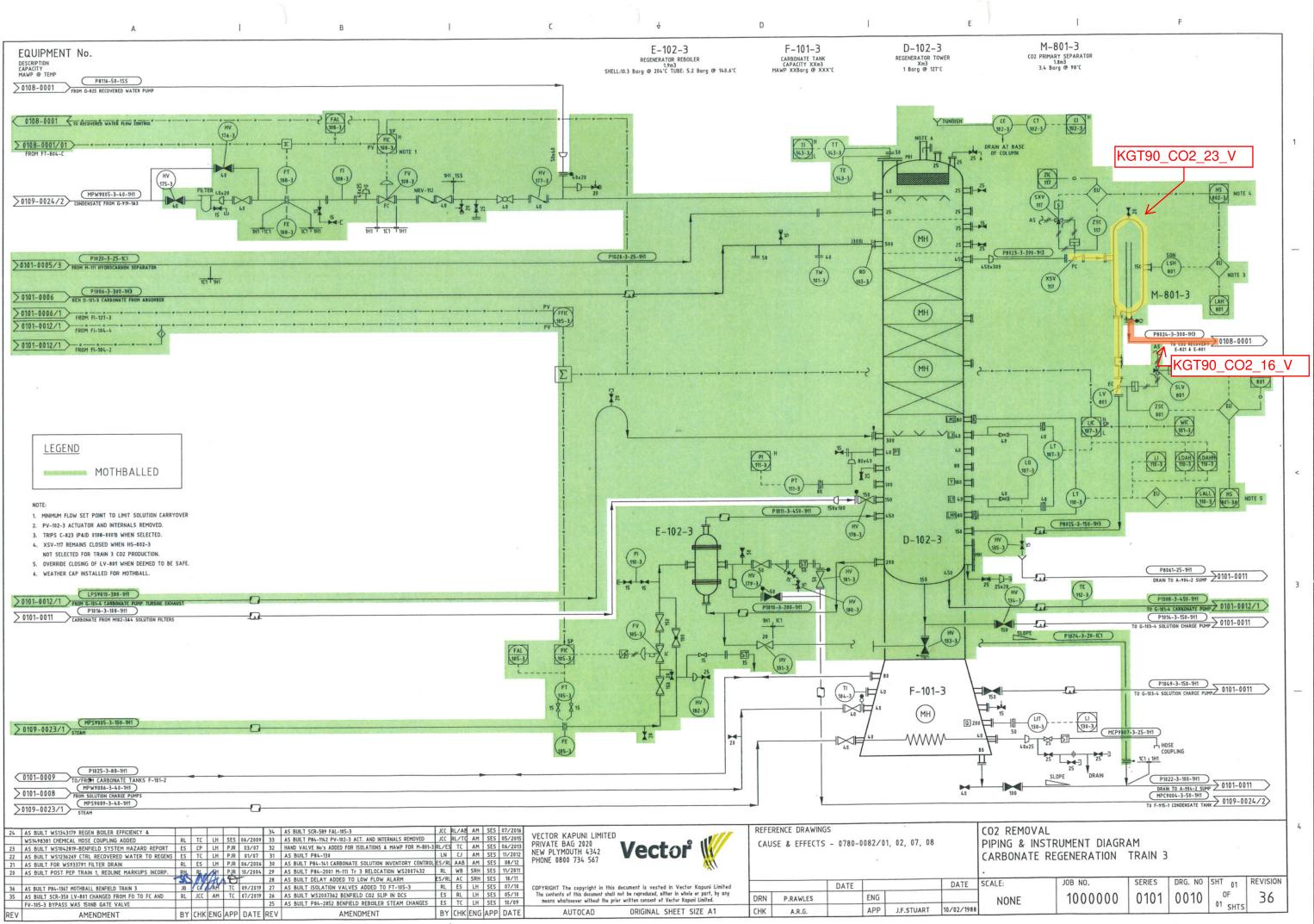


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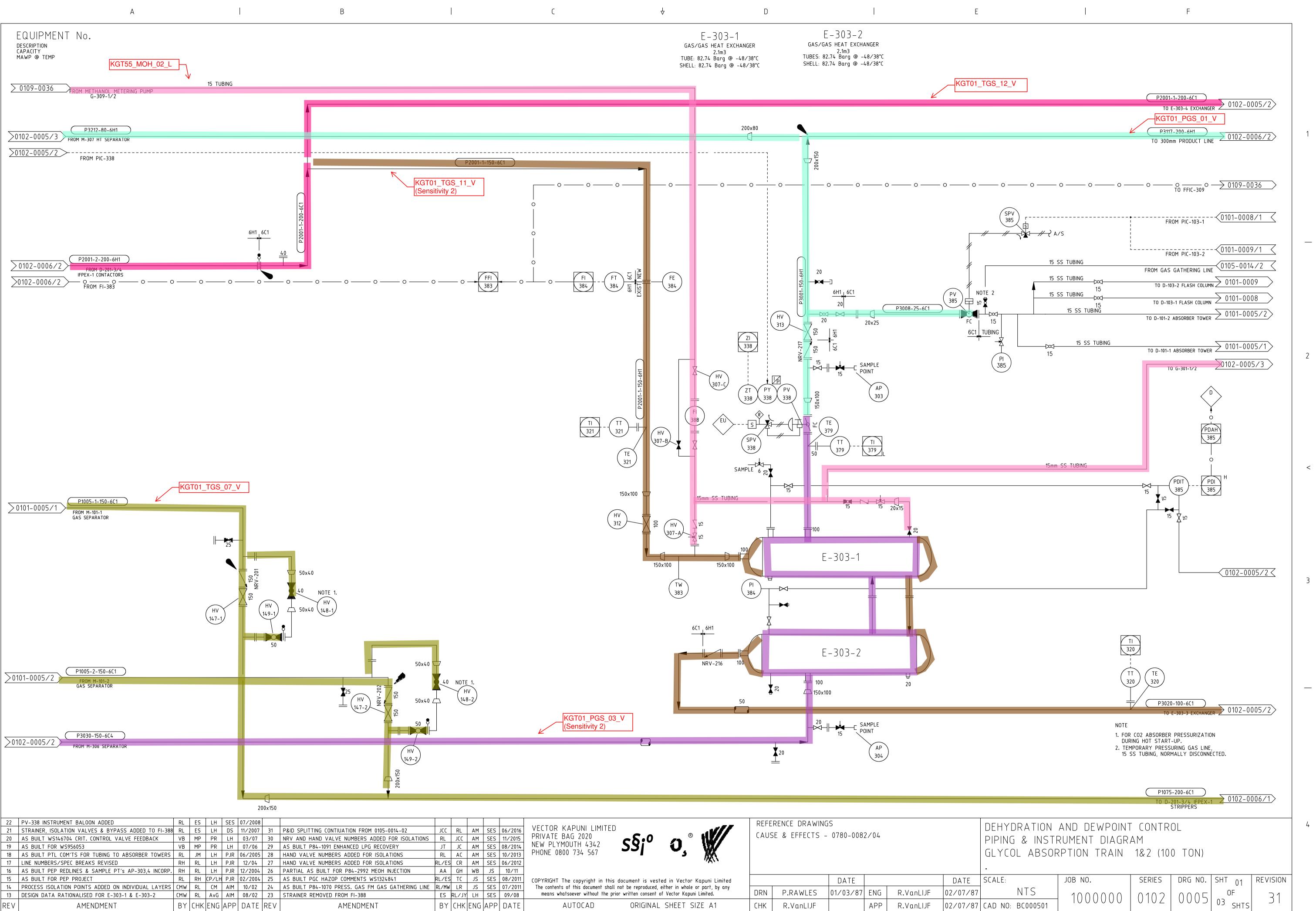
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			49-1-150-1H1	ING					
		Р	1-1 CHARGE PUM 1206-80-101	N0101 0					
80 MPC9004-1-50-IH1 TO F-915-1 CONDENSATE TANK0109-0024/2									
	DRAIN TO C		NT SUMP A-904	<u>&gt; 0101</u>		3.			
	RUMENT DIAGRA					4			
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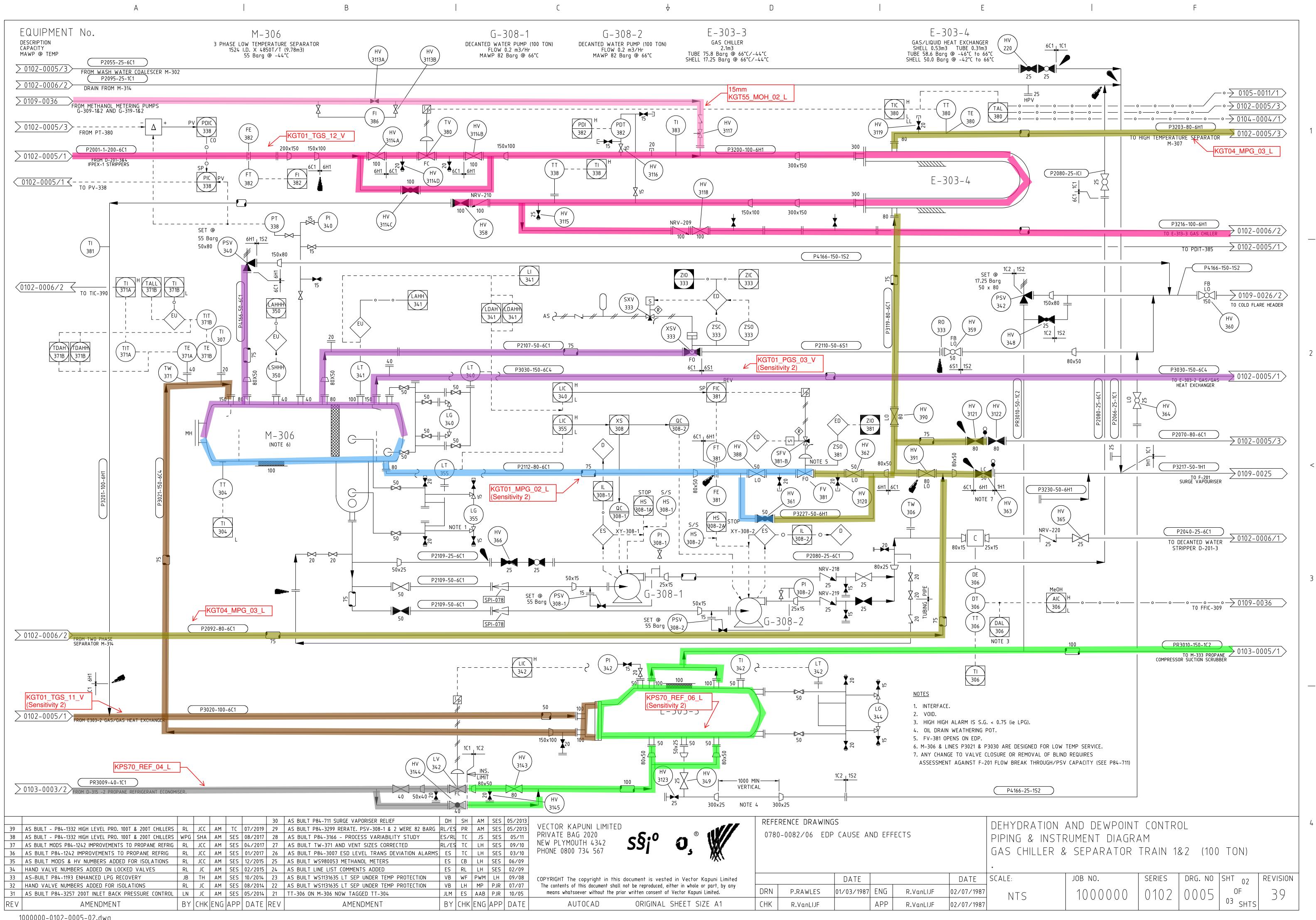
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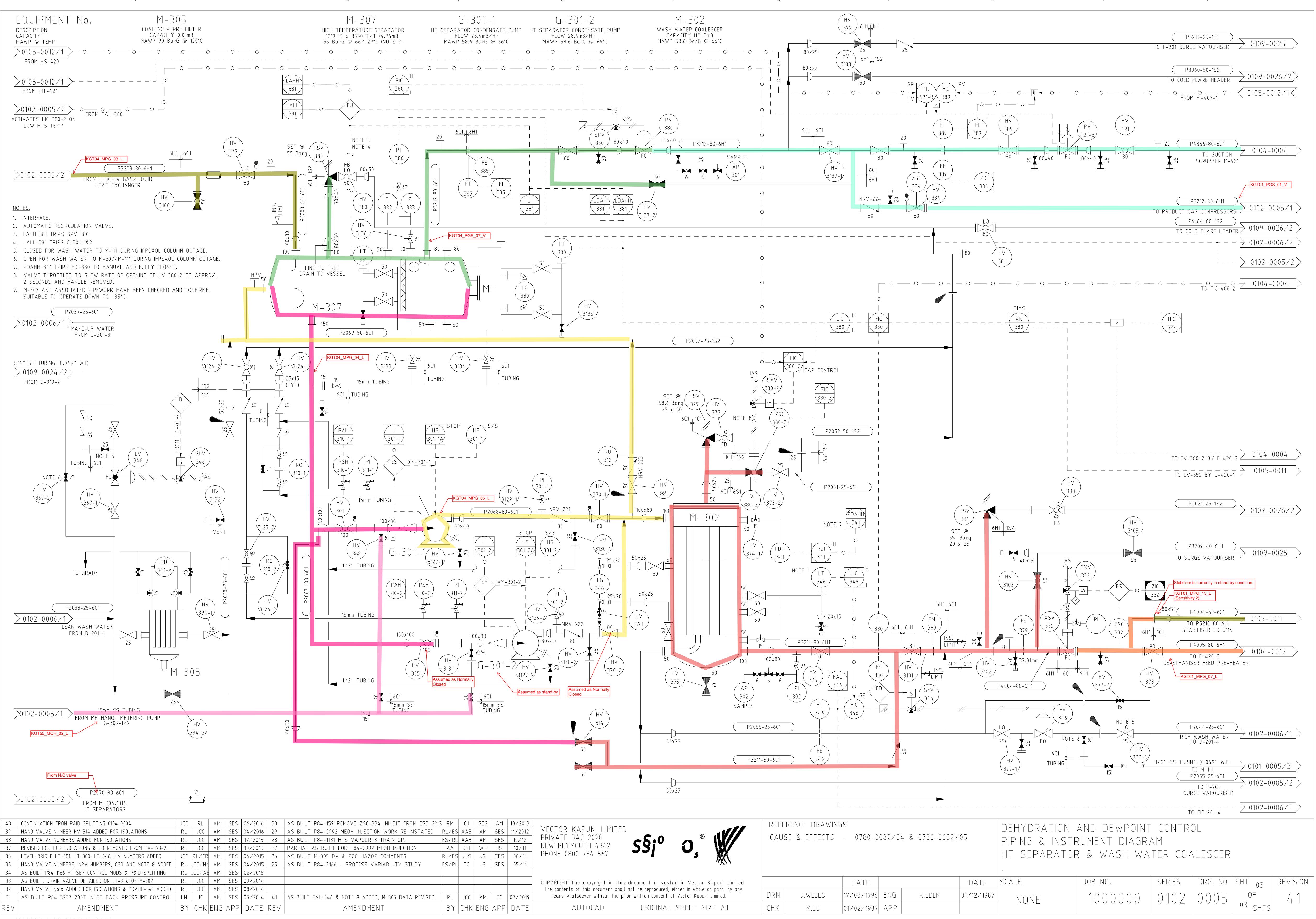
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	08/2011	COPYRIGHT The copyright in this document is vested in Vector Kapuni Limited			DATE			DATE	SCALE:	
ES	07/2011	The contents of this document shall not be reproduced, either in whole or part, by any			04 (07 (07			02 (07 (07	1 1	٨
ES	09/08	means whatsoever without the prior written consent of Vector Kapuni Limited.	DRN	P.RAWLES	01/03/87	ENG	R.VanLIJF	02/07/87		. ` _
PP	DATE	AUTOCAD ORIGINAL SHEET SIZE A1	СНК	R.VanLIJF		APP	R.VanLIJF	02/07/87	CAD NO: E	3



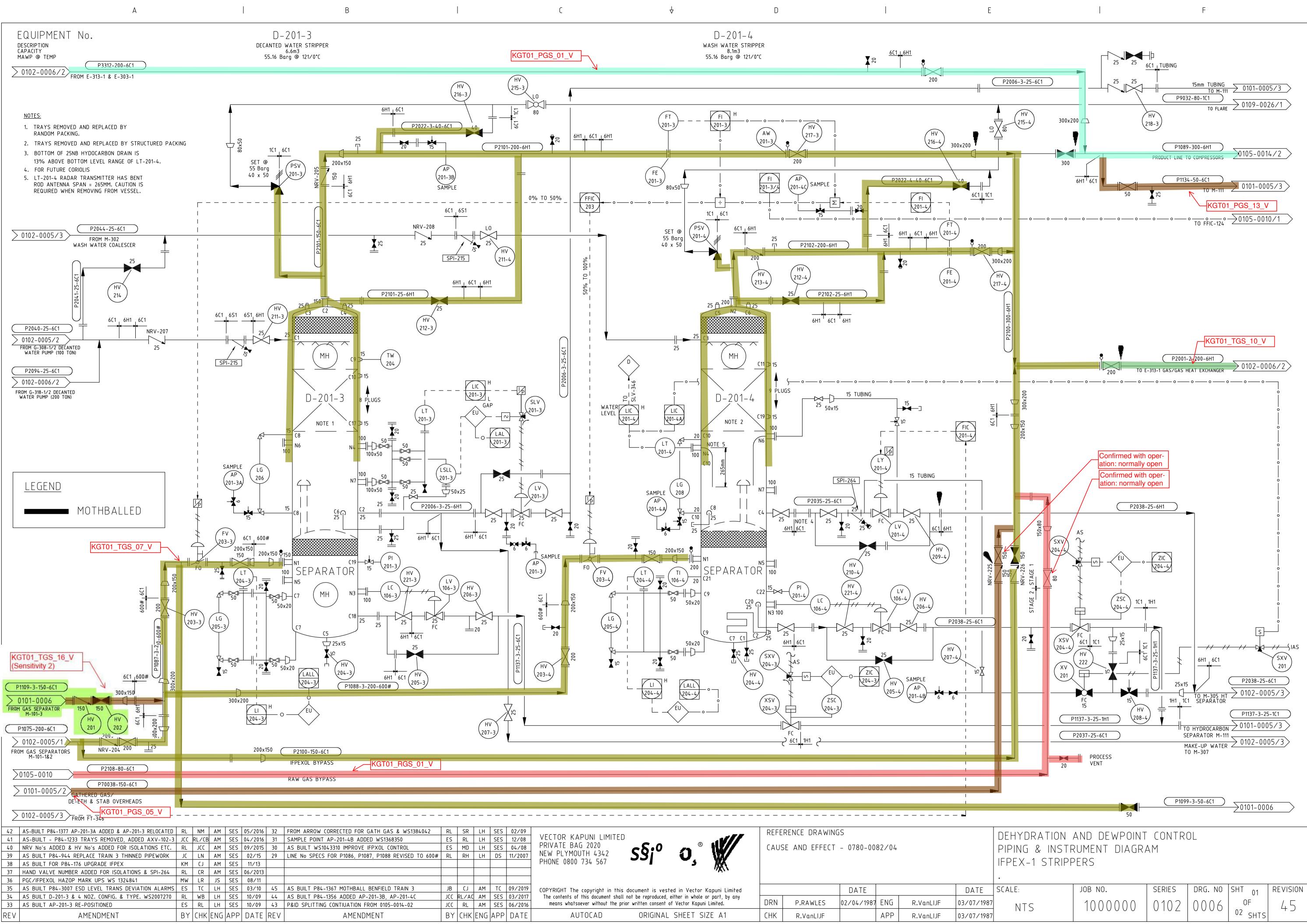
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5 BUILT P84-159 REMOVE ZSC-334 INHIBIT FROM ESD SYS	RM	CJ	SES	AM	10/2013	
S BUILT P84-2992 MEOH INJECTION WORK RE-INSTATED	RL/ES	AAB	AM	SES	11/2012	
5 BUILT P84-1131 HTS VAPOUR 3 TRAIN OP.	ES/RL	AAB	АM	SES	10/12	
ARTIAL AS BUILT FOR P84-2992 MEOH INJECTION	AA	GH	WВ	JS	10/11	
5 BUILT M-305 DV & PGC HAZOP COMMENTS	RL/ES	JHS	JS	SES	08/11	
5 BUILT P84-3166 - PROCESS VARIABILITY STUDY	ES/RL	ТC	JS	SES	05/11	
5 BUILT FAL-346 & NOTE 9 ADDED, M-305 DATA REVISED	RL	JCC	AM	TC	07/2019	1
AMENDMENT	BY	CHK	ENG	APP	DATE	

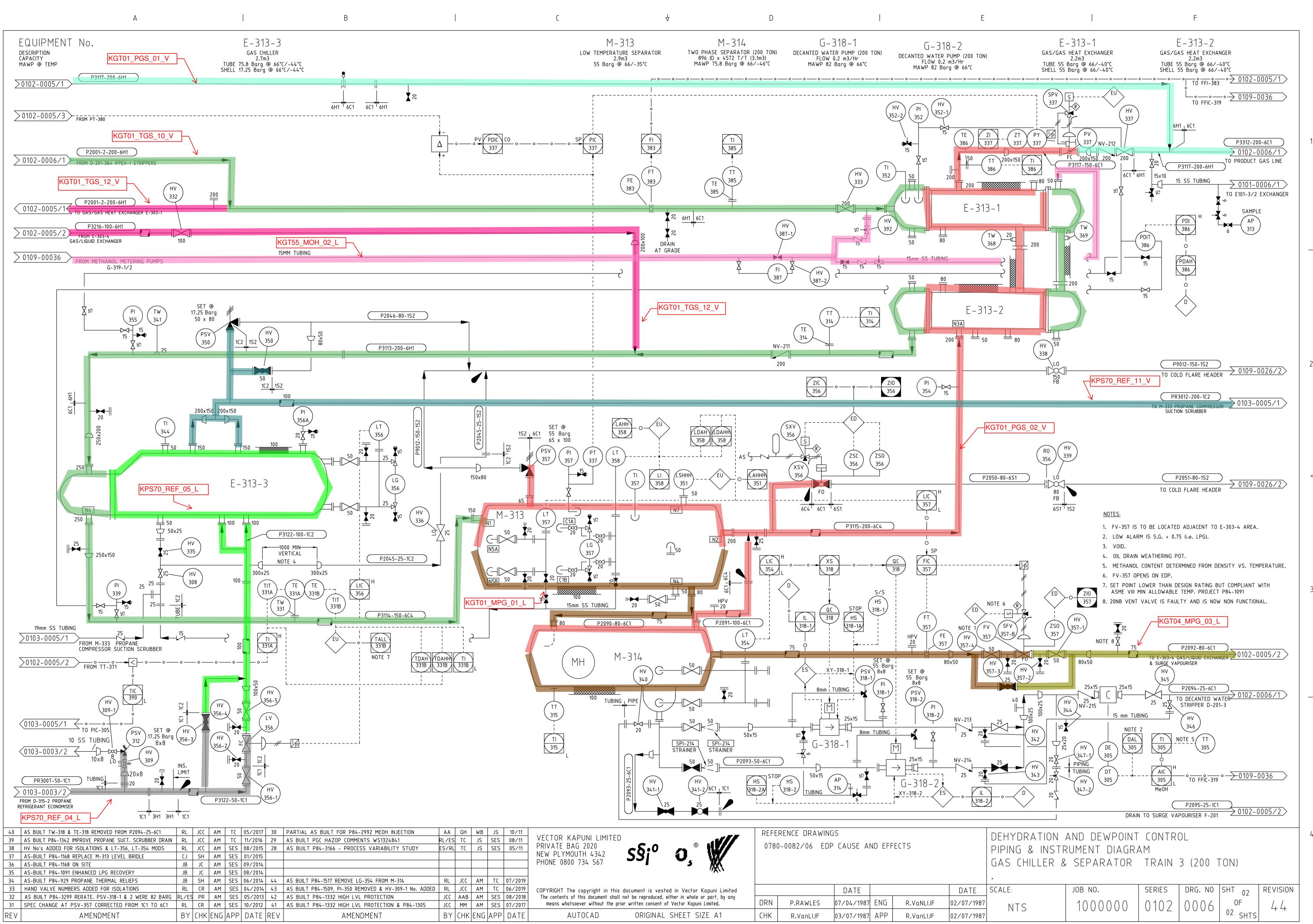
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DRN	J.WELLS	17/08/1996	ENG	K.EDEN	01/12/1987	
СНК	M.LU	01/02/1987	APP			



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AM	TC	09/2019	COPYRIGHT The copyright in this document is vested in Vector Kapuni Limited			DATE			DATE	S
AM	SES	03/2017	The contents of this document shall not be reproduced, either in whole or part, by any							ł
AM	SES	06/2016	means whatsoever without the prior written consent of Vector Kapuni Limited.	DRN	P.RAWLES	02/04/1987	ENG	R.VanLIJF	03/07/1987	
ENG	APP	DATE	AUTOCAD ORIGINAL SHEET SIZE A1	СНК	R.VanLIJF		APP	R.VanLIJF	03/07/1987	
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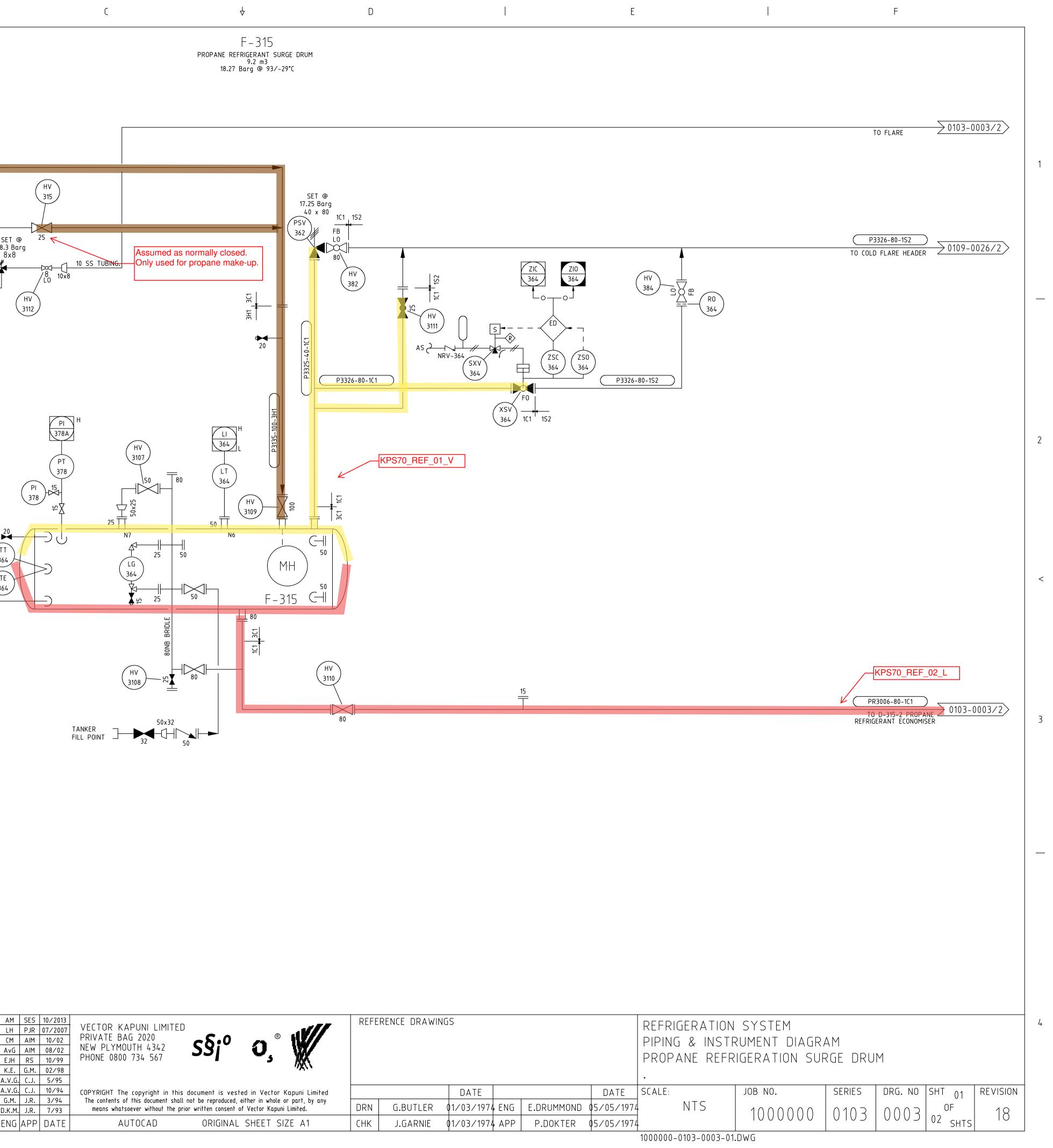
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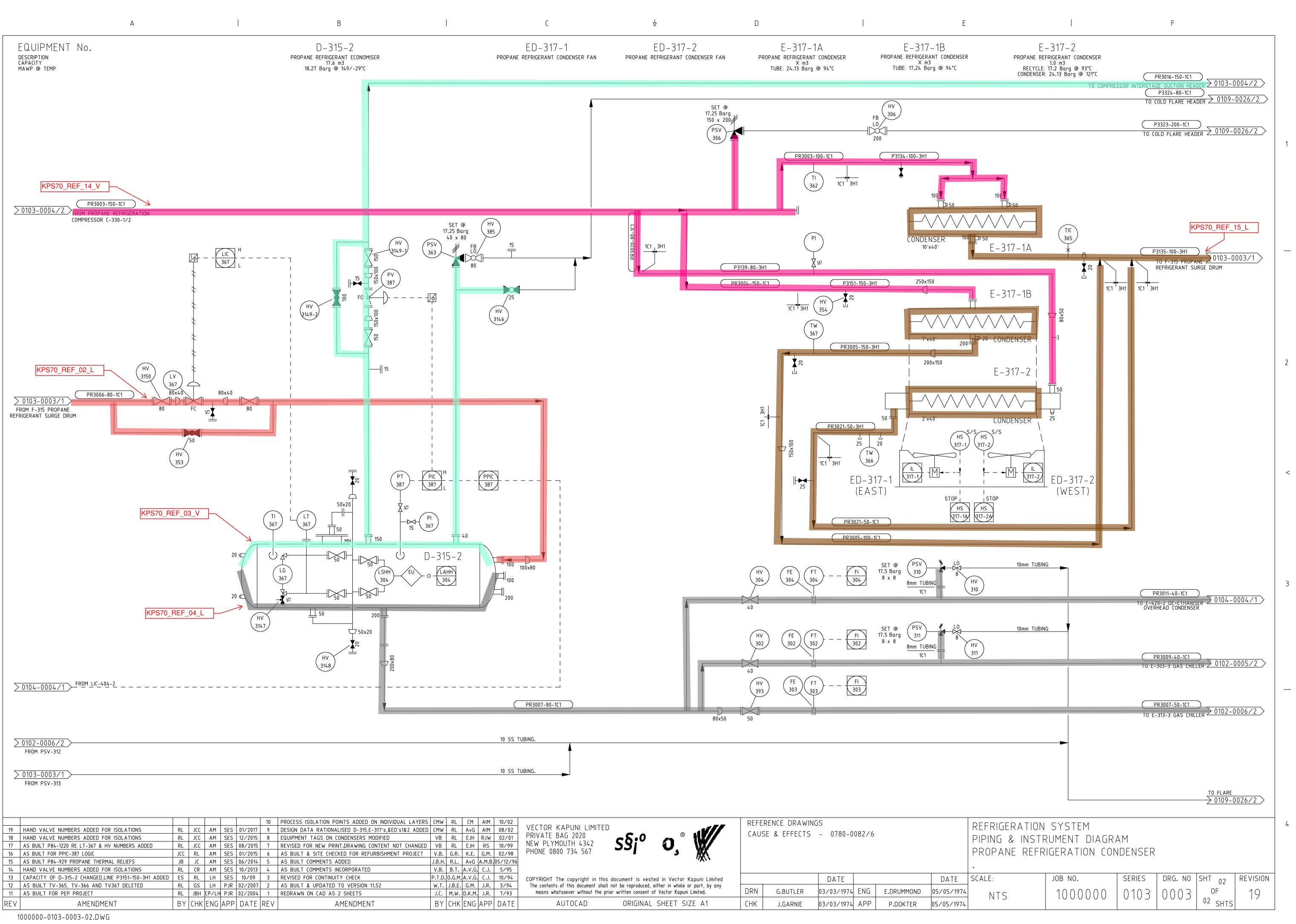


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A EQUIPMENT No. description capacity mawp @ temp	B	I C ↓ D I E F-315 PROPANE REFRIGERANT SURGE DRUM 9.2 m3 18.27 Barg @ 93/-29*C
P3135-100-3H1         0103-0003/2       FROM E-317-1/2 PROPANE REFRIGERANT COND         0104-0009       P3207-25-3C1         P3207-25-3C1       MAKE UP REFRI         0104-0009       FROM PROPANE PRODUCT COOLER         P3207-25-3C1       O104-0009         P3207-25-3C1       P3207-25-3C1         0104-0009       FROM PROPANE PRODUCT COOLER         TRAIN 1       TRAIN 1	$\frac{1}{3C1}$	ST 0 T 25 to 0 T 25
	$\overline{1}$	$\begin{array}{c} 378 \\ 378 \\ 78 \\ 78 \\ 78 \\ 78 \\ 78 \\ 78$
	13       HAND VALVE NUMBERS ADDED FOR ISOLATIONS         12       AS BUILT WS1059590 F-315 LEVEL TRANSMITTER UPGRADE         11       PPOCESS ISOLATION POPED ON INDIVIDUAL LAYERS	RL CR AM SES 10/2013 E RL NO LH P.R 07/2003 VECTOR KAPUNI LIMITED FRVM ZI VI ON 1002 PRIVATE BAG 2020
17HAND VALVE NUMBERS ADDED FOR ISOLATIONSRL16AS BUILT FOR P&ID SPLITTING - CONT. DRG. No'S REVISEDRL15AS-BUILT P84-856 INTERLOCH LOW TEMP PROTECHTIONLN14AS-BUILT P84-929 PROPANE THERMAL RELIEFSJB	Image: style styl	s cmw rl cm aim 10/02 cmw rl avg aim 08/02 D VB rl ejh rs 10/99 PRIVATE BAG 2020 NEW PLYMOUTH 4342 PHONE 0800 734 567 PRIVATE BAG 2020 SS; O J (1) SS; O J (1) PRIVATE BAG 2020 NEW PLYMOUTH 4342 PHONE 0800 734 567 PRIVATE BAG 2020 NEW PLYMOUTH 4342 PHONE 0800 734 567 PRIVATE BAG 2020

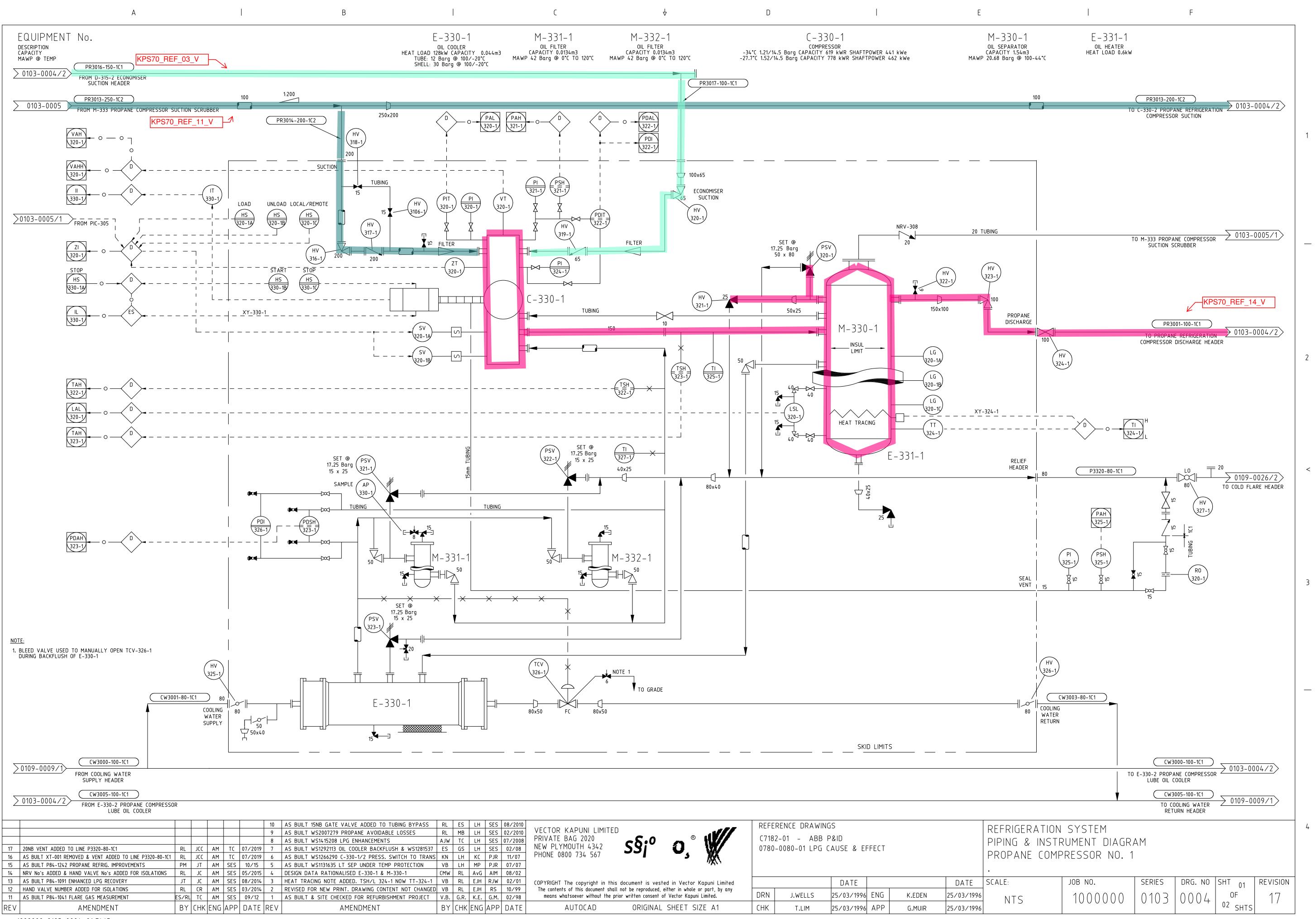
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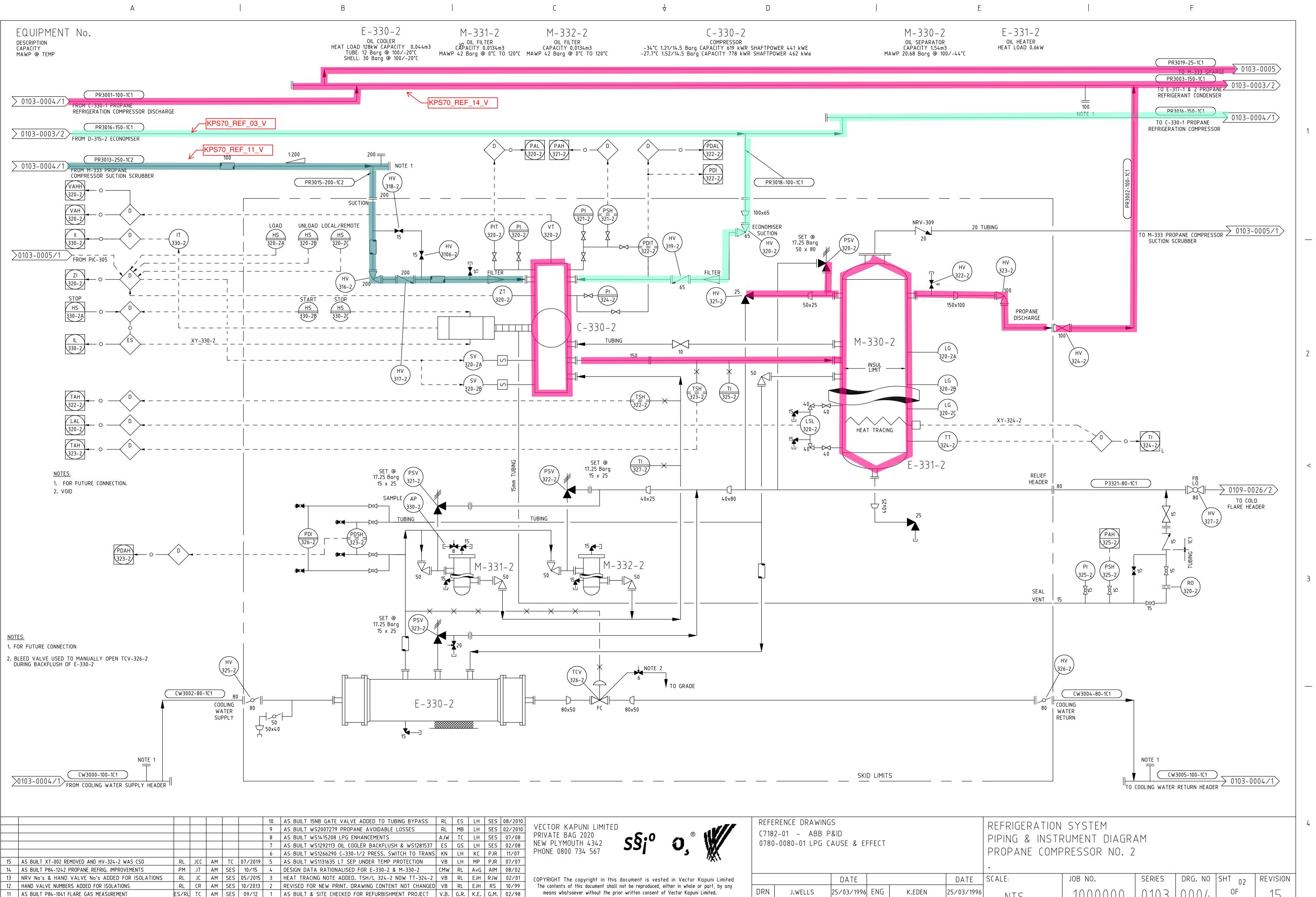
							10	PROCESS ISOLATION POINTS ADDED ON INDIVIDUAL LAYERS	CMW	RL
19	HAND VALVE NUMBERS ADDED FOR ISOLATIONS	RL	JCC	AM	SES	01/2017	9	DESIGN DATA RATIONALISED D-315,E-317's,&ED's1&2 ADDED	CMW	RL
18	HAND VALVE NUMBERS ADDED FOR ISOLATIONS	RL	JCC	AM	SES	12/2015	8	EQUIPMENT TAGS ON CONDENSERS MODIFIED	VB	RL
17	AS BUILT P84-1220 RE LT-367 & HV NUMBERS ADDED	RL	JCC	AM	SES	08/2015	7	REVISED FOR NEW PRINT.DRAWING CONTENT NOT CHANGED	VB	RL
16	AS BUILT FOR PPIC-387 LOGIC	JCC	RL	AM	SES	01/2015	6	AS BUILT & SITE CHECKED FOR REFURBISHMENT PROJECT	V.B.	G.R.
15	AS BUILT P84-929 PROPANE THERMAL RELIEFS	JB	JC	AM	SES	06/2014	5	AS BUILT COMMENTS ADDED	J.B.H.	R.L.
14	HAND VALVE NUMBERS ADDED FOR ISOLATIONS	RL	CR	AM	SES	10/2013	4	AS BUILT COMMENTS INCORPORATED	V.B.	B.T.
13	CAPACITY OF D-315-2 CHANGED,LINE P3151-150-3H1 ADDED	ES	RL	LH	SES	10/09	3	REVISED FOR CONTINUITY CHECK	P.T.D.	0.G.M.
12	AS BUILT TV-365, TV-366 AND TV367 DELETED	RL	GS	LH	РJR	02/2007	2	AS BUILT & UPDATED TO VERSION 11.52	W.T.	J.B.E.
11	AS BUILT FOR PEP PROJECT	RL	JBH	CP/LH	РJR	02/2004	1	REDRAWN ON CAD AS 2 SHEETS	J.C.	M.W.
REV	AMENDMENT	ΒY	СНК	ENG	APP	DATE	REV	AMENDMENT	ΒY	СНК

	C.J.	10/94	COPYRIGHT The copyright in this document is vested in Vector Kapuni Limited	DATE							
	J.R. J.R.		The contents of this document shall not be reproduced, either in whole or part, by any means whatsoever without the prior written consent of Vector Kapuni Limited.	DRN	G.BUTLER	03/03/1974	ENG	E.DRUMMOND	05/05/19		
ING	APP	DATE	AUTOCAD ORIGINAL SHEET SIZE A1	СНК	J.GARNIE	03/03/1974	APP	P.DOKTER	05/05/19		



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٦L	ES	LH	SES	08/2010					REFE	RENCE DRAWIN	GS			
٦L	MB	LH	SES	02/2010	VECTOR KAPUNI LIMITED	-								
JW	TC	LH	SES	07/2008	PRIVATE BAG 2020	c2.0	R		C7183	2-01 - ABB	P&ID			
S	GS	LH	SES	02/08	NEW PLYMOUTH 4342	S§i <sup>0</sup>	Ú		0780	-0080-01 LPG	CAUSE & EI	FECT		
٢N	LH	KC	PJR	11/07	PHONE 0800 734 567		- 5	ĸ						
/B	LH	MP	PJR	07/07				<i>''</i> 7N						
MW	RL	AvG	AIM	08/02										
/B	RL	EJH	RJW	02/01	COPYRIGHT The copyright in this c	locument is vest	ed in Vector	Kapuni Limited			DATE			DATE
/B	RL	EJH	RS	10/99	The contents of this document shall n									
.в.	G.R.	K.E.	G.M.	02/98	means whatsoever without the prior	•			DRN	J.WELLS	25/03/1996	ENG	K.EDEN	25/03/1996
3Y	снк	ENG	APP	DATE	AUTOCAD	ORIGINAL	SHEET SI	ZE A1	СНК	T.LIM	25/03/1996	APP	G.MUIR	25/03/1996
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AMENDMENT

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AMENDMENT

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	AJW	TC	LH	SES	07/08	PRIVATE BAG 2020						PIPING & INS	TRUMENT DIAGR	ΔΜ		
537	ES	GS	LH	SES	02/08	VECTOR KAPUNI LIMITED PRIVATE BAG 2020 NEW PLYMOUTH 4342 PHONE 0800 734 567	0780-0	080-01 LPG (	AUSE & EFFE	ECT						
ANS	KN	LH	KC	PJR	11/07	PHONE 0800 734 567						PROPANE COP	1PRESSOR NO. 2	-		
	VB	LH	MP	PJR	07/07	<b>2X</b> \\										
	CMW	RL	AvG	AIM	08/02							٥				
4-2	VB	RL	EJH	RJW	02/01	COPYRIGHT The copyright in this document is vested in Vector Kapuni Limited			DATE		DATE	SCALE:	JOB NO.	SERIES	DRG. NO SHT 02	REVISION
IGED	VB	RL	EJH	RS	10/99	The contents of this document shall not be reproduced, either in whole or part, by any						-			02	
Т	V.B.	G.R.	K.E.	G.M.	02/98	means whatsoever without the prior written consent of Vector Kapuni Limited.	DRN	J.WELLS	25/03/1996 E	NG K.EDEN	25/03/1996	NTS	100000	10103	$ 0004 _{00}$	15
	ΒY	CHK	ENG	APP	DATE	AUTOCAD ORIGINAL SHEET SIZE A1	СНК	T.LIM	25/03/1996 A	G.MUIR	25/03/1996				0000 02 SHTS	S



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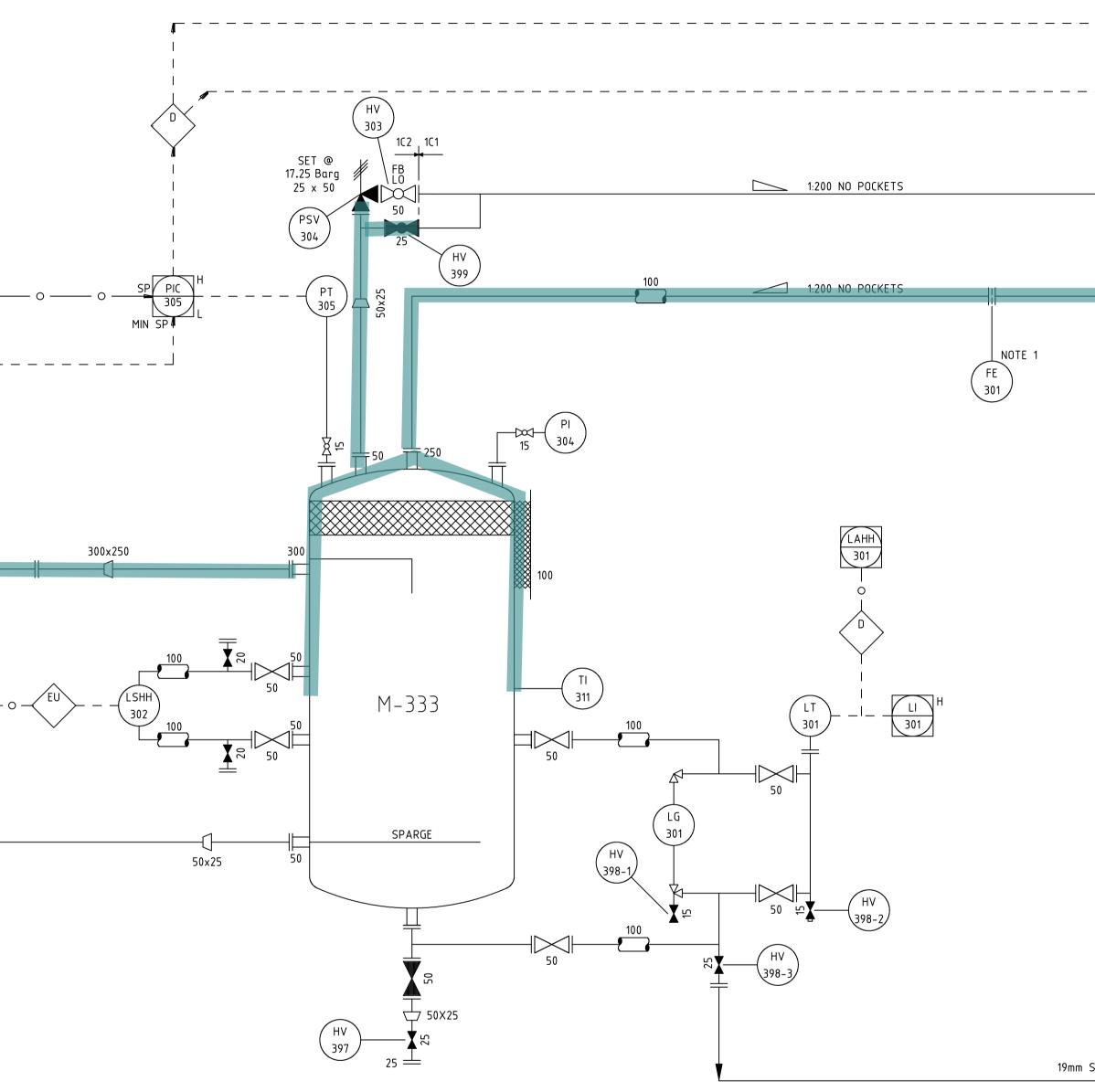
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[ (	EQUIPMENT NO. Description CAPACITY MAWP @ TEMP								
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	>0102-0006/2 FI	О О С С	o	— o —— o	Fx	o o o o o o	o	- o —— o —	SP PIC H 305 L MIN SP I
	> 0104-0004	FROM FT-136 P3205-150-3H1 FROM E-420-2 DE-ETHANISER OVERHEAD CONDENSER	3H1 1C1	75 NRV-1	303	HV 328 PR3008-150-1C1			
	>0102-0006/2	PR3012-200-1C1 FROM E-313-3 GAS CHILLER		100 NRV-3 20 100 NRV-3	200		100	300×250	N
	> 0102-0005/2	PR3010-150-1C2 FROM E-303-3 GAS CHILLER KPS70_REF_06_L (Sensitivity 2)		100 NRV-1 15		150x250 HV 330			
							LAHH 302 0 -		100 LSHH 302 100
		KPS70_REF_14	_ <u>v</u>	HV 395	R 30		25		
	> 0103-0004/2	FROM COMPRESSOR DISCHARGE				HV 831-1	PIPE TUBE		50×25
	> 0103-0004/1 F	20 TUBING ROM M-330-1 OIL SEPARATOR			20	20	HV 396		
	> 0103-0004/2	20 TUBING ROM M-330-2 OIL SEPARATOR			20	HV			
						331-2			
						EVEL BRIDLE LT-301, NRV, HV NUMBERS ADDED IAND VALVE NUMBERS ADDED FOR ISOLATIONS	JCC RL/CB AM RL CR AM	SES 04/2015 SES 10/2013	VECTOR KAP
					8 M 7 A 6 A 5 A	AND VALVE NOMBERS ADDED FOR ISOLATIONS 1-333 LEVEL BRIDLE AND DRAIN AS BUILT AS BUILT WS955915 PERMANENT DRAIN FROM M-333 AS BUILT WS2007279 PROPANE AVOIDABLE LOSSES AS BUILT REDUCER CHANGED AS BUILT WS1131635 LT SEP UNDER TEMP PROTECTION	RL     CR     AM       RL     MB     LH       RL     MB     LH       RL     MB     LH       ES     RL     LH       VB     LH     MP	SES         10/2015           SES         02/2011           SES         03/2010           SES         02/2010           SES         10/09           PJR         07/07	PRIVATE BAG NEW PLYMOUT PHONE 0800 7
13 12 11 RE V	AS BUILT M-333 LEVEL HIG AS BUILT P84-1242 PROPAI		JCC RL/AC A		5 3 P 6 2 M 5 1 A	PROCESS ISOLATION POINTS ADDED ON INDIVIDUAL LAYERS 1ANHOLE ON M-333 REMOVED AS BUILT FOR REFURBISHMENT PROJECT AMENDMENT		AIM 10/02 RS 10/99 G.M. 02/98	COPYRIGHT The c The contents of th means whatsoev AUT

							5	AS BUILT REDUCER CHANGED
							4	AS BUILT WS1131635 LT SEP
13	AS BUILT P84-1342 IMPROVE PROPANE SUCT. SCRUBBER DRAIN	RL	JCC	AM	TC	11/2016	3	PROCESS ISOLATION POINTS A
12	AS BUILT M-333 LEVEL HIGH HIGH	JCC	RL/AC	AM	SES	06/2016	2	MANHOLE ON M-333 REMOVED
11	AS BUILT P84-1242 PROPANE REFRIG. IMPROVEMENTS	PM	JT	AM	SES	10/2015	1	AS BUILT FOR REFURBISHMEN
REV	AMENDMENT	BY	СНК	ENG	APP	DATE	REV	AMENI

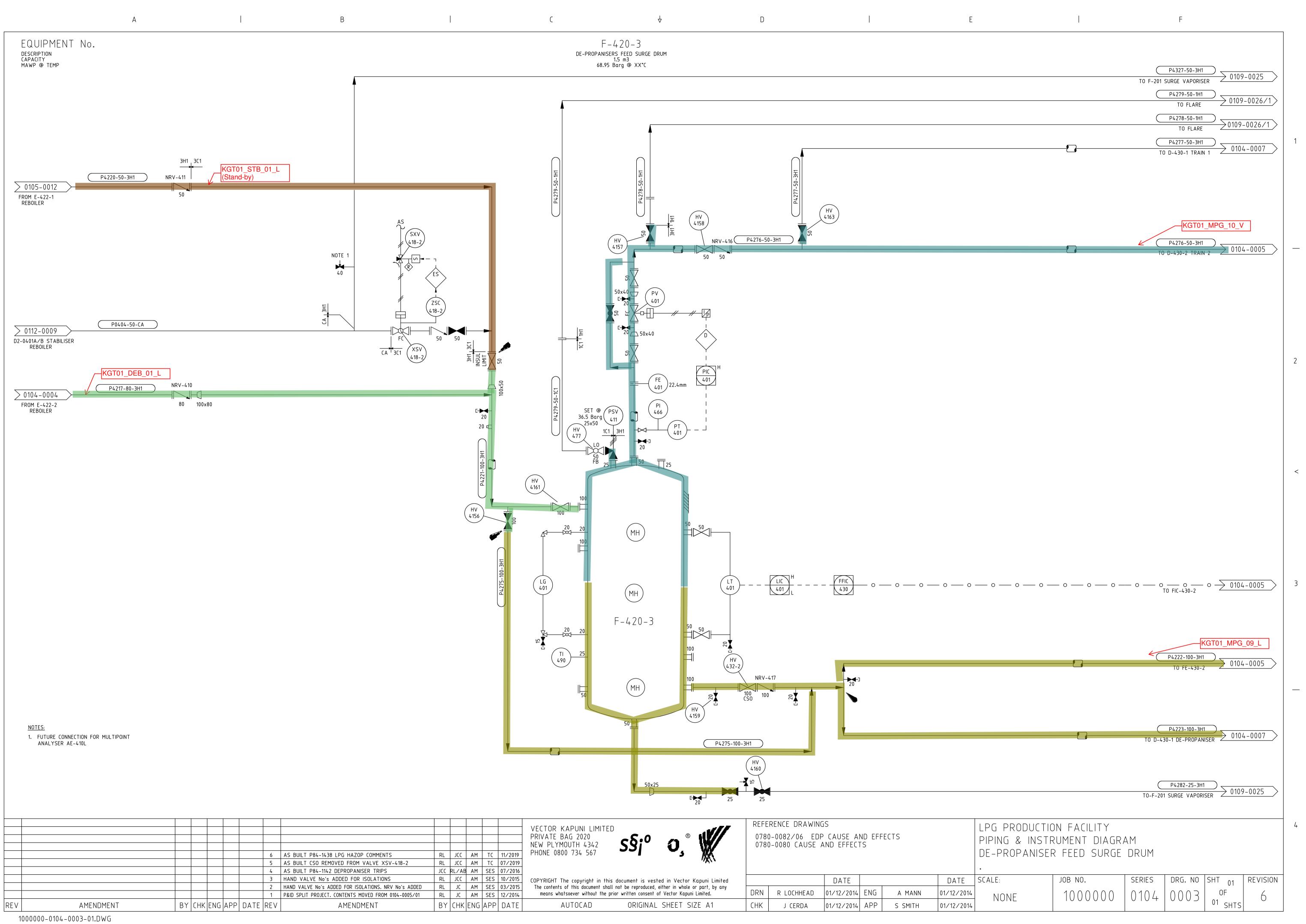
## M-333 PROPANE COMPRESSOR SUCTION SCRUBBER 1090 Ø x 2150 MAWP 17.25Barg @ +60°C TO -44°C

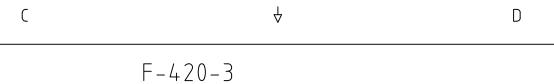
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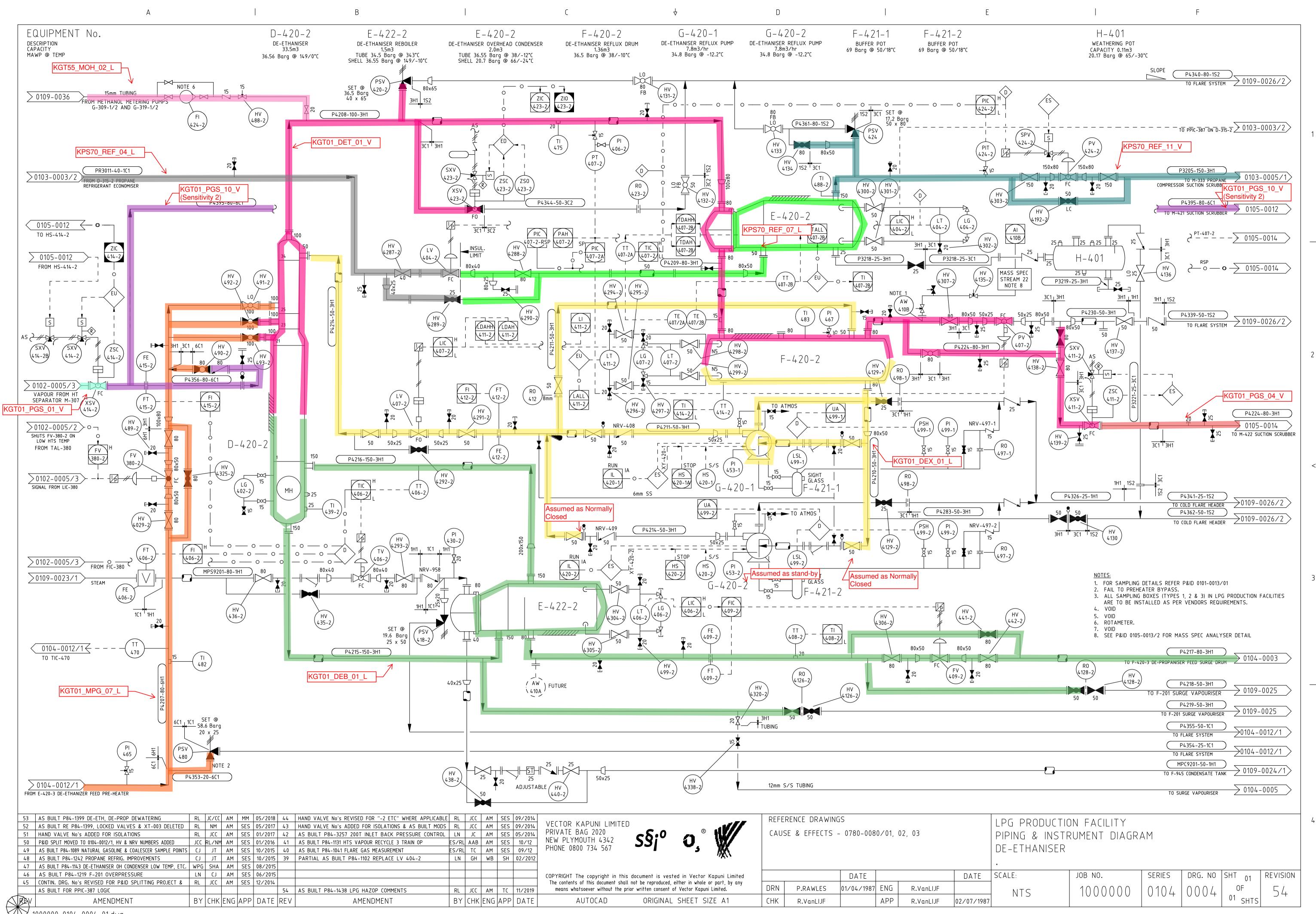
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					— — — — <u>—</u> — <u>—</u> — — — — — — — — — — —	- >0103-0004/1
					TO C-330-2	>0103-0004/2>
	1:200 NO POCKETS				( P3322-50-1C1	) 0109-0026/2
			KP	670_REF_11_V		
2	1:200 NO POCKETS		4		PR3013-250-1C2	0103-0004/1>
2				PROPA	TO C-330-1 & C-330-2 NE REFRIGERATION COMPRESS	
		FE NOTE 1				
		301				
		LIH				
		301				
LG 301						
× ₽	50 LD HV 398-2					
- <b>X</b> 25	(HV)					
Ŧ	398-3					
▼		19mm SS	TUBING		TO COLD FLARE	0102-0006/2
					<u>NOTES:</u> 1. FLOW ELEMENT RE	PLACED WITH A FULL BORE
					ORIFICE.	
ENCE DRAW						
LINCE DRAW			REFRIGERATIO PIPING & INS	on system Strument diag	IRAM	
				MPRESSOR SEF		
	DATE	DATE SC	CALE:	JOB NO.	SERIES DRG.	NO SHT <sub>01</sub> REV
J.WELLS	27/03/1996 ENG	K.EDEN 26/03/1996	NTS	100000		ης OF 1
T.LIM	26/03/1996 APP	26/03/1996				01 SHTS



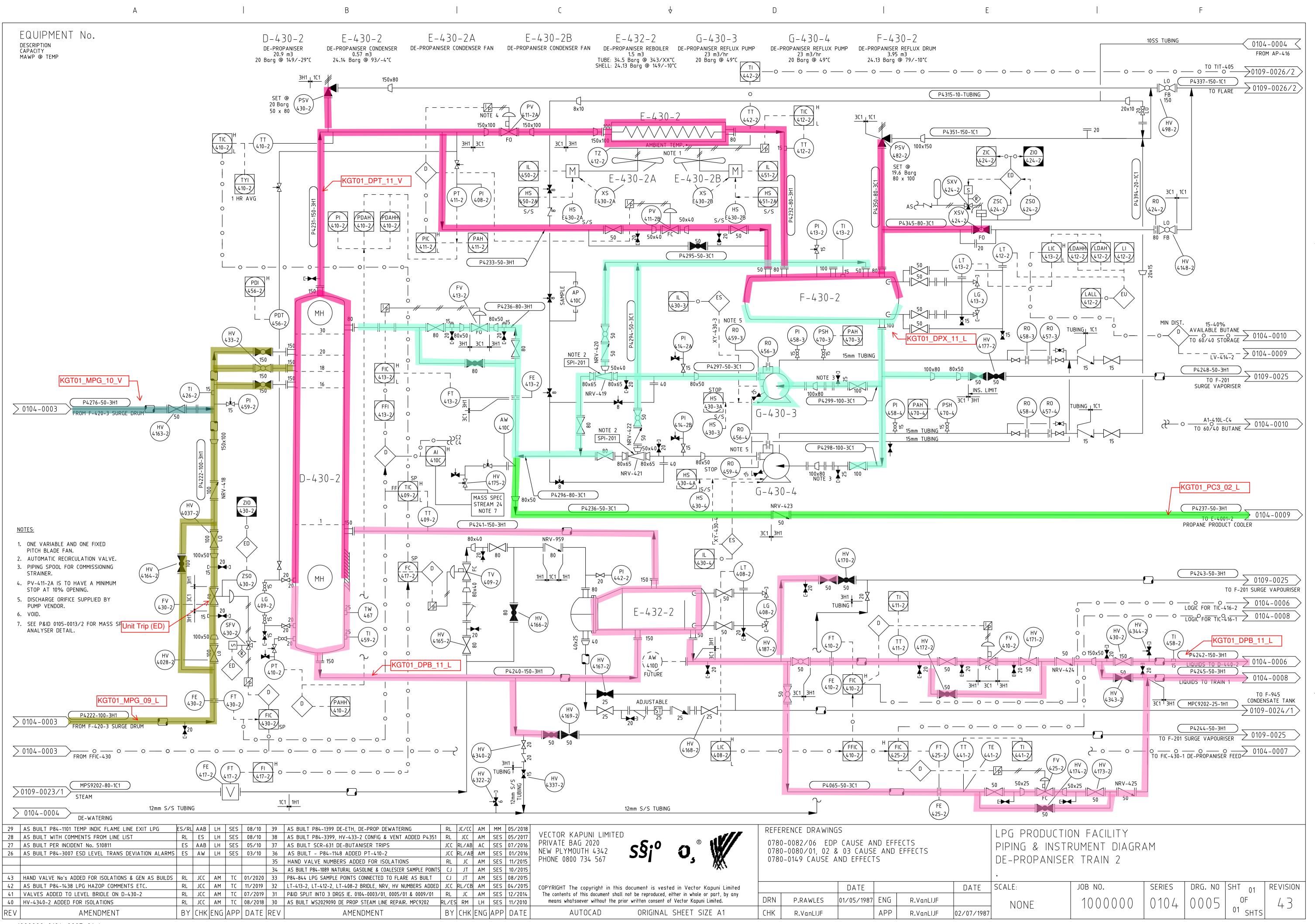


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			PRIVATE BAG 2020 NEW PLYMOUTH 4342 DHONE 0800 734 547 SS;°0 0 ®	0780	)-0080 CAUSE /	AND EFFEC	S			1
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3 AM	SES	07/2016								۰
AM	SES	10/2015	COPYRIGHT The copyright in this document is vested in Vector Kapuni Limited			DATE			DATE	SC
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ENC	i APP	DATE	AUTOCAD ORIGINAL SHEET SIZE A1	CHK	J CERDA	01/12/2014	APP	S SMITH	01/12/2014	
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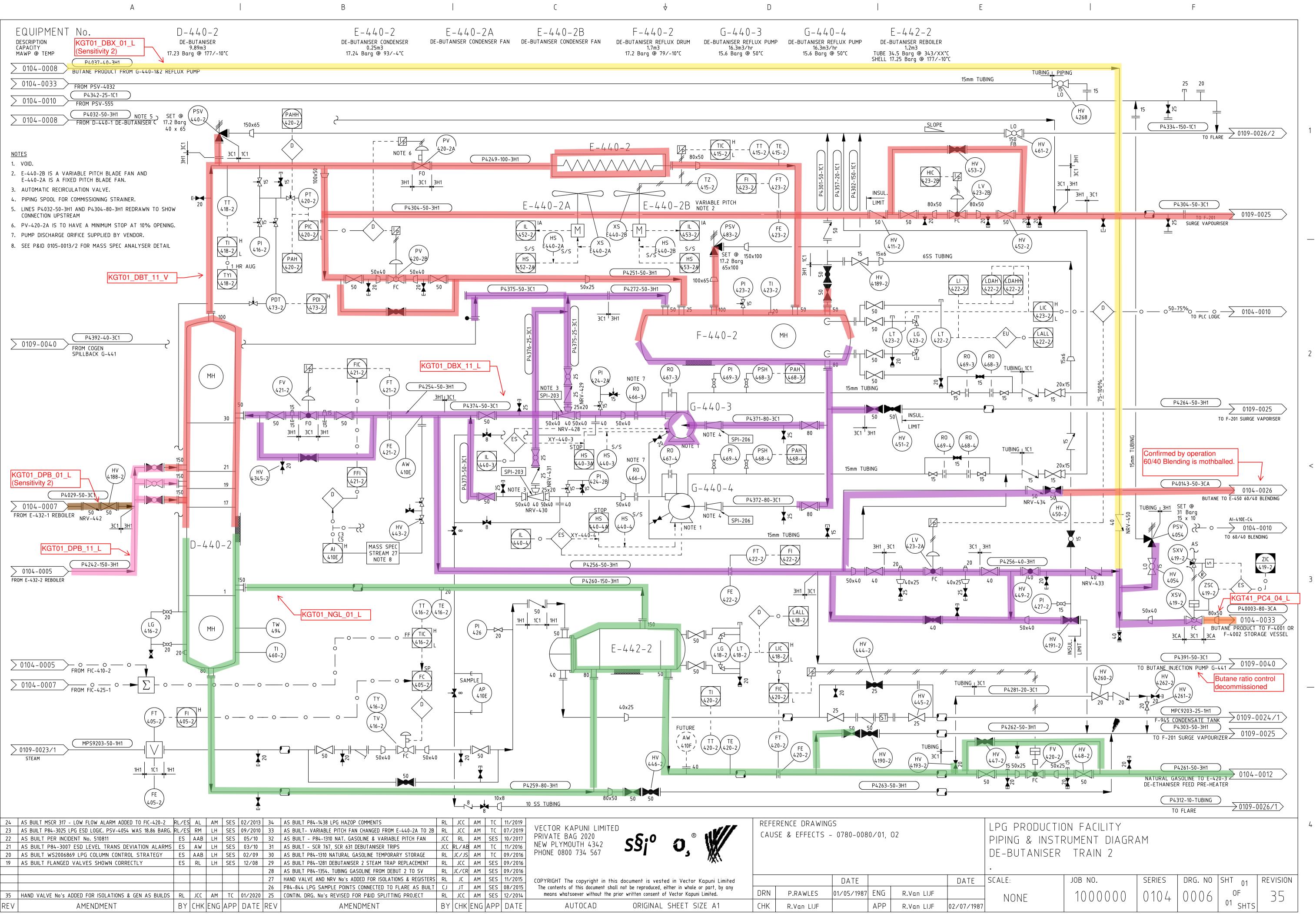


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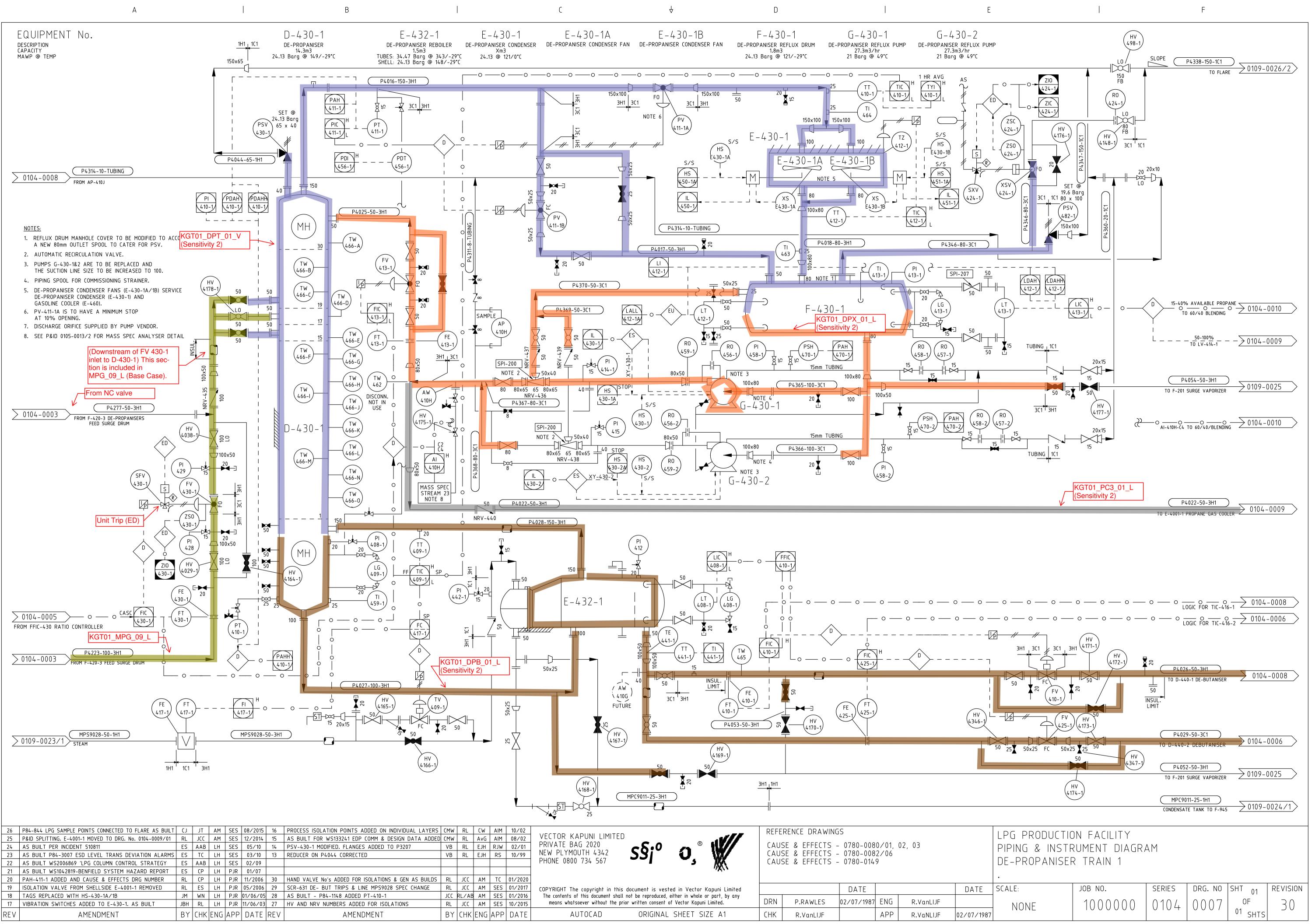




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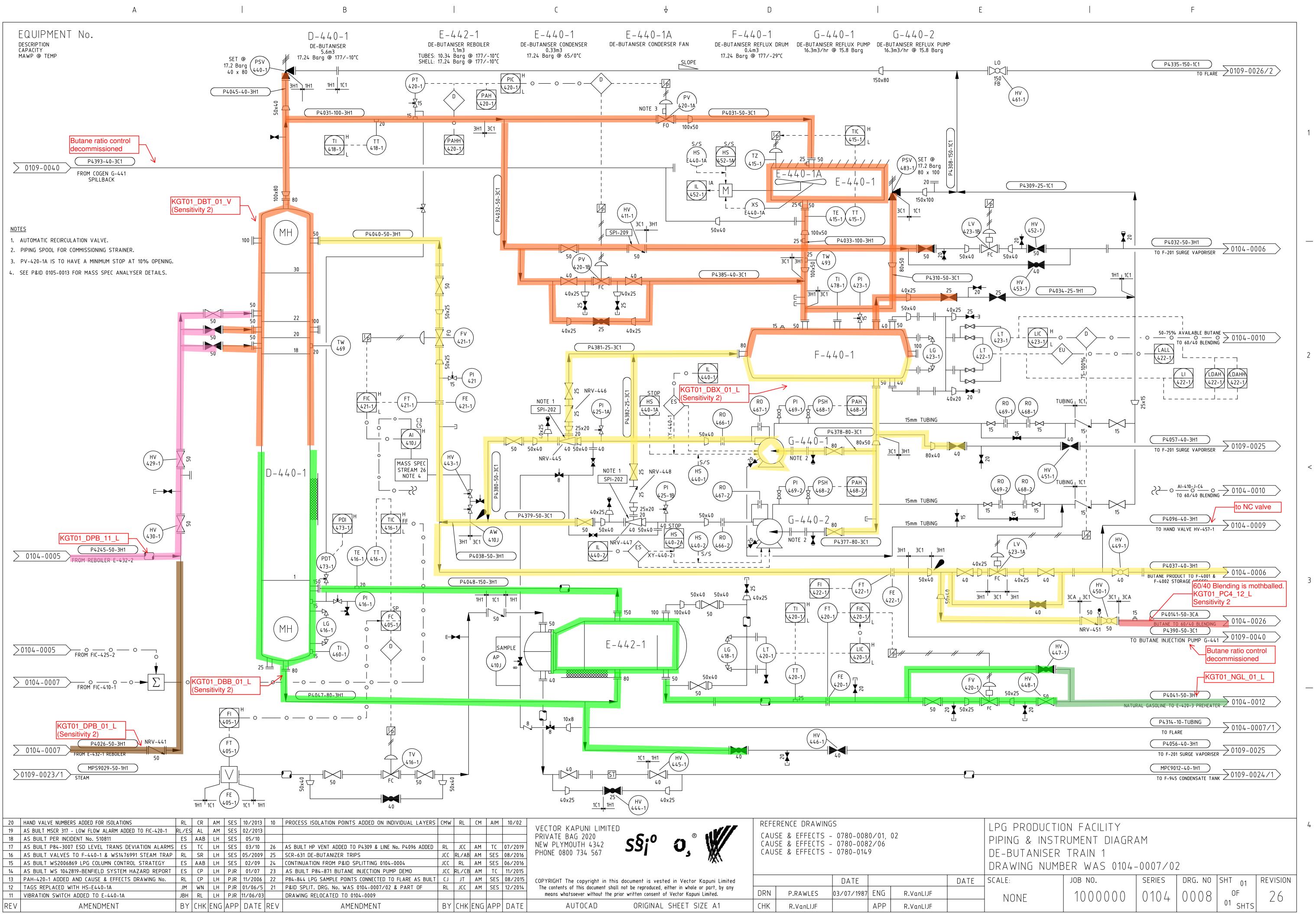


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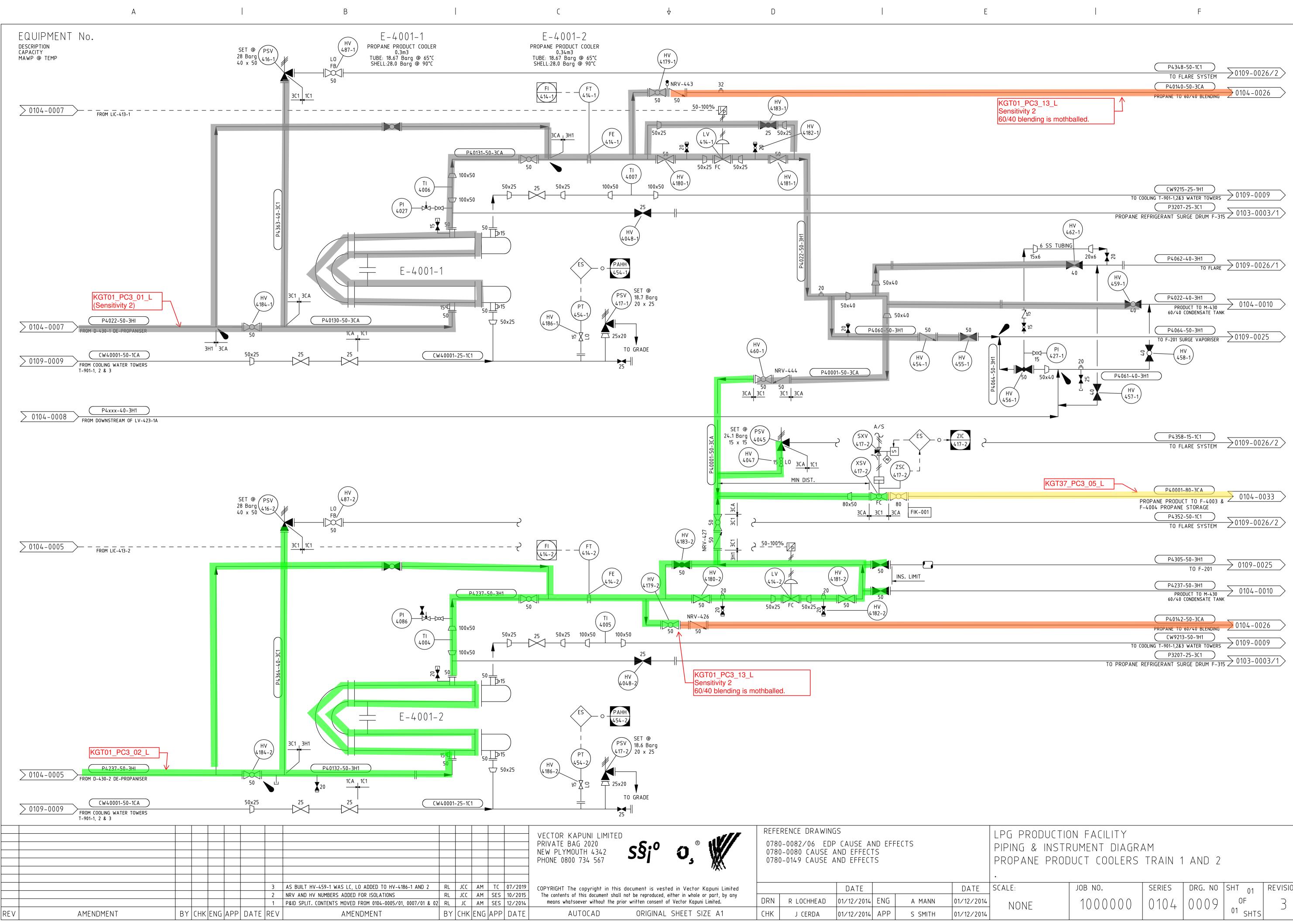


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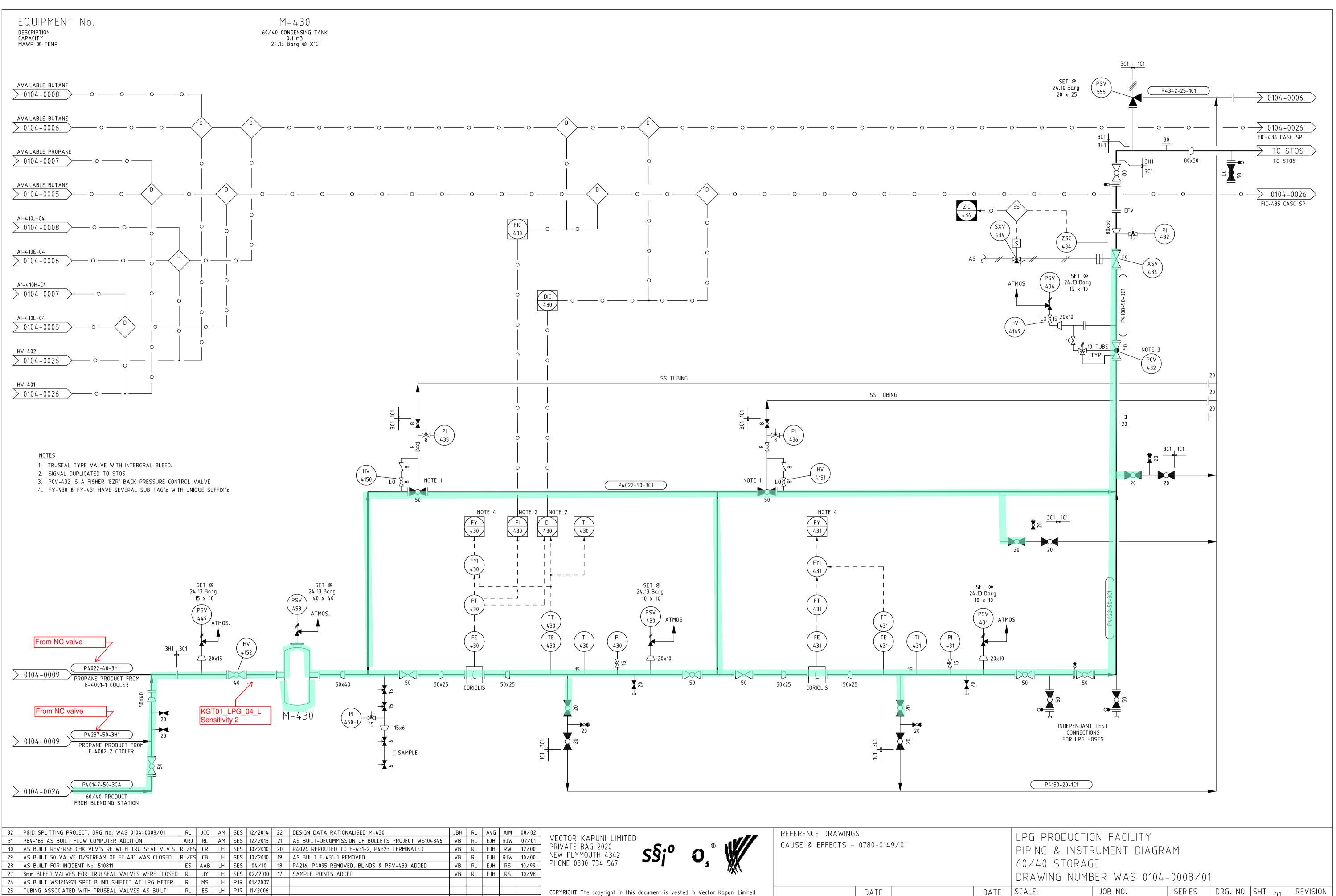
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23 AS BUILT - WS177367 STOS BACK PRESSURE VALVE

AMENDMENT

ES WN LH PJR 10/06

BY CHK ENG APP DATE REV

PL RL LH AIM 01/03 33 HV HAND VALVE NUMBERS ADDED TO LOCKED VALVES RL JCC

AMENDMENT

24 AS BUILT

REV

JBH VB VB VB VB	RL RL RL RL RL	AvG EJH EJH EJH EJH	AIM RJW RW RJW RS	08/02 02/01 12/00 10/00 10/99	VECTOR KAPUNI LIMITE PRIVATE BAG 2020 NEW PLYMOUTH 4342 PHONE 0800 734 567	s§;°	Ĵ,			RENCE DRAWIN E & EFFECTS		9/01			L P 6
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 RL		AM	TC	07/2019	The contents of this document shal means whatsoever without the p				DRN	P.RAWLES	02/07/1987	ENG	R.VanLIJF	02/07/1987	
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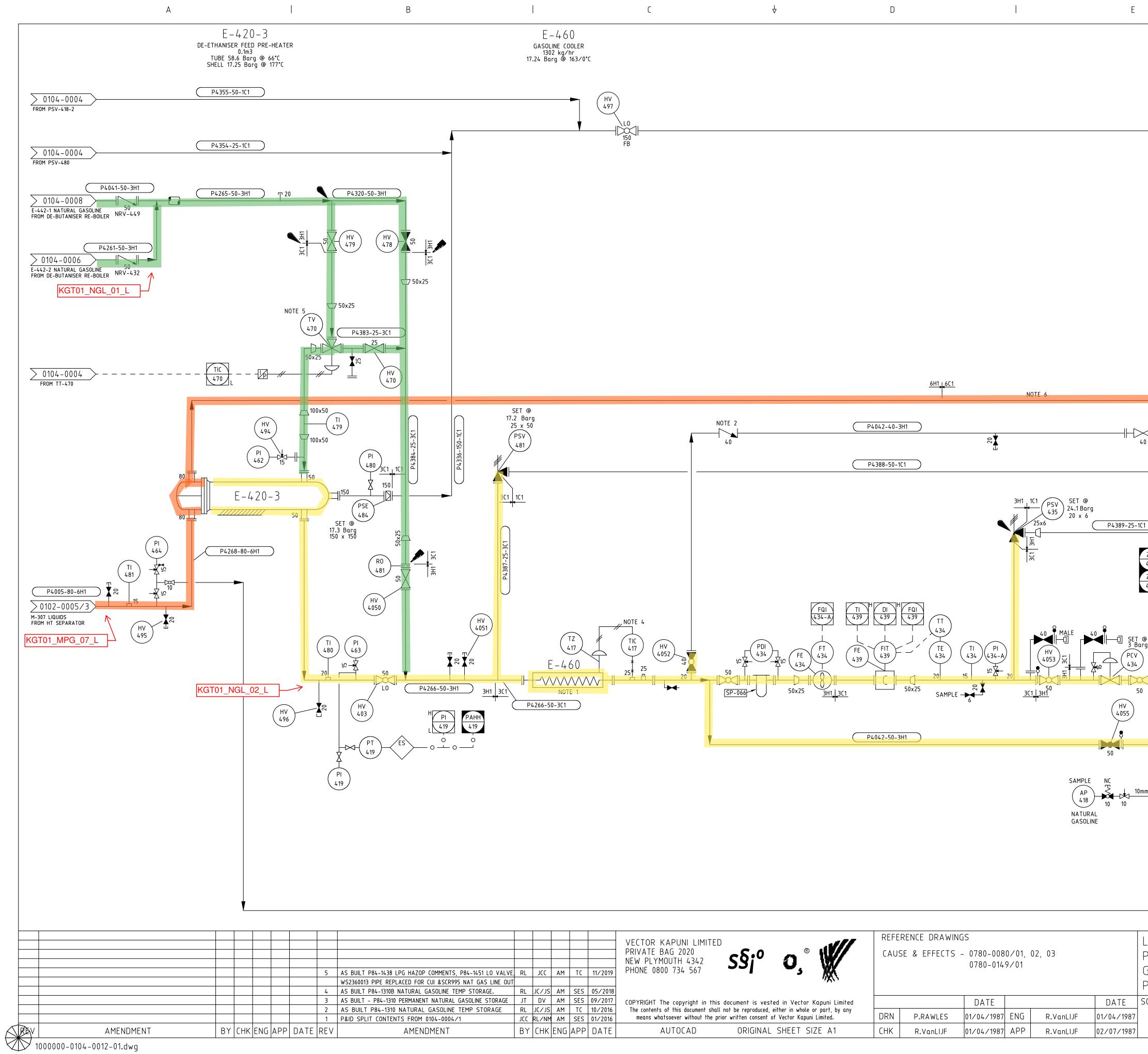
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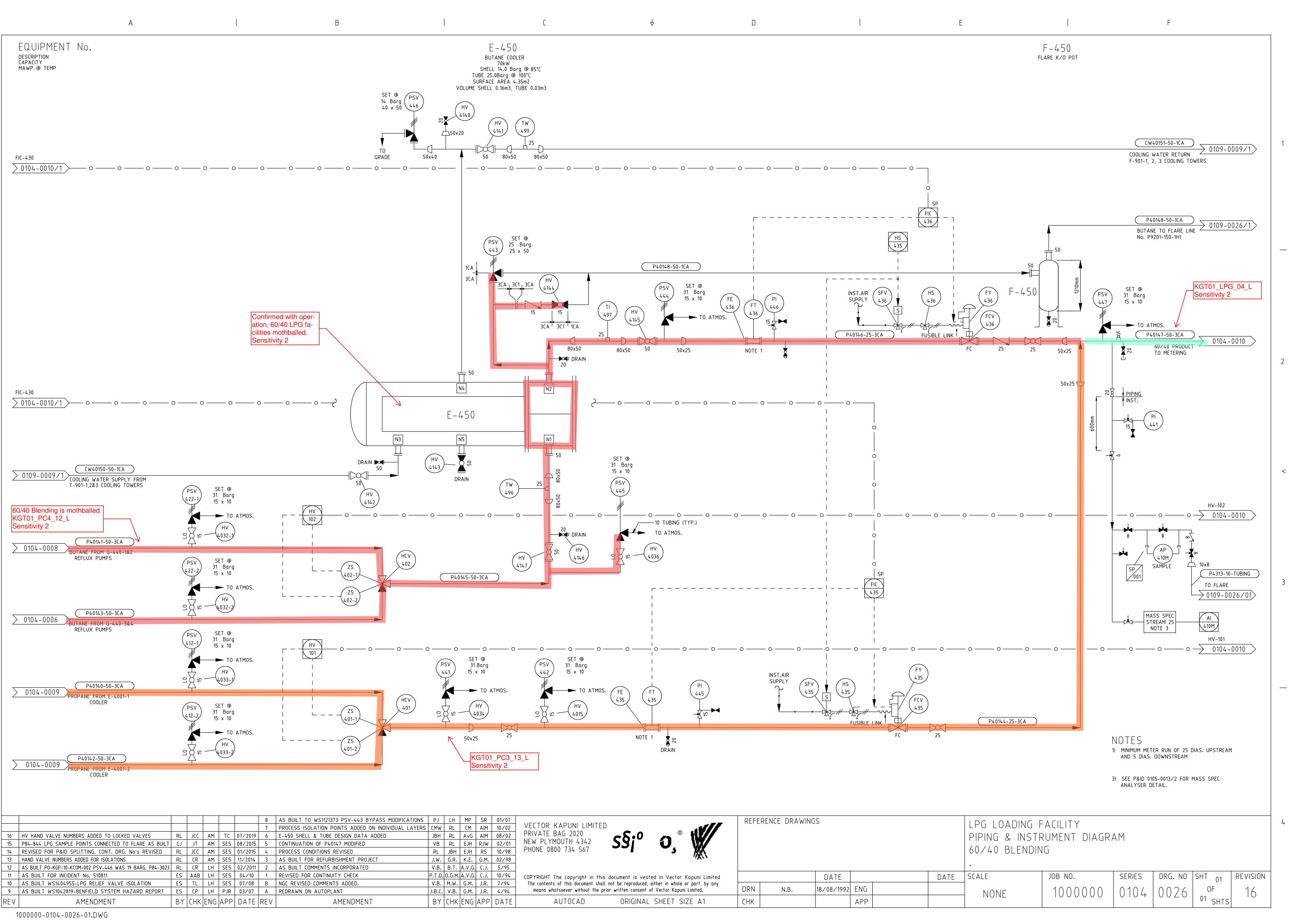
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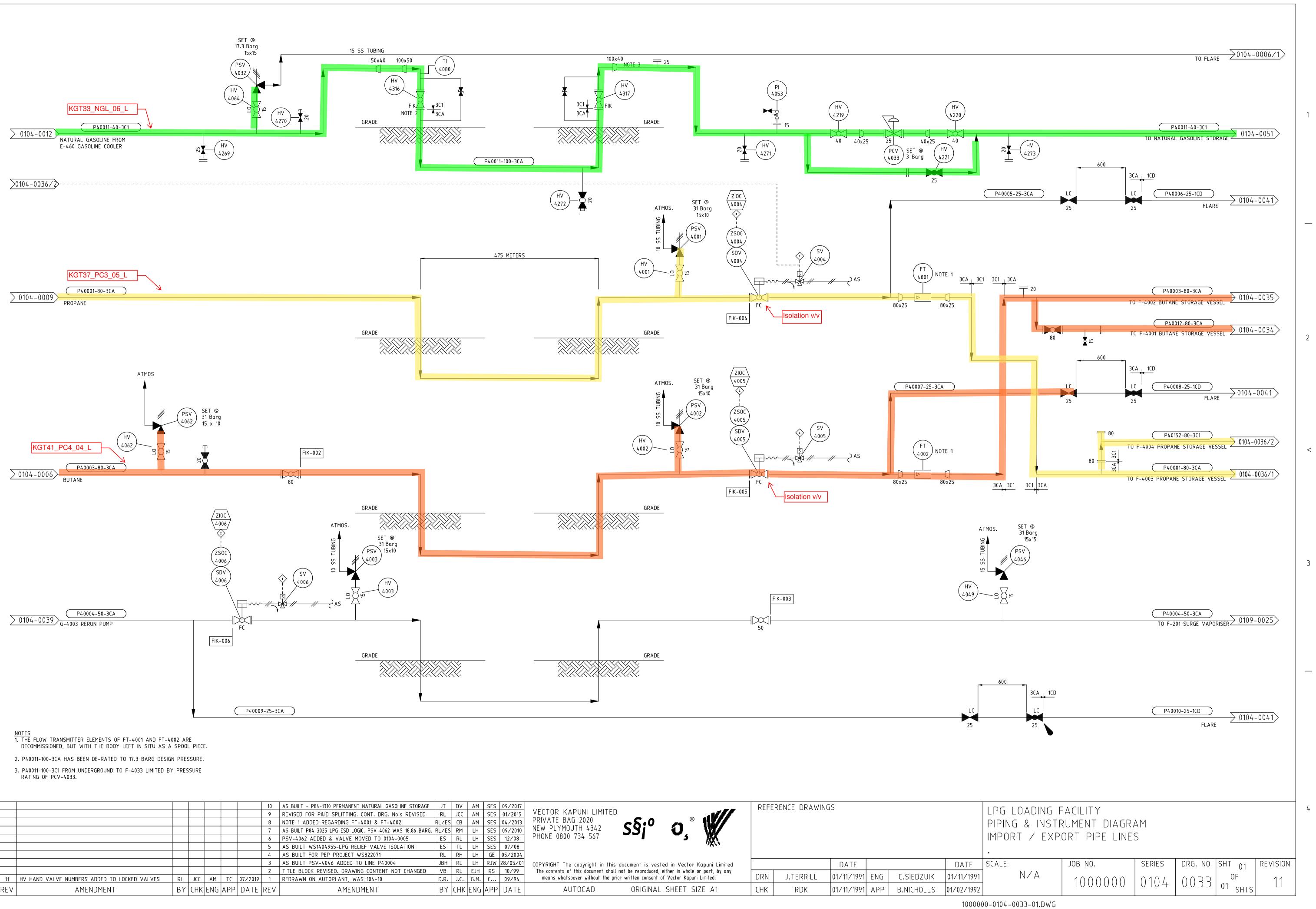
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E - 4 6 () GASOLINE COOLER 1302 kg/hr 17.24 Barg @ 163/0°C HV 497 L0 150 FB	SLOPE (P4336-150-1C1) TO FLARE SYSTEM 0109-0026/2	> 1
	<u>NOTES:</u> 1. DE-PROPANISER CONDENSER FANS (E-430-1A/2B) SERVICE DE-PROPANISER CONDENSER (E-430-1) AND GASOLINE COOLER (E-460) 2. NON-RETURN VALVE TO BE LOCATED IN HORIZONTAL POSITION.	
T@ Barg x 50 SV 81	ALL SAMPLING BOXES (TYPES 1, 2 & 3) IN LPG PRODUCTION FACILITIES ARE TO BE INSTALLED AS PER VENDORS REQUIREMENTS. 4. LOUVERS MANUALLY OPEN 100%. TIC-417 ABANDONED IN SITU. 5. TV-470 FAIL OPEN TO BYPASS. 6. SECTION OF LINE P4207-80-6H1 REPLACED WITH SPEC 6C1 SCH80, W52360013. 611_661 NOTE 6 0104-0004 10 D-420-2 DE-ETHANISER 0109-0025	> 2
1 <u>C1</u>	40 $P4388-50-1(1)$ $HV$ $40$ $HV$ $422$ $42$ $HV$ $422$ $HV$ $42$ $HV$ $HV$ $42$ $HV$ $HV$ $HV$ $HV$ $HV$ $HV$ $HV$ $HV$	> <
NOTE 4 (417) E - 4 6 0 NOTE 1 P4266-50-3C1	$\begin{array}{c} 1.2 \text{ Barg} \\ 1.2 \text{ Barg} \\ 2.0 \\ 4.16 \end{array}$	> 3
	P4.04.2-50-3H1 $P4.04.2-50-3H1$ $P4.04.2-50-3H1$ $P4.04.2-50-3H1$ $FC$ $AP$ $AP$ $AP$ $AP$ $AP$ $AP$ $AP$ $AP$	
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RL JC/JS AM TC 10/2016 The contents of this doce	n this document is vested in Vector Kapuni Limited t shall not be reproduced, either in whole or part, by any the prior written consent of Vector Kapuni Limited. DRN P.RAWLES 01/04/1987 ENG R.VanLIJF 01/04/1987 ORIGINAL SHEET SIZE A1 CHK R.VanLIJF 01/04/1987 APP R.VanLIJF 02/07/1987 PROM 0104-0004-01 JOB NO. SERIES DRG. NO SHT 01 OF 01 OF 01 SHTS O	NC



ł	MP	SR	01/07		DEEE	RENCE DRAWING	c						
<u>.</u>	СМ	AIM	10/02	VECTOR KAPUNI LIMITED		KLINCE DRAWING	13						
-	AvG	AIM	08/02	PRIVATE BAG 2020 NEW PLYMOUTH 4342 DHONE 0800 734 F(7)									
-	EJH	RJW	02/01	NEW PLYMOUTH 4342 SSI O. W							',		
H	EJH	RS	10/98	PHONE 0800 734 567							6		
۲.	K.E.	G.M.	02/98	/AN1									
Γ.	A.V.G.	C.J.	5/95								۰		
Μ.	A.V.G.	C.J.	10/94	COPYRIGHT The copyright in this document is vested in Vector Kapuni Limited			DATE			DATE	S		
٧.	G.M.	J.R.	7/94	The contents of this document shall not be reproduced, either in whole or part, by any									
3.	G.M.	J.R.	4/94	means whatsoever without the prior written consent of Vector Kapuni Limited.	DRN	N.B.	18/08/1992	ENG					
Κ	ENG	APP	DATE	AUTOCAD ORIGINAL SHEET SIZE A1	СНК			APP					



				10	AS BUILT - P84-1310 PERMANENT NATURAL GASOLINE STORAGE	JT	DV AM	SES	09/2017		REFE	RENCE DRAWING	īS				
				9	REVISED FOR P&ID SPLITTING. CONT. DRG. No's REVISED	RL	JCC AM	SES	01/2015	VECTOR KAPUNI LIMITED							
				8	NOTE 1 ADDED REGARDING FT-4001 & FT-4002	RL/ES	CB AM	SES	04/2013	VECTOR KAPUNI LIMITED PRIVATE BAG 2020 S.O							P
				7	AS BUILT P84-3025 LPG ESD LOGIC. PSV-4062 WAS 18.86 BARG.	RL/ES	RM LH	SES	09/2010	NEW PLIMUUTH 4342 SSI U UN							
				6	PSV-4062 ADDED & VALVE MOVED TO 0104-0005	ES	RL LH	SES	12/08	PHONE 0800 734 567							
				5	AS BUILT WS1404955-LPG RELIEF VALVE ISOLATION	ES	TL LH	SES	07/08								
				4	AS BUILT FOR PEP PROJECT WS822071	RL	RH LH	GE	05/2004							<b>.</b>	•
				3	AS BUILT PSV-4046 ADDED TO LINE P40004	JBH	RL LH	RJW	28/05/01	COPYRIGHT The copyright in this document is vested in Vector Kapuni Limited			DATE			DATE	SC
				2	TITLE BLOCK REVISED. DRAWING CONTENT NOT CHANGED	VB	RL EJ⊦	RS	10/99	The contents of this document shall not be reproduced, either in whole or part, by any							_
11	HV HAND VALVE NUMBERS ADDED TO LOCKED VALVES	RL	JCC AM TC	07/2019 1	REDRAWN ON AUTOPLANT, WAS 104-10	D.R.	J.C. G.M	. C.J.	09/94	means whatsoever without the prior written consent of Vector Kapuni Limited.	DRN	J.TERRILL	01/11/1991	ENG	C.SIEDZUIK	01/11/1991	
REV	AMENDMENT	BY	CHK ENG APP	DATE REV	AMENDMENT	ΒY	CHK ENG	i APP	DATE	AUTOCAD ORIGINAL SHEET SIZE A1	СНК	RDK	01/11/1991	APP	B.NICHOLLS	01/02/1992	,

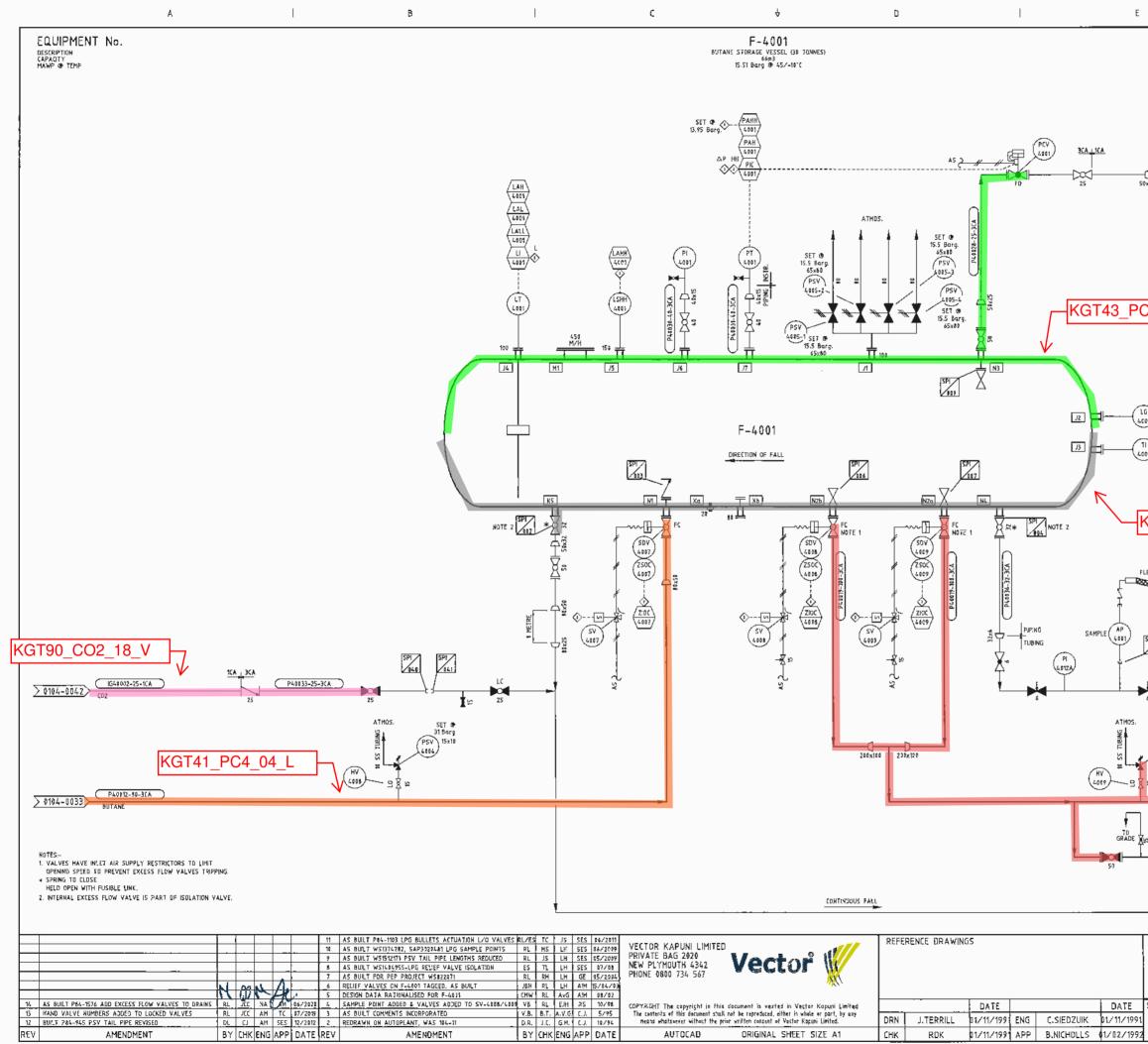






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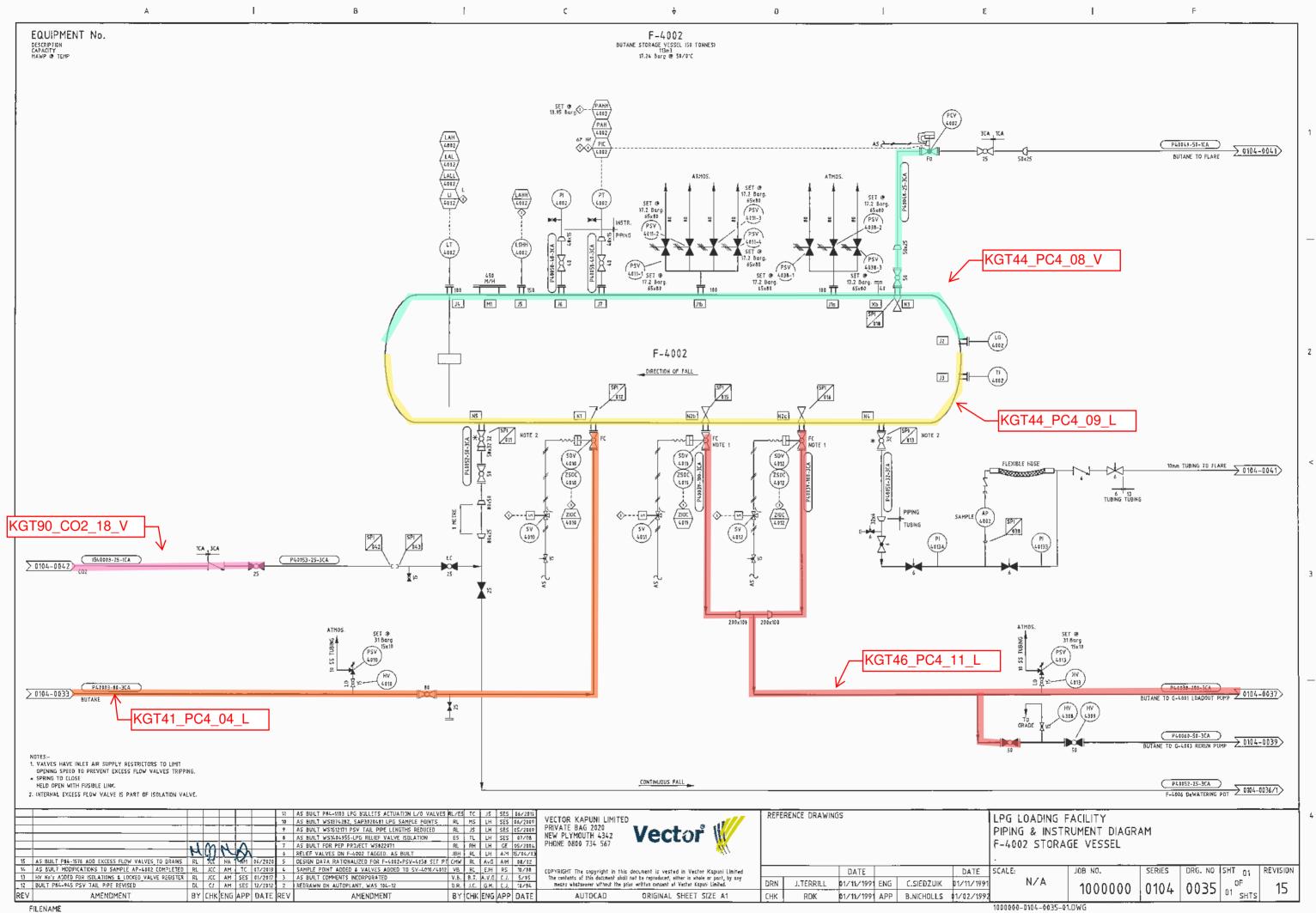
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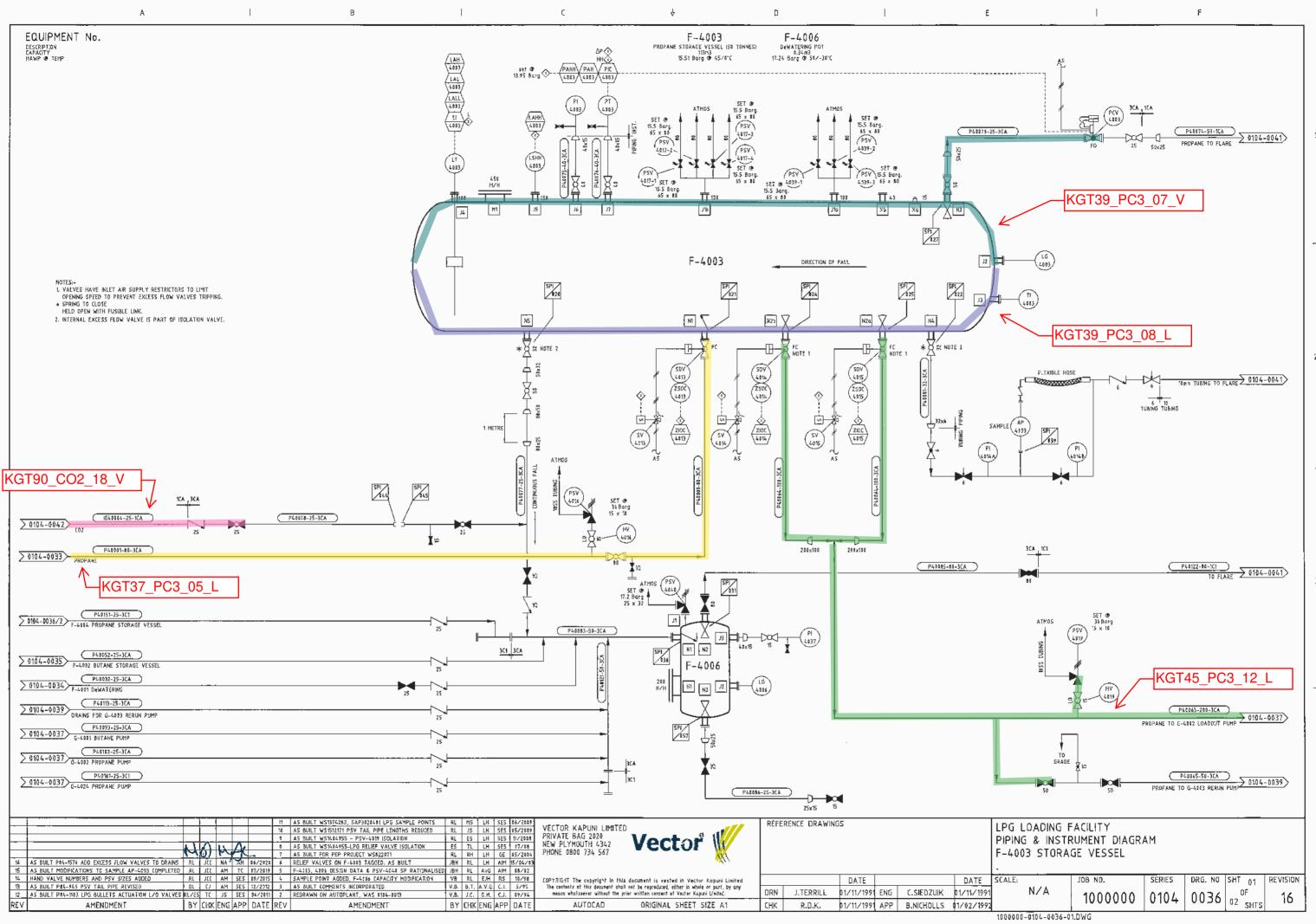


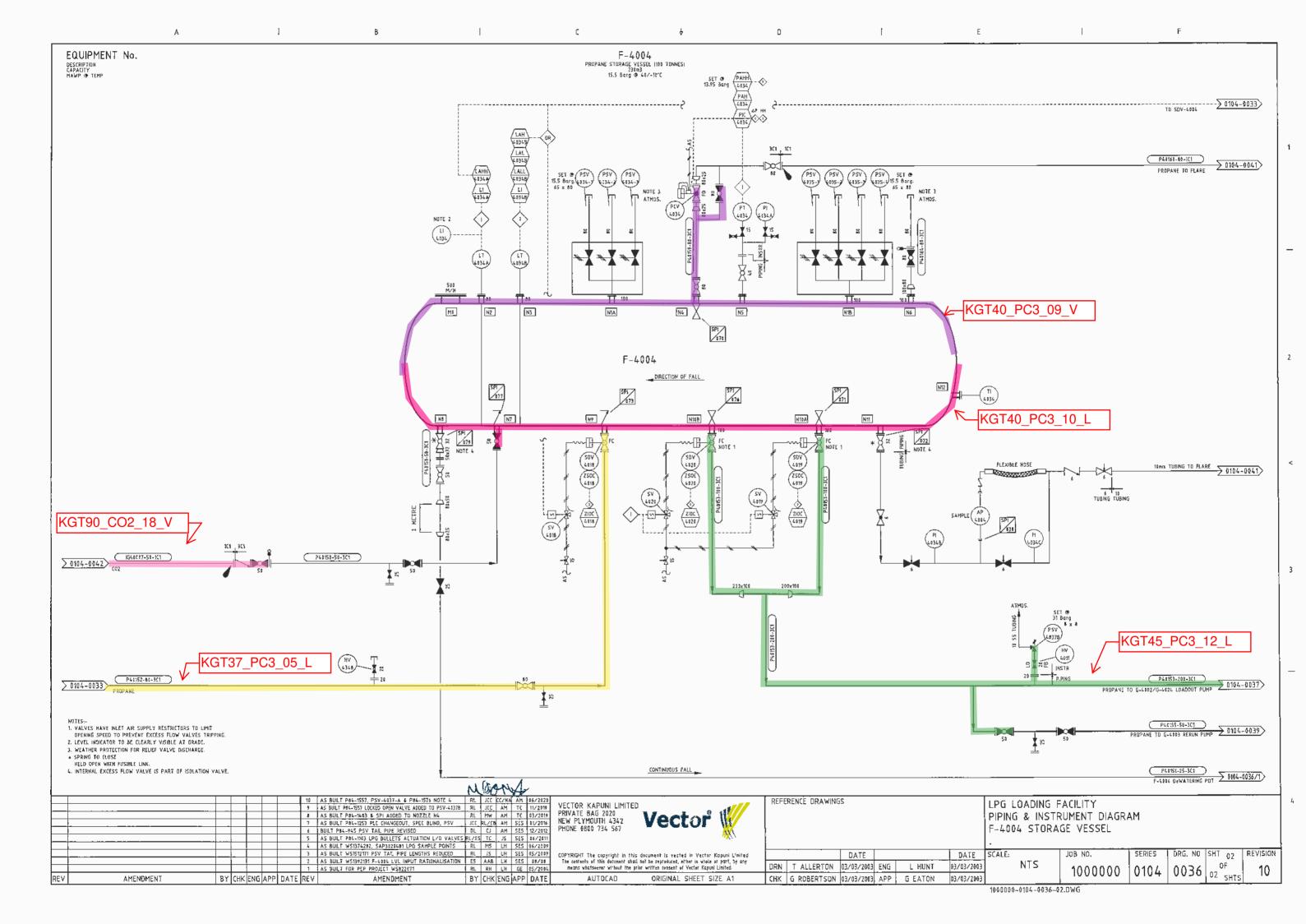
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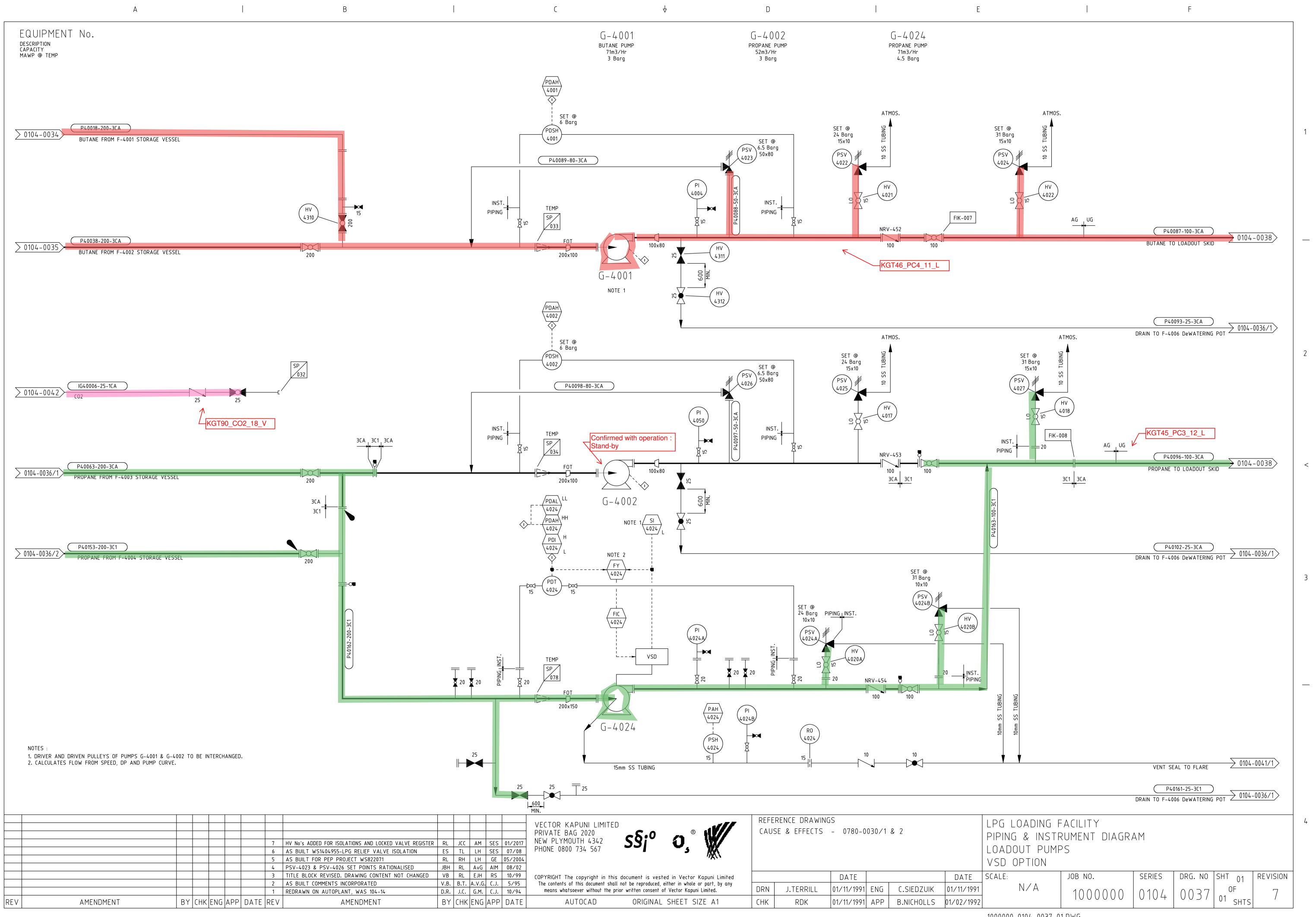
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SET * 31 Bars PSV IS 10 KGT46_PC4_11_L PADDM 280-3CA BUTANE TO G-4801 LOADOUT PUMP	
P4.1020-50-3CA           BUTAME TO G-4003 RERUN PUMP           50           P4.0132-25-3CA           F-4006 DeWATERNG POT	04-0039
LPG LOADING FACILITY PIPING & INSTRUMENT DIAGRAM F-4001 STORAGE VESSEL SCALE: JOB ND. SERIES DRG. ND SHT O	4
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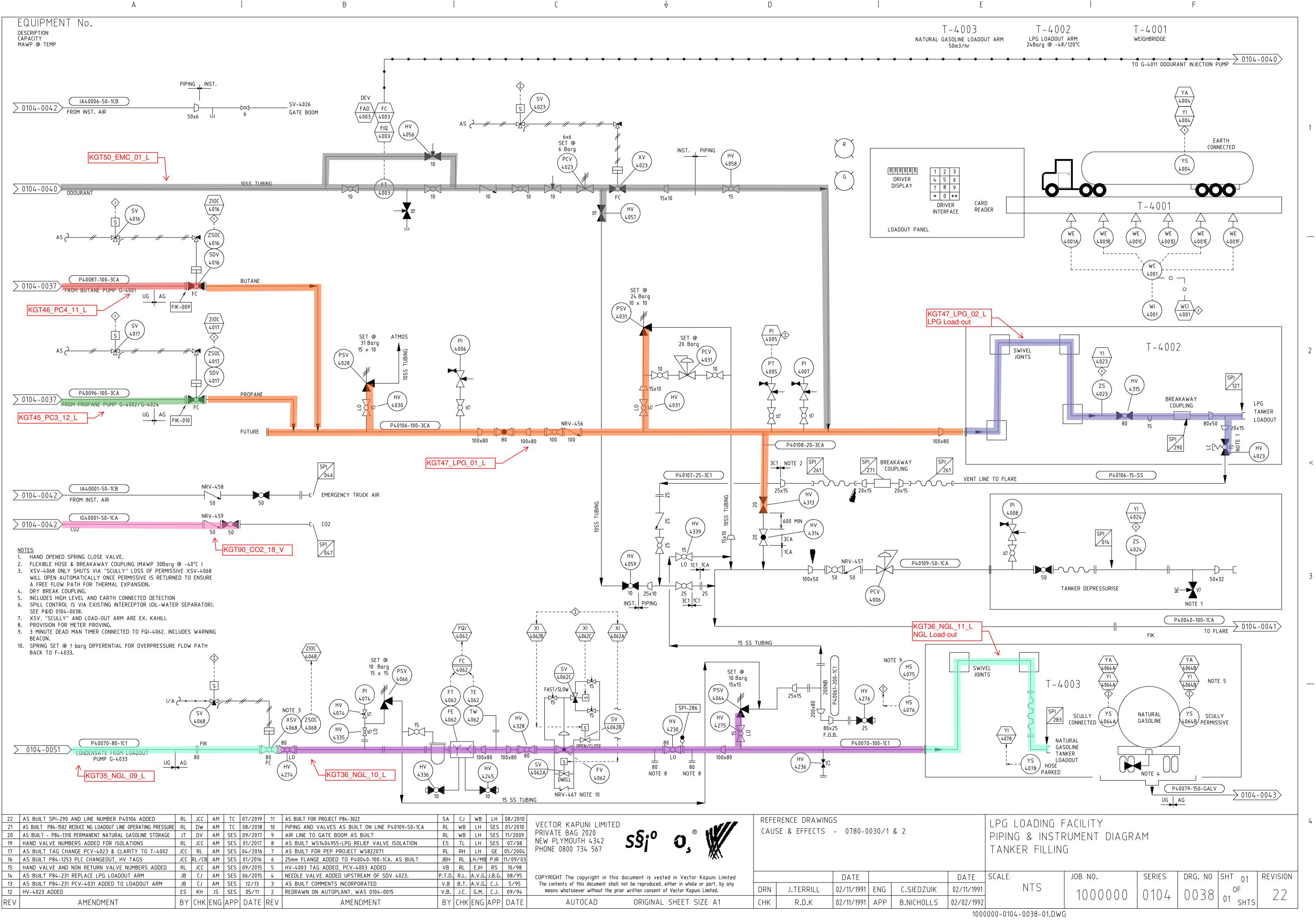








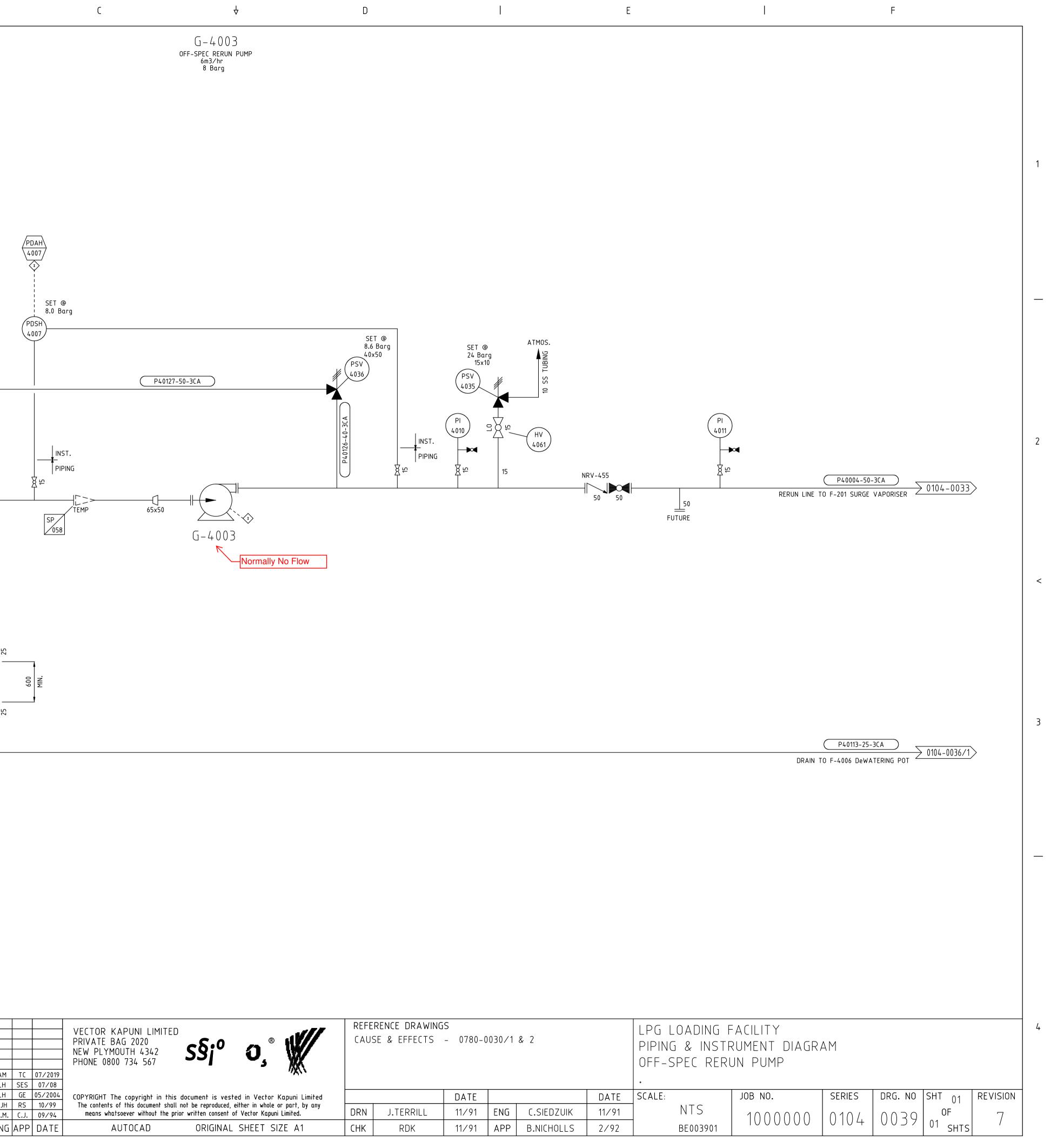
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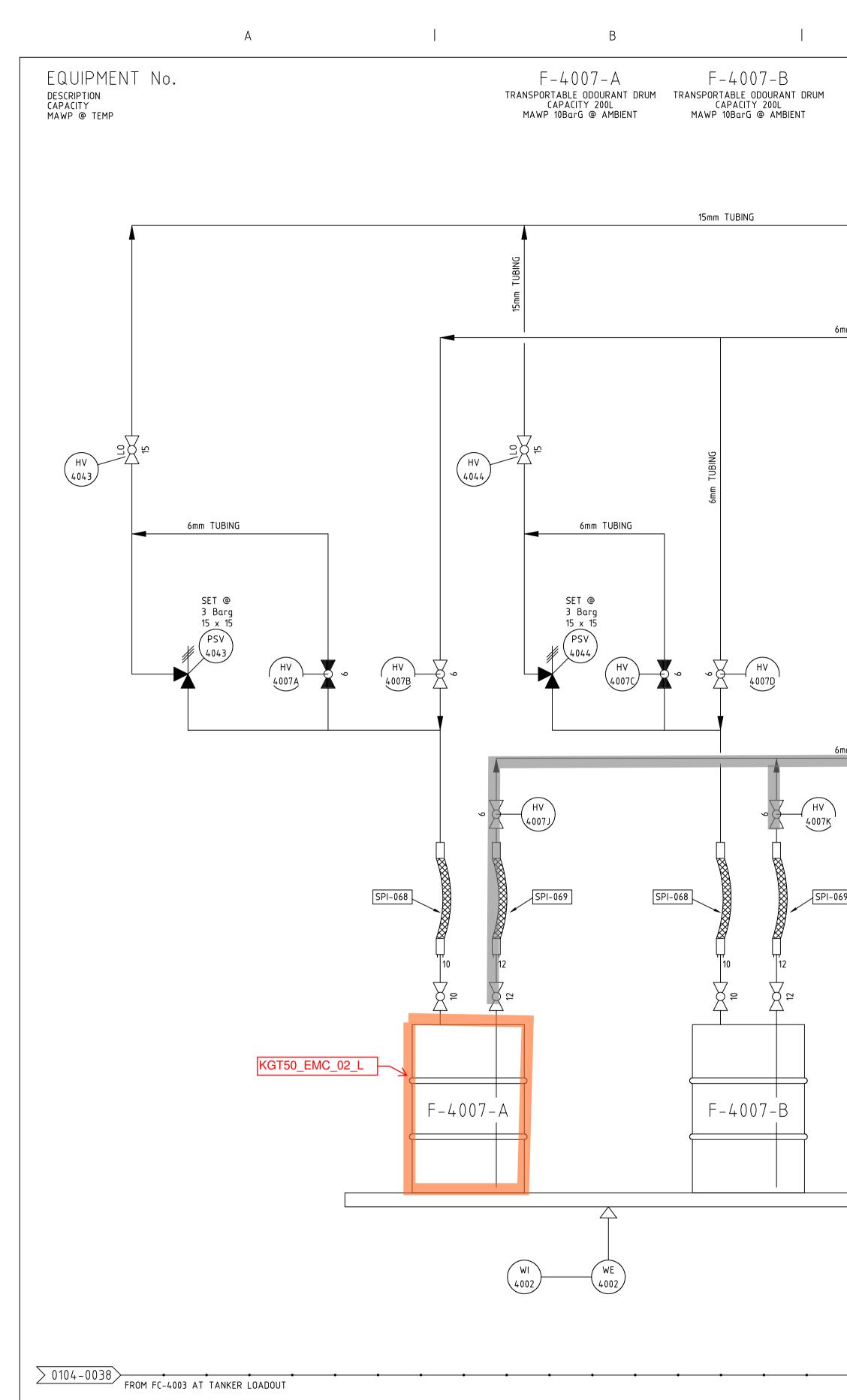


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	LH	GE	05/2004	PHONE 0800 734 567							
	LH/ME	PJR	11/09/03	7 <b>X</b> \\							
	EJH	RS	10/98								
•	A.V.G	J.B.G.	08/95	COPYRIGHT The copyright in this document is vested in Vector Kapuni Limited			DATE			DATE	S
•	A.V.G.	C.J.	5/95	The contents of this document shall not be reproduced, either in whole or part, by any							
	G.M.		09/94	means whatsoever without the prior written consent of Vector Kapuni Limited.	DRN	J.TERRILL	02/11/1991	ENG	C.SIEDZUIK	02/11/1991	
K	ENG	APP	DATE	AUTOCAD ORIGINAL SHEET SIZE A1	СНК	R.D.K	02/11/1991	APP	B.NICHOLLS	02/02/1992	
										1000	

A EQUIPMENT No. DESCRIPTION CAPACITY MAWP @ TEMP		В	C	G − 4003 OFF-SPEC RERUN PUMP 6m3/hr 8 Barg	D I E
	= ■ 15 3 4 15 5 15 15 15 15 15 15 15 15	ATMOS.	PDAH 4007 T SET @ 8.0 Barg PDSH 4007		SET @ 8.6 Barg 40x50 PSV SET @ 24 Barg 15x10 SET @ 24 Barg
P40065-50-3CA         PROPANE FROM F-4003 STORAGE VESSEL         0104-0036/2         P40155-50-3C1         PROPANE FROM F-4004 STORAGE VESSEL         3C1         P40119-50-3C1	3CA P40119-50-3CA	SET @ JIBarg 31 Barg 15x10 PSV 4033 PFV 4060 15 50	INST. PIPING	P40127-50-3CA 65x50 $G-4003$ Normally No Flow	VE-07-95107 VE-07
			25 600 MIN.		
	6     AS BUIL       5     AS BUIL	D VALVE NUMBERS ADDED TO LOCKED VALVES T WS1404955-LPG RELIEF VALVE ISOLATION T FOR PEP PROJECT WS822071 LOCK REVISED. DRAWING CONTENT NOT CHANGED	RL         JCC         AM         TC         07/2019           ES         TL         LH         SES         07/08	AG 2020 OUTH 4342 0 734 567 Me copyright in this document is vested in Vector Kapuni Limi of this document shall not be reproduced, either in whole or part, by of tsoever without the prior written consent of Vector Kapuni Limited.	•







							8	AS BUILT P84-1375 ADDITION SPI-288 & 3 HV No's ADDED	RL	JC
							7	AS BUILT WS2060791 REPLACE ODORANT INJECTION PUMP	RL	MK
							6	NOTE 3 ADDED REGARDING STATUS OF PSV-4049	RL	MK
							5	AS BUILT FOR WS145015 TRANSPOR. ODOURANT DRUMS	VB	RL
							4	TITLE BLOCK REVISED. DRAWING CONTENT NOT CHANGED	VB	RL
							3	AS BUILT COMMENTS INCORPORATED	V.B.	B.T.
							2	REDRAWN ON AUTOPLANT, WAS 0104-0017	V.B.	J.C.
REV	AMENDMENT	ΒY	СНК	ENG	APP	DATE	REV	AMENDMENT	ΒY	СНК

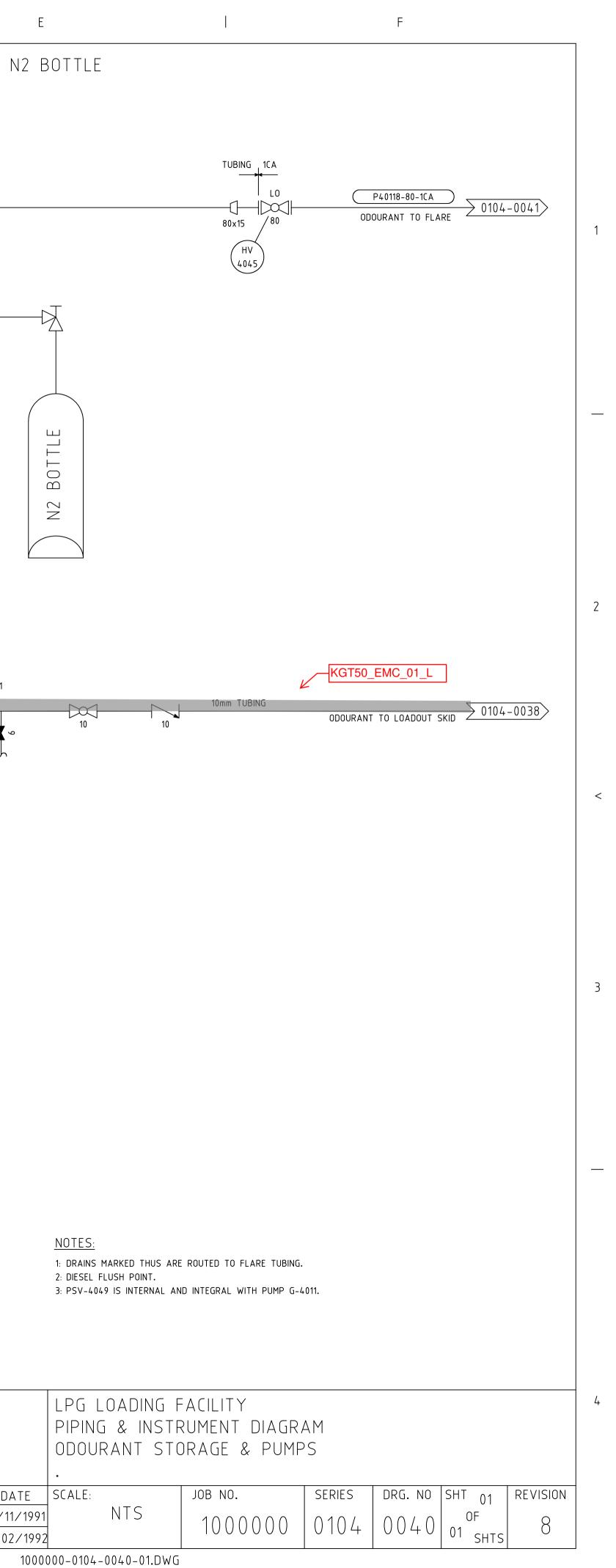
			G – 4011 ODOURANT INJECTION PUMP 1.9-66 l/hr 0-123 Barg 0.37kW	N2 B07
		ODOURANT BUILDIN	١G	
6mm TUBING	PI 4018	ATMOS 4042 6		PI 4015 FCV 4007
HV 4007E	NOTE 1 J HV 4007F VG 4001			SET @ 1.0 Barg
6mm TUBING		HV 4007I 6 HV 4007M NOTE 1	SPI-288 6 BSP G = 4 0 11	PI 4017B NOTE 1
069				

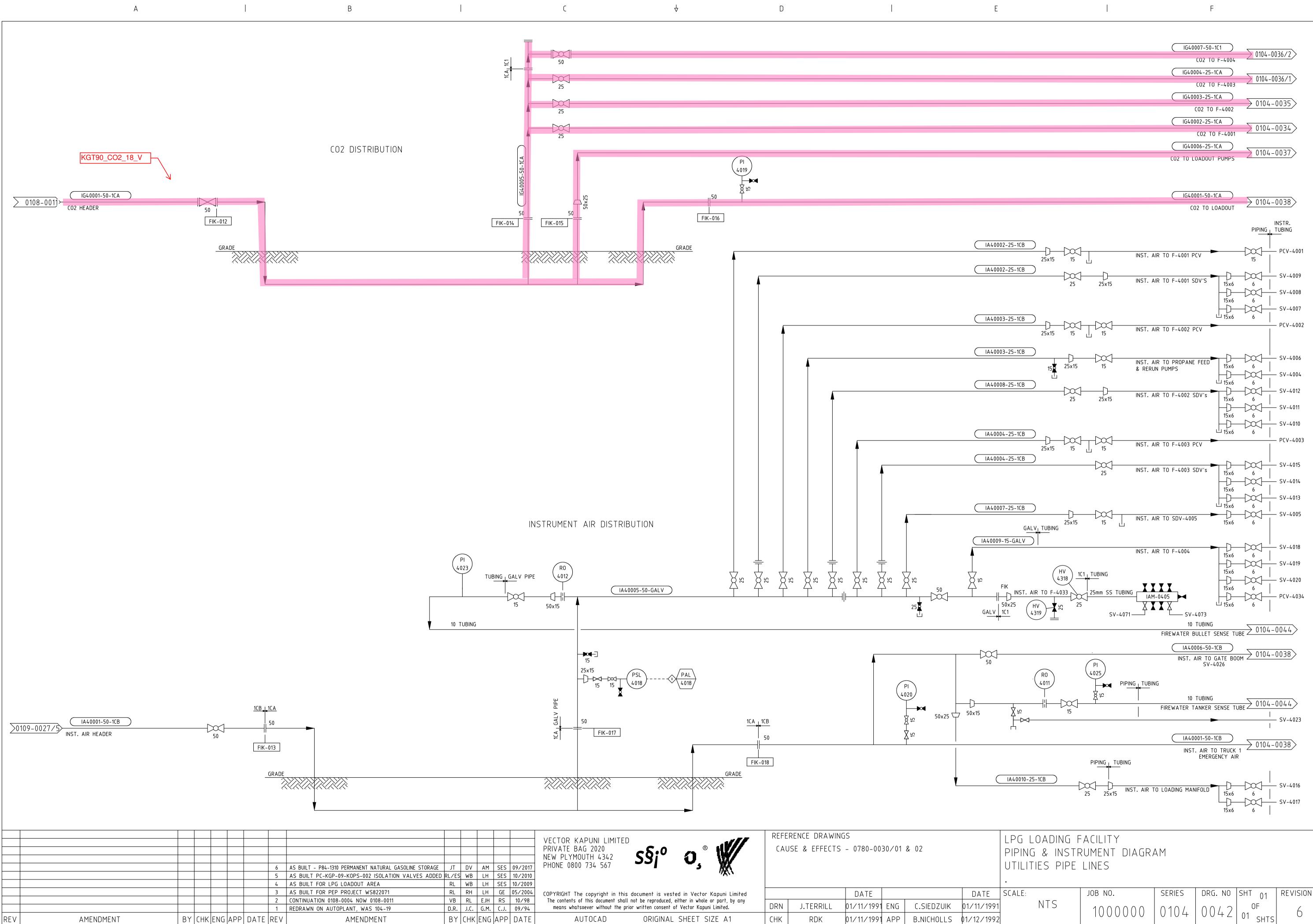
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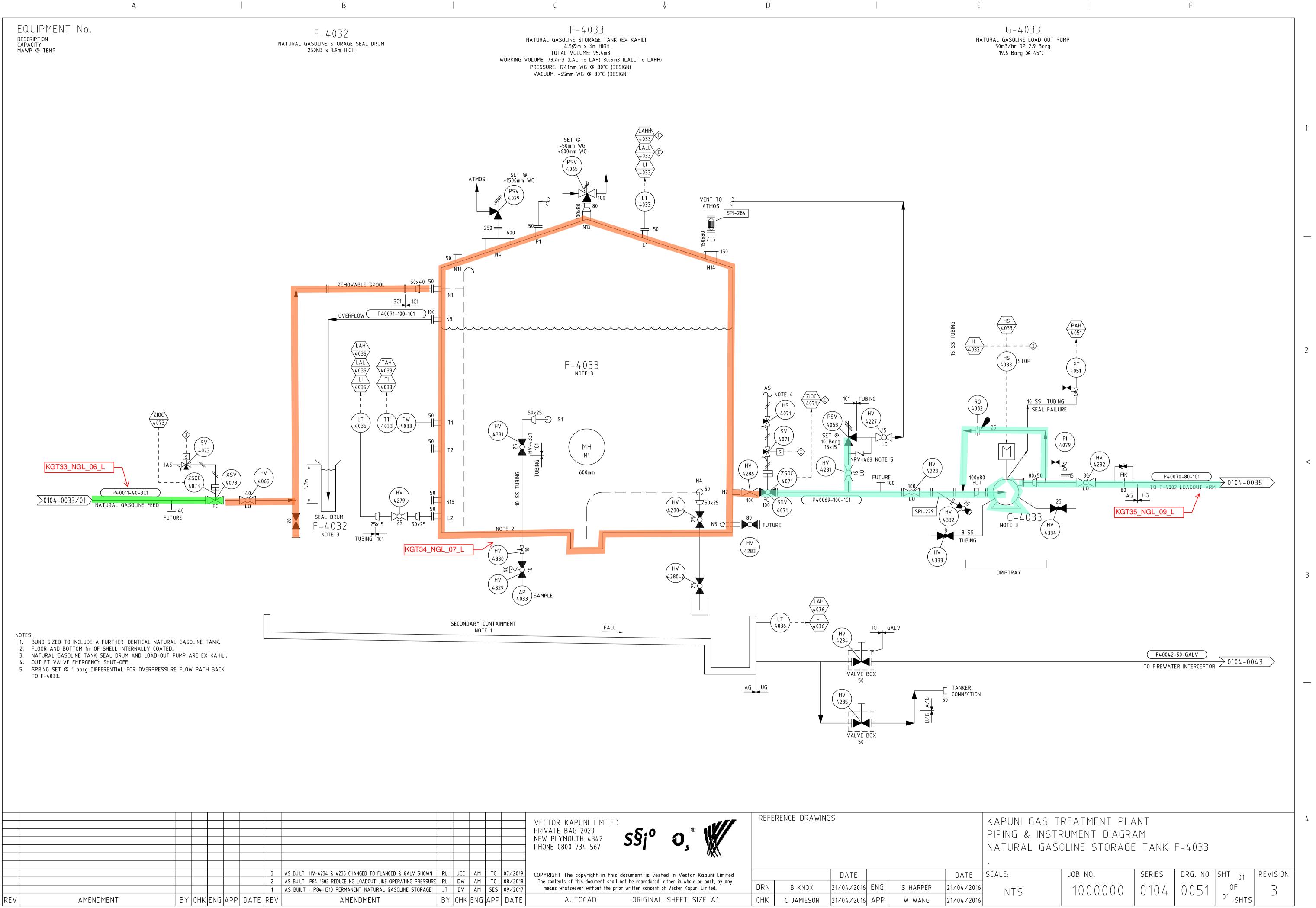
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AM	SES	07/2013	"X\\						
LH	RJW	05/01							
EJH	RS	10/99	COPYRIGHT The copyright in this document is vested in Vector Kapuni Limited			DATE			DATE
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ENG	APP	DATE	AUTOCAD ORIGINAL SHEET SIZE A1	СНК	R.D.K.	01/11/1991	APP	B.NICHOLLS	01/02/1992
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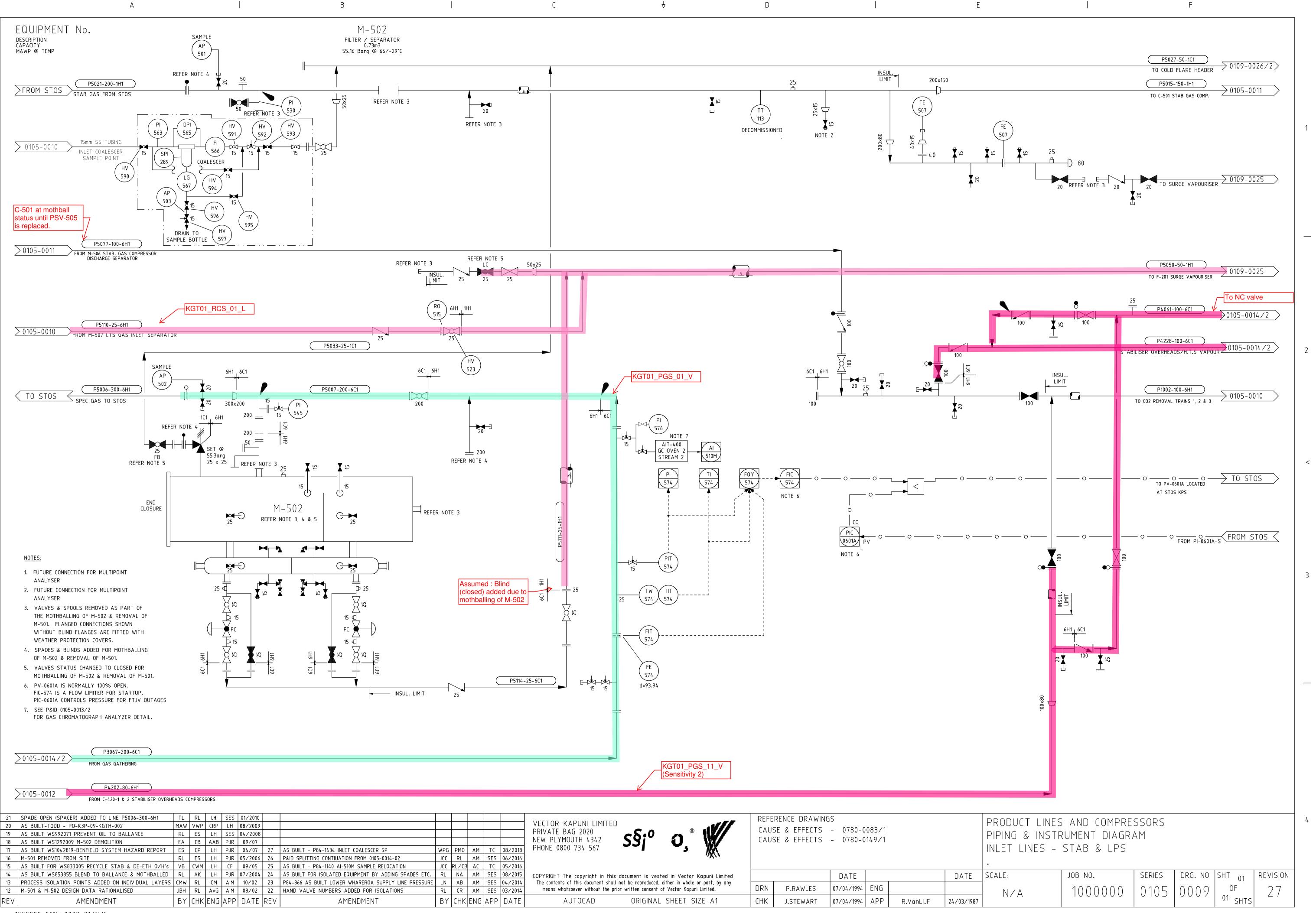
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	AM	SES	09/2017	means whatsoever without the prior written consent of Vector Kapuni Limited.	DRN	B KNOX	21/04/2016	ENG	S HARPER	21/04/2016	
<	ENG	APP	DATE	AUTOCAD ORIGINAL SHEET SIZE A1	СНК	C JAMIESON	21/04/2016	APP	W WANG	21/04/2016	

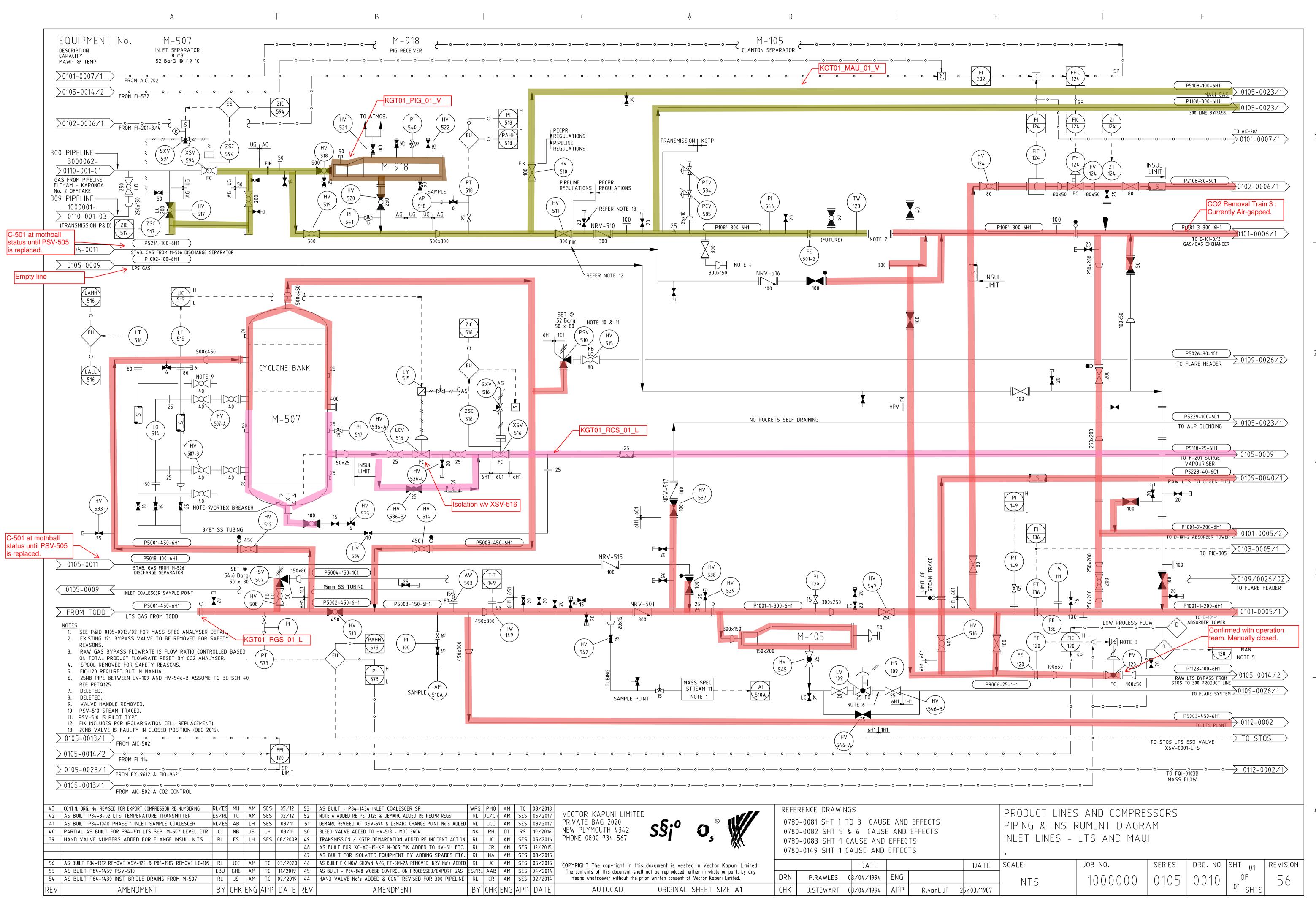


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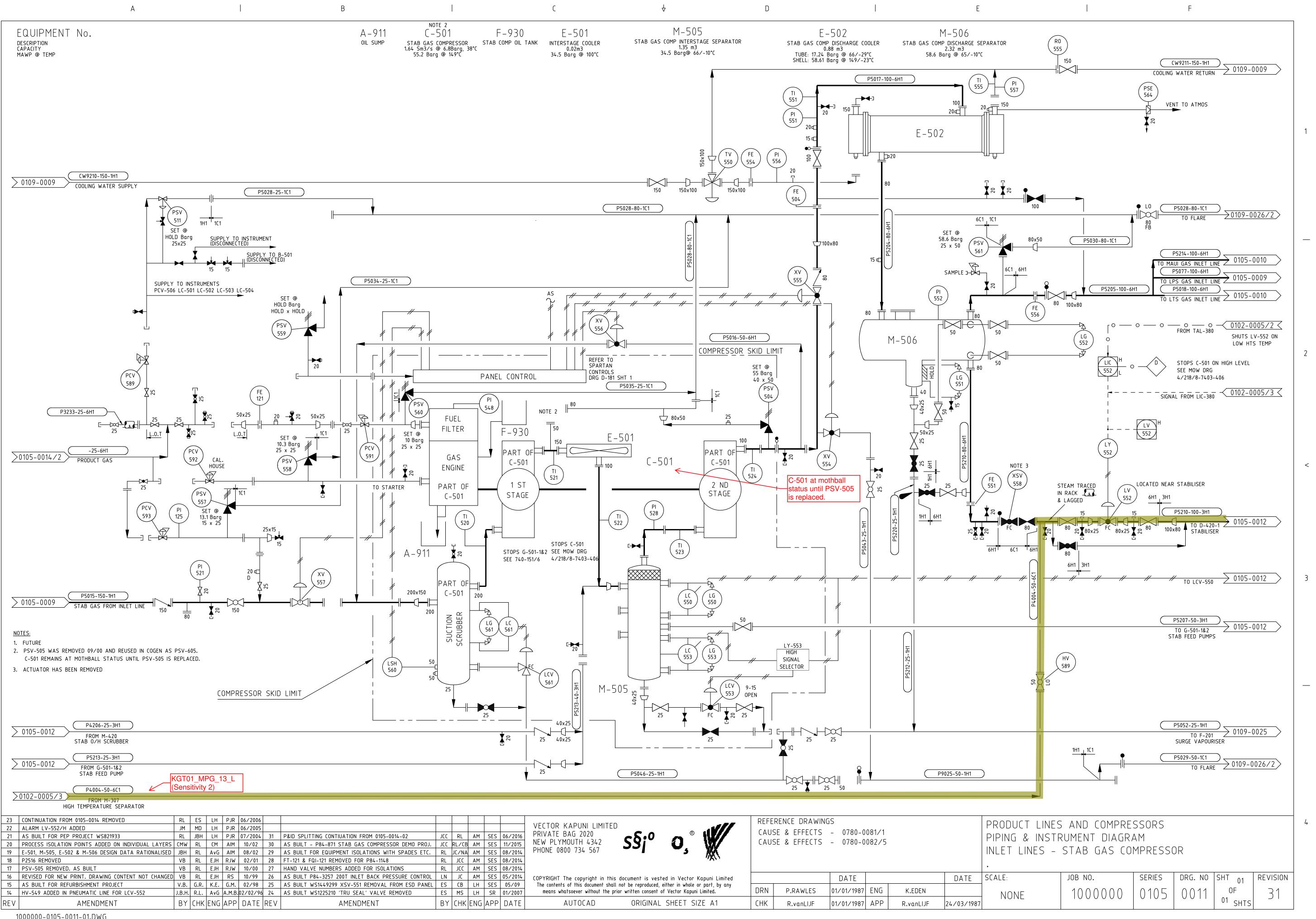
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AM	SES	04/2014	The contents of this document shall not be reproduced, either in whole or part, by any							
AM	SES	03/2014	means whatsoever without the prior written consent of Vector Kapuni Limited.	DRN	P.RAWLES	07/04/1994	ENG			
ENG	APP	DATE	AUTOCAD ORIGINAL SHEET SIZE A1	СНК	J.STEWART	07/04/1994	APP	R.VanLIJF	24/03/1987	
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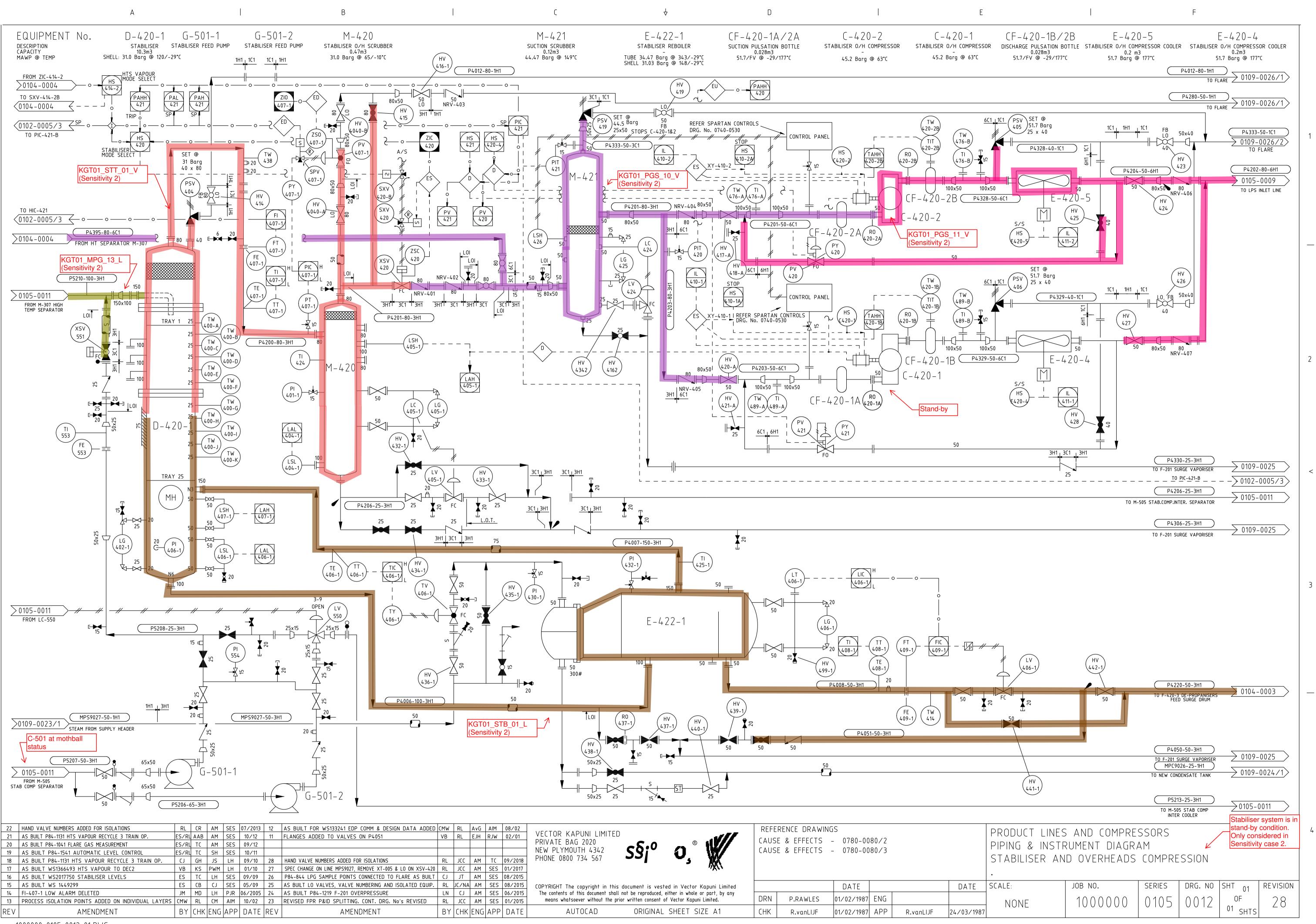
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	AM	SES	03/2017	VECTOR KAPUNI LIMITED PRIVATE BAG 2020	780-0081 SHT 1 TO 3 CA			Ρ
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	AM	SES	05/2016	PHONE 0800 734 567	780-0083 SHT 1 CAUSE A	ND EFFECTS		IN
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	ENG	APP	DATE	AUTOCAD ORIGINAL SHEET SIZE A1	J.STEWART 08/04/199	04 APP R.vanLIJF 25/	/03/1987	



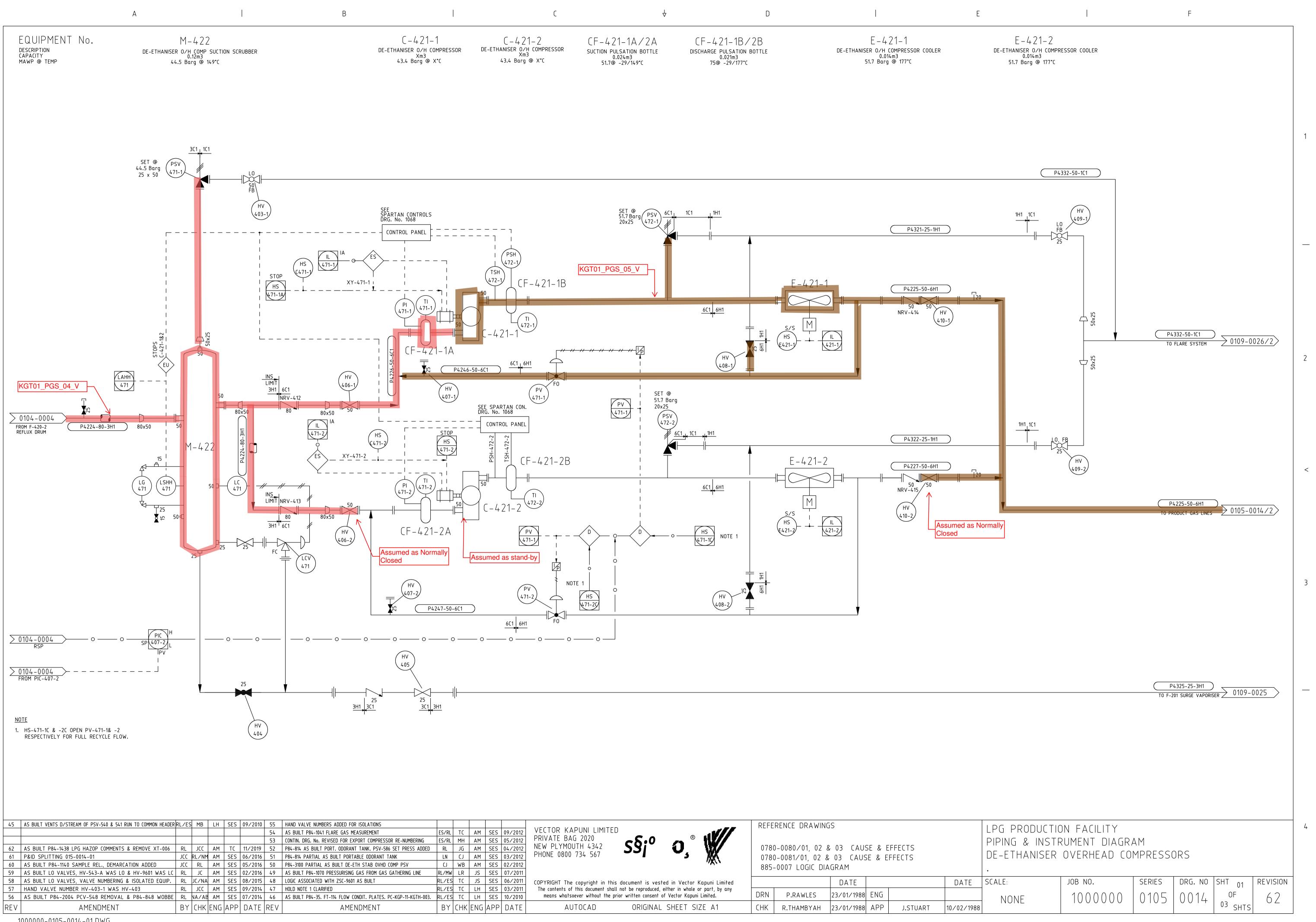
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ΒY	СНК	ENG	APP	DATE	AUTOCAD	ORIGINAL	SHEET SI	ZE A1	СНК	R.vanLIJF	01/01/1987	APP	R.vanLIJF	24/03/1987	



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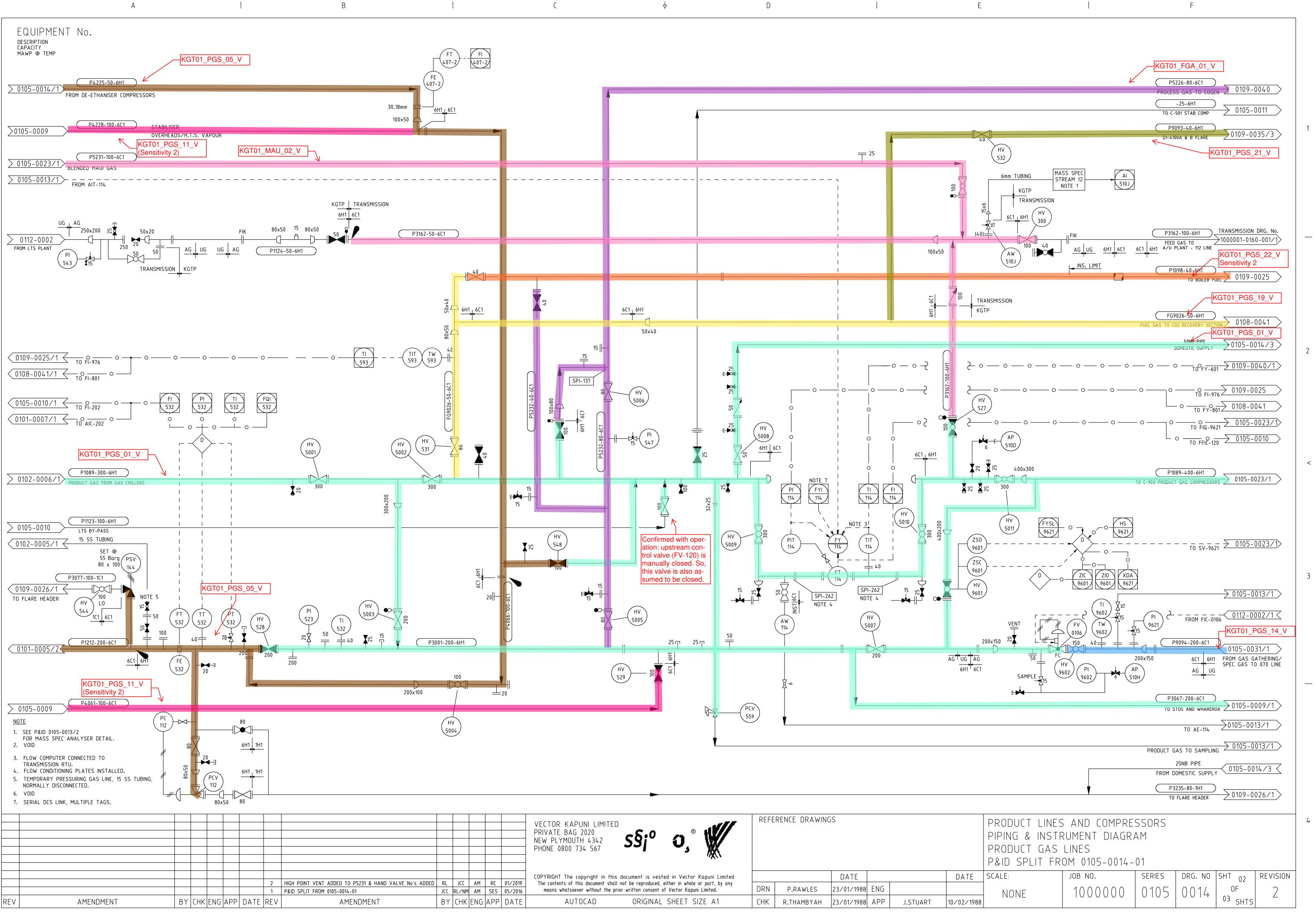
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ENG	APP	DATE	AUTOCAD ORIGINAL SHEET SIZE A1	СНК	R.vanLIJF	01/02/1987	APP	<b>R.vanLIJF</b>	24/03/1987



45	AS BUILT VENTS D/STREAM OF PSV-540 & 541 RUN TO COMMON HEADER RL/ES MB LH SES 09/2010	5 HAND VALVE NUMBERS ADDED FOR ISOLATIONS		REFERENCE DRAWINGS	
		AS BUILT P84-1041 FLARE GAS MEASUREMENT ES/RL TC AM SES 09/2012	VECTOR KAPUNI LIMITED		L
		3 CONTIN. DRG. No. REVISED FOR EXPORT COMPRESSOR RE-NUMBERING ES/RL MH AM SES 05/2012	VECTOR KAPUNI LIMITED PRIVATE BAG 2020 NEW PLYMOUTH 4342 DHONE 0800 734 567		P
62	2 AS BUILT P84-1438 LPG HAZOP COMMENTS & REMOVE XT-006 RL JCC AM TC 11/2019	2 P84-814 AS BUILT PORT. ODORANT TANK. PSV-586 SET PRESS ADDED RL JG AM SES 04/2012	NEW PLYMOUTH 4342 SSI O W	0780-0080/01, 02 & 03 CAUSE & EFFECTS	
61	1 P&ID SPLITTING 015-0014-01 JCC RL/NM AM SES 06/2016	1 P84-814 PARTIAL AS BUILT PORTABLE ODORANT TANK LN CJ AM SES 03/2012	PHONE 0800 734 567	0780-0081/01, 02 & 03 CAUSE & EFFECTS	
60	0 AS BUILT P84-1140 SAMPLE REL., DEMARCATION ADDED JCC RL AM SES 05/2016	D P84-3100 PARTIAL AS BUILT DE-ETH STAB OVHD COMP PSV CJ WB AM SES 02/2012	<u>, ''X\\'</u>	885-0007 LOGIC DIAGRAM	
59	9 AS BUILT LO VALVES, HV-543-A WAS LO & HV-9601 WAS LC RL JC AM SES 02/2016	9 AS BUILT P84-1070 PRESSURISING GAS FROM GAS GATHERING LINE RL/MW LR JS SES 07/201			۰
58	8 AS BUILT LO VALVES, VALVE NUMBERING & ISOLATED EQUIP. RL JC/NA AM SES 08/2015	B LOGIC ASSOCIATED WITH ZSC-9601 AS BUILT RL/ES TC JS SES 06/201	COPYRIGHT The copyright in this document is vested in Vector Kapuni Limited	DATE DATE	SC
57	7 HAND VALVE NUMBER HV-403-1 WAS HV-403 RL JCC AM SES 09/2014	7 HOLD NOTE 1 CLARIFIED RL/ES TC LH SES 03/201	The contents of this document shall not be reproduced, either in whole or part, by any		-
56	6 AS BUILT P84-2004 PCV-548 REMOVAL & P84-848 WOBBE RL NA/AB AM SES 07/2014	6 AS BUILT P84-35. FT-114 FLOW CONDIT. PLATES. PC-KGP-11-KGTH-003. RL/ES TC LH SES 10/2010	means whatsoever without the prior written consent of Vector Kapuni Limited.	DRN P.RAWLES 23/01/1988 ENG	
REV	AMENDMENT BY CHK ENG APP DATE F	V AMENDMENT BY CHK ENG APP DATE	AUTOCAD ORIGINAL SHEET SIZE A1	CHK R.THAMBYAH 23/01/1988 APP J.STUART 10/02/198	8

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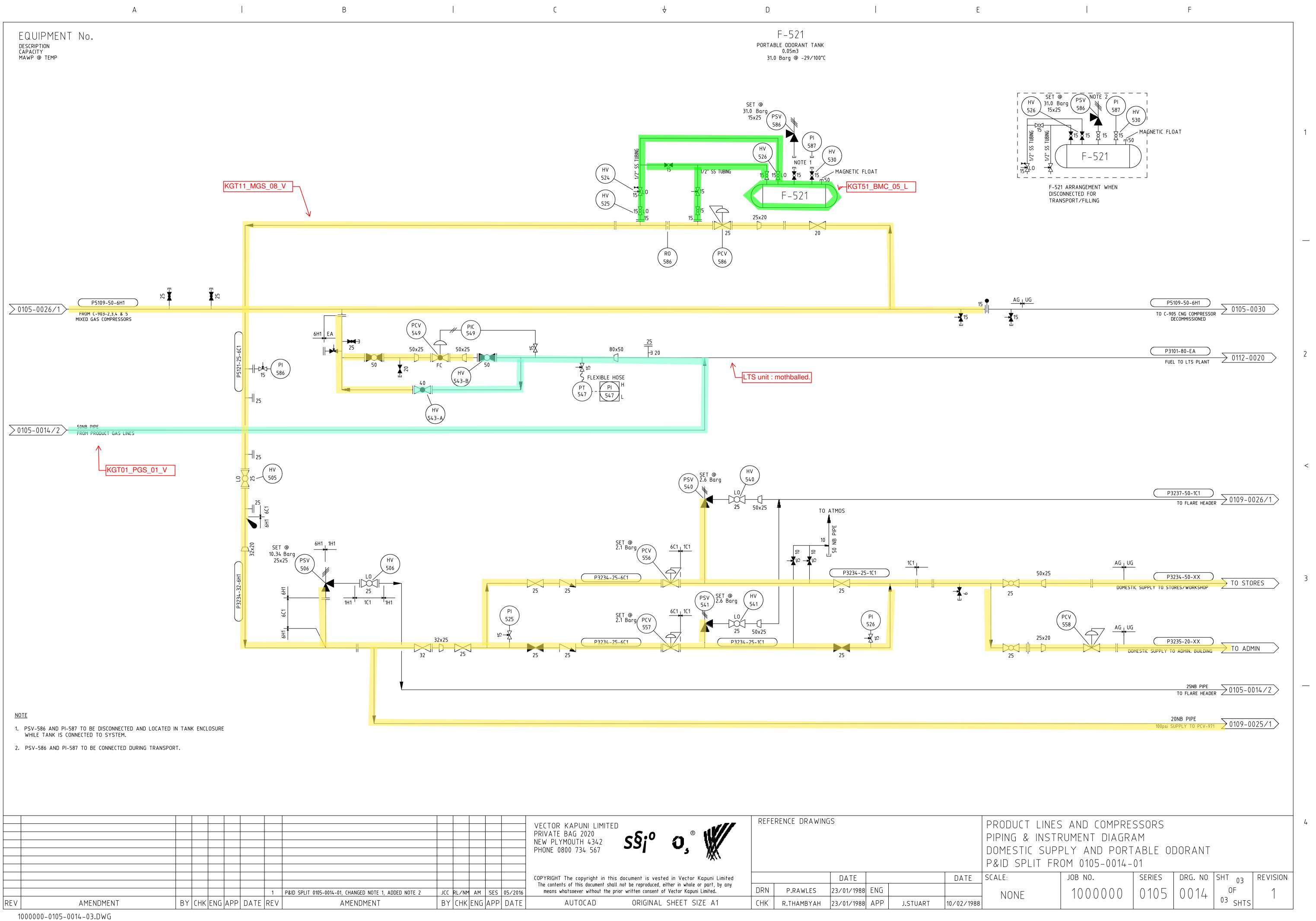
C – 4 21– 2 DE-ETHANISER 0/H COMPRESSOR Xm3 43.4 Barg @ X°C	CF-421-1A/2A suction pulsation bottle 0.024m3 51.7@ -29/149°C	CF-421-1B/2B discharge pulsation bottle 0.021m3 75@ -29/177°C	E – 4 2 1 – 1 DE-ETHANISER 0/H COMPRESSOR COOLER 0.014m3 51.7 Barg @ 177°C
43.4 Barg @ X°C			51.7 Barg @ 177°C



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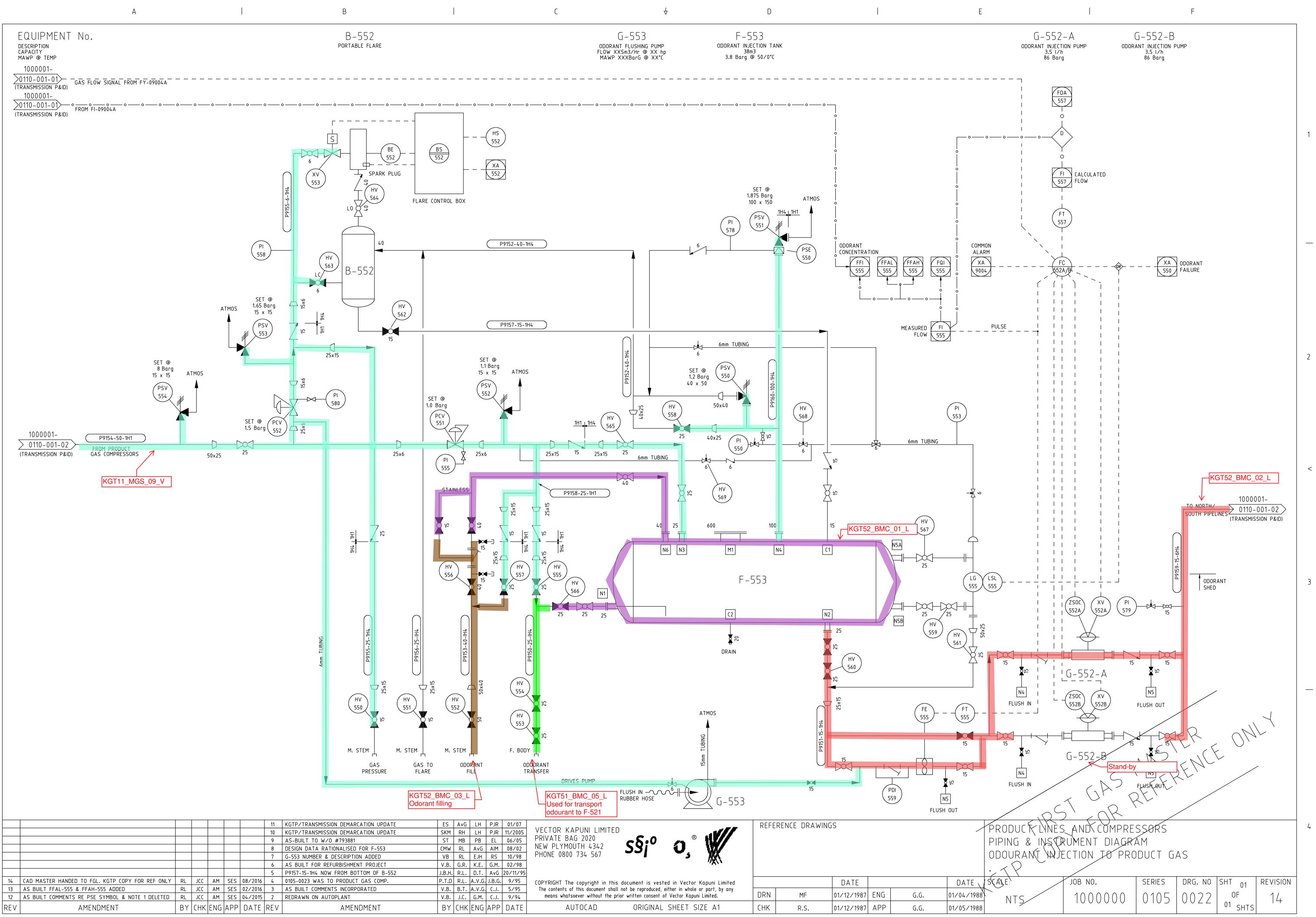
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				COPYRIGHT The copyright in this document is vested in Vector Kapuni Limited			DATE			DATE	SC
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M	AM		05/2016	means whatsoever without the prior written consent of Vector Kapuni Limited.	DRN	P.RAWLES	23/01/1988	ENG			
K	ENG	APP	DATE	AUTOCAD ORIGINAL SHEET SIZE A1	СНК	R.THAMBYAH	23/01/1988	APP	J.STUART	10/02/1988	

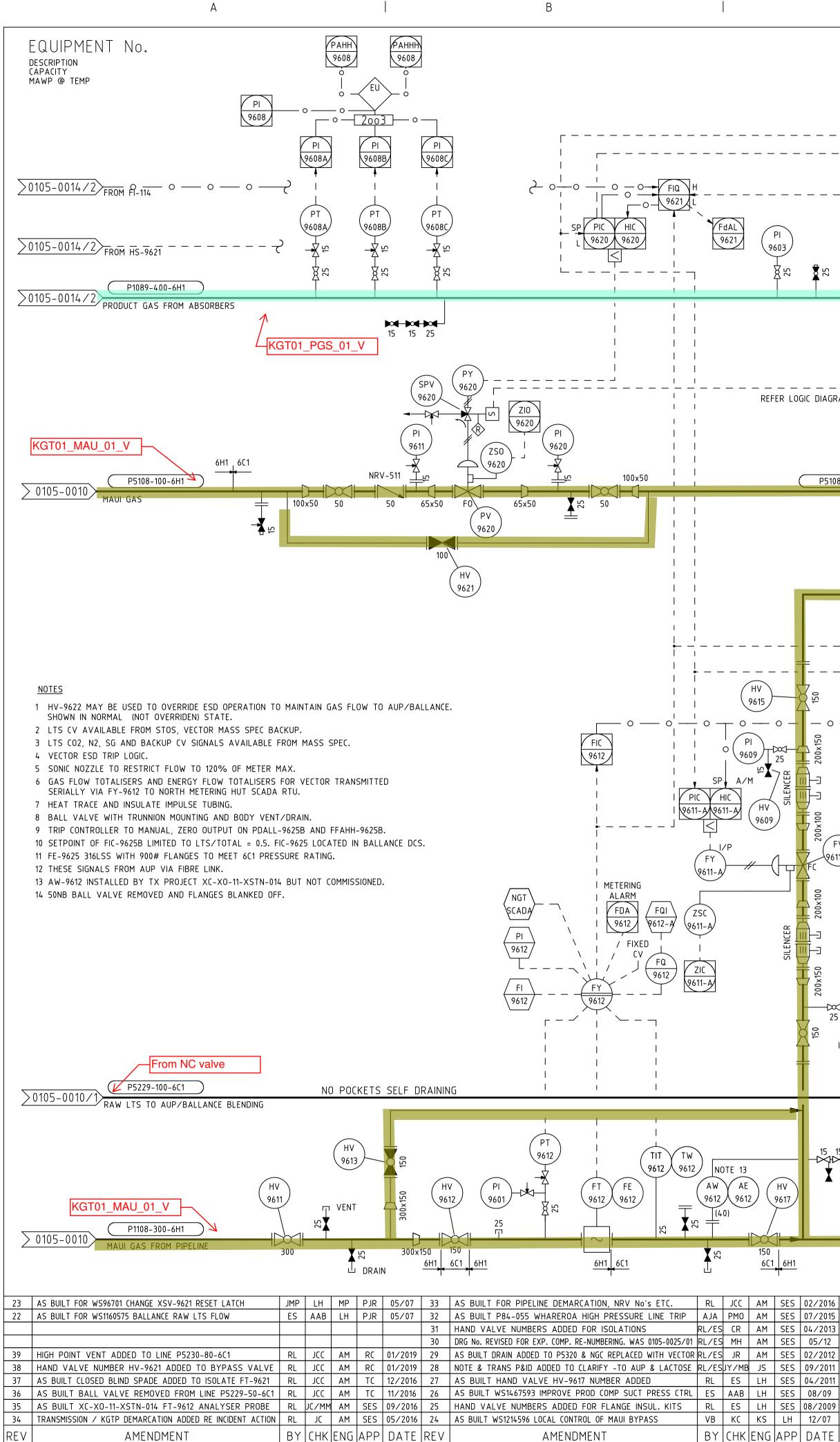
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AM	SES	05/2016		Britt	1.10000223	237 017 1700	2110			i
ENG	APP	DATE	AUTOCAD ORIGINAL SHEET SIZE A1	СНК	R.THAMBYAH	23/01/1988	APP	J.STUART	10/02/1988	

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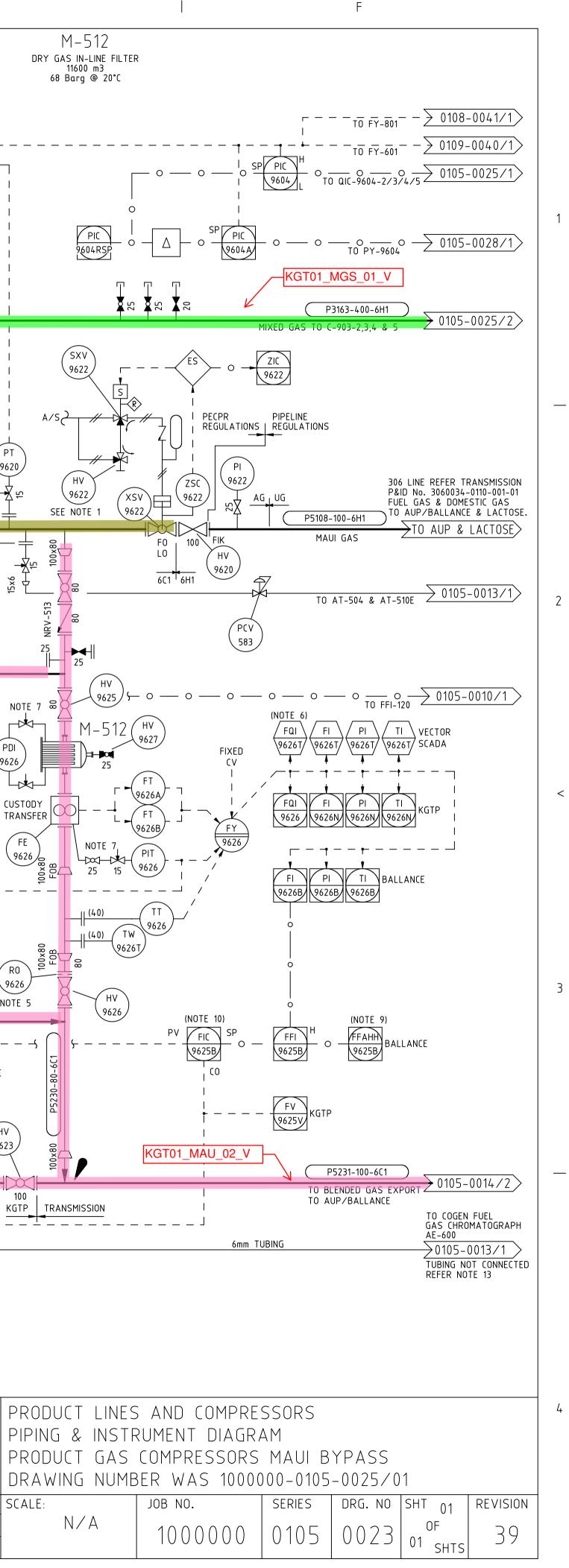


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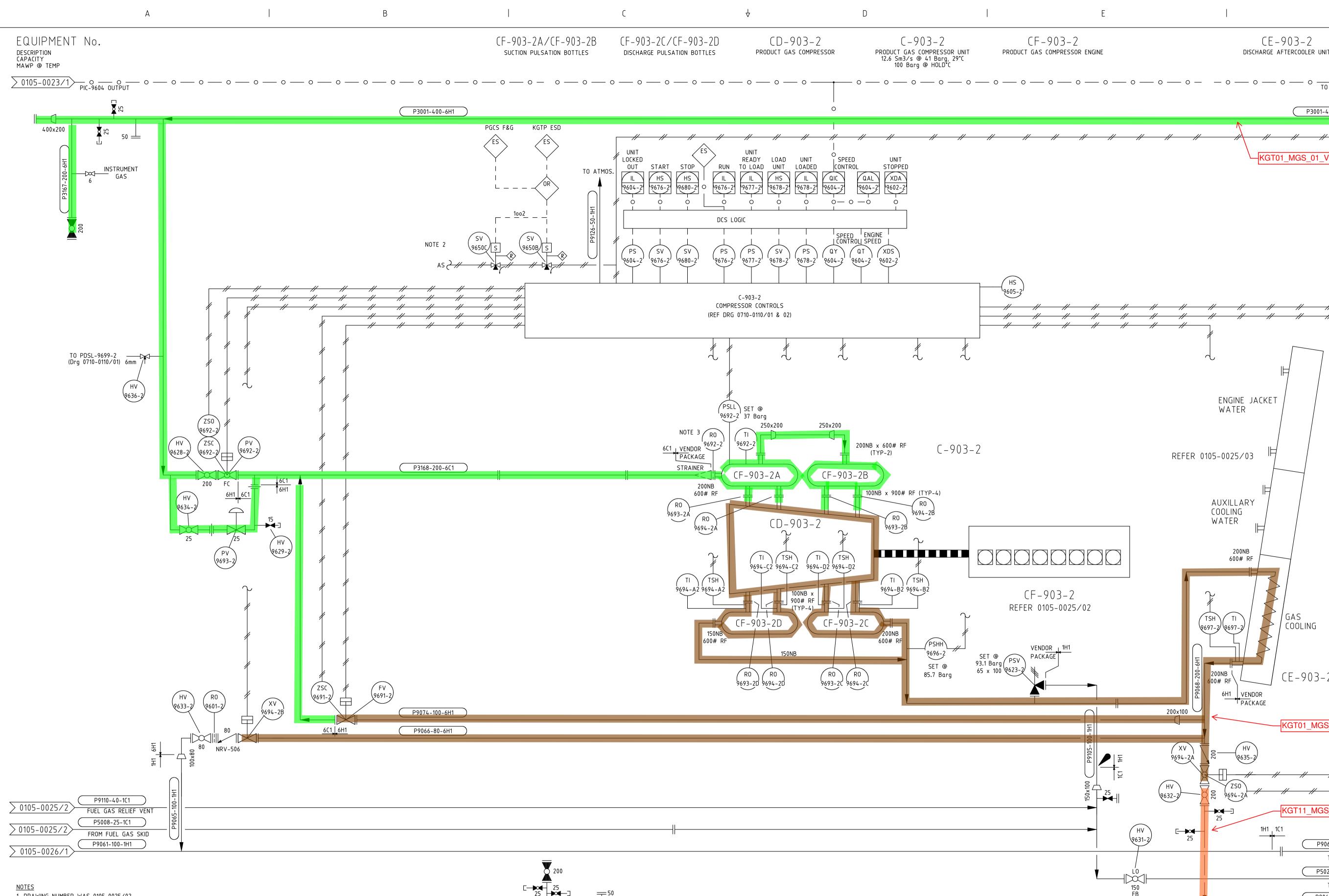
AUTOCAD

ORIGINAL SHEET SIZE A1

CHK



APP



1. DRAWING NUMBER WAS 0105-0025/02

2. SV TRIP - MANUAL BYPASS DRG No. 0760-0263 3. R09692-1 AND STRAINER ARE A SINGLE UNIT

350x200

13 DRG No. REVISED FOR EXP. COMP. RE-NUMBERING. WAS 0105-0025/02 RL/ES MH 
 RL
 JCC
 AM
 TC
 06/2019
 12
 AS BUILT NOTE TO PDSL-9699-2 ADDED

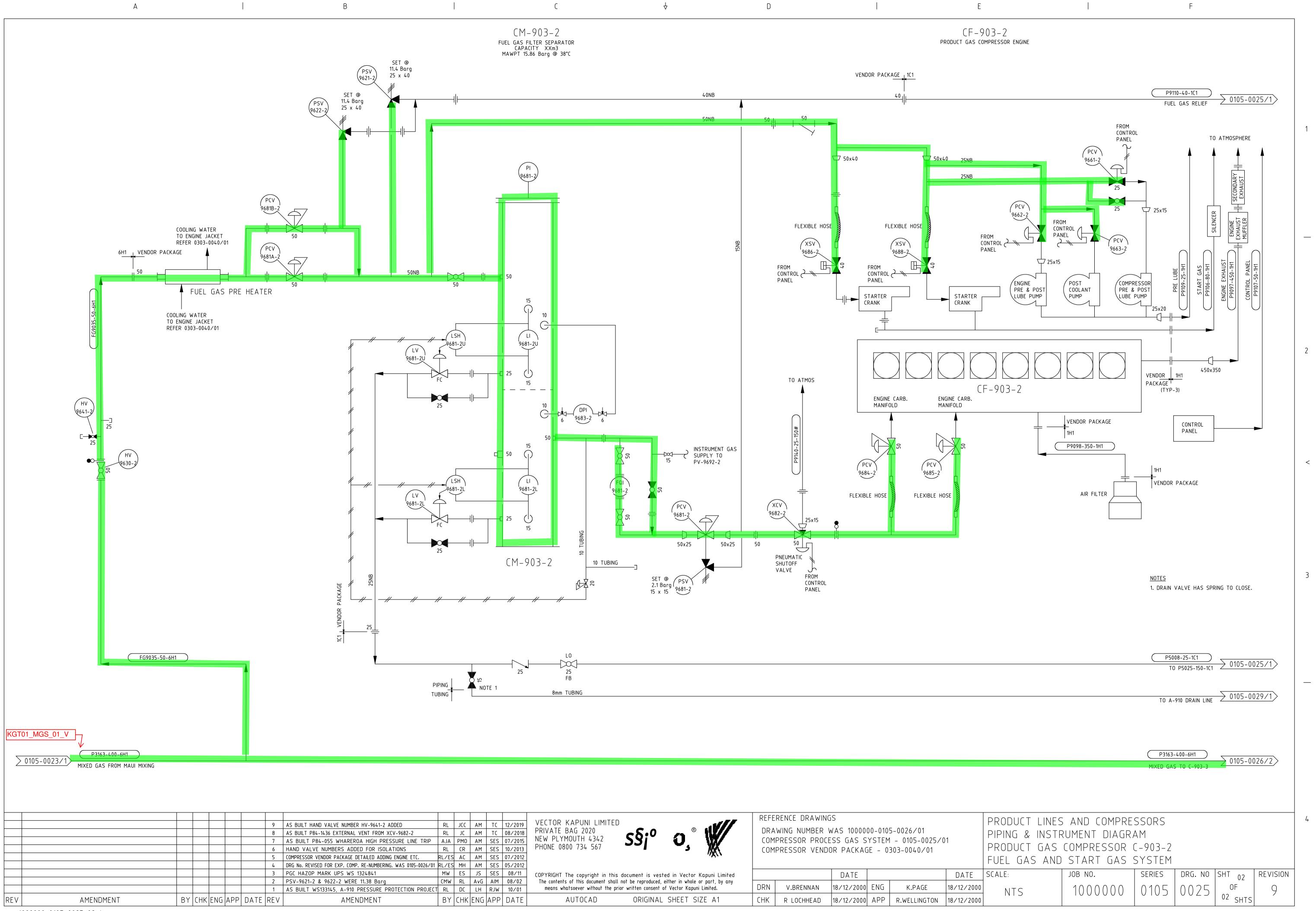
 RL
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 11
 MAC UNIONS & 15NB VENT ADDED TO PV-9693-2
 22 AS BUILT P84-1506 PSH-9696-2 CHANGED FROM 89.6 BARG ES JY ES RL 21 ADD 8 RO'S TO PULSATION BOTTLES & DELETE XT-018 20 AS-BUILT - PRODUCT GAS COMP. CONTROL IMPROVEMENTS JCC RL/AC AM SES 04/2016 10 AS BUILT WS133145, A-910 PRESSURE PROTECTION PROJECT RL DC 19AS-BUILT DRAIN ADDED TO LINE P9105 & NRV No. ADDEDRLJCAMSES02/20169AS BUILT COMMENTS ADDED18AS-BUILT P84-1128 KGTP#2 PGC PULSATIONJBCJAMSES10/20148AS BUILT FOR REFIRBISHMENT PROJECT 
 VB
 RL

 V.B.
 G.R.
 ES/RL TC AM SES 01/2014 7 AS BUILT - AUP GAS SUPPLY MODS J.W. B.T. 17 AS BUILT P84-2085 CONTROL HUT RW PENSTOCK 
 RL
 CR
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 SES
 10/2013
 6
 AS BUILT MCKEE STAGE 1. ZSOC-9606, 8 & SLU REMOVED
 J.B.H.
 R.L.

 ES/RL
 TC
 AM
 SES
 09/2012
 5
 AS BUILT COMMENTS INCORPORATED
 V.B.
 B.T.
 16 HAND VALVE NUMBERS ADDED FOR ISOLATIONS 15 AS BUILT P84-1041 FLARE GAS MEASUREMENT 14 COMPRESSOR VENDOR PACKAGE DETAILED ADDING AFTERCOOLER ETC. RL/ES AC AM SES 07/2012 4 REDRAWN ON AUTOPLANT, NOW 4 SHEETS. D.R. J.C. BY CHK ENG APP DATE REV ВҮ СНК AMENDMENT AMENDMENT REV

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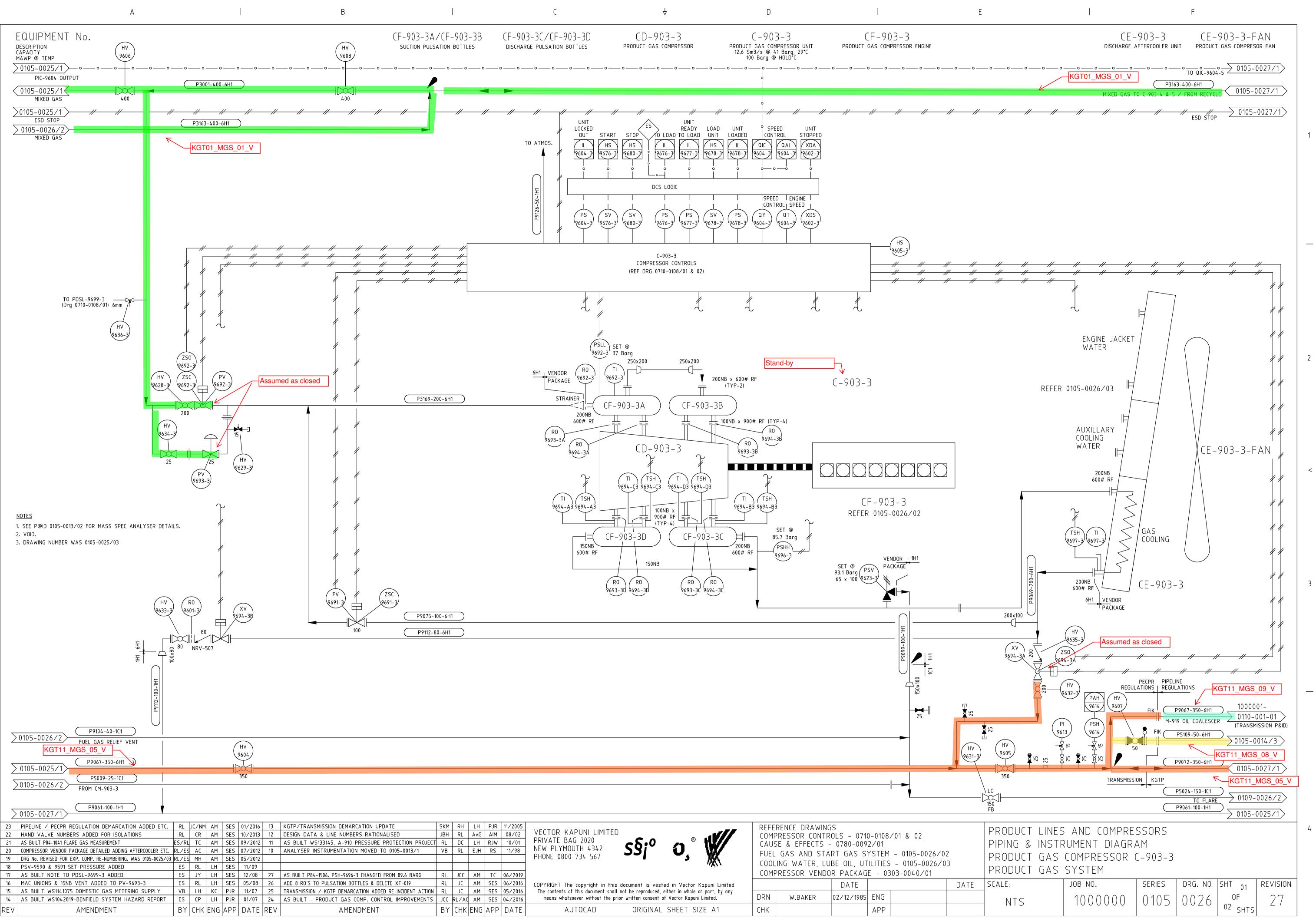
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ses 12/08 VECTOR KAPUNI LIMITED REFERENCE DRAWINGS COMPRESSOR CONTROLS - 0710-0110/01 & 02 PRODUCT LINES AND COMPRESSORS	
SES       05/2012         SES       12/08         VECTOR KAPUNI LIMITED PRIVATE BAG 2020       SSiO       SSiO         NW       10/01         RS       10/98         G.M.       10/97         A.V.G.       12/95             VECTOR KAPUNI LIMITED PRIVATE BAG 2020       SSiO         NW       PRODUCT LINES AND COMPRESSORS         CAUSE & EFFECTS - 0780-0092/01       FUEL GAS AND START GAS SYSTEM - 0105-0025/02         COOLING WATER, LUBE OIL, UTILITIES - 0105-0025/03       PRODUCT GAS COMPRESSOR C-903-2         PRODUCT GAS SYSTEM       PRODUCT GAS SYSTEM	
A.V.d.       IZ773       Converties of this document is vested in Vector Kapuni Limited       DATE       DATE       JOB NO.       SERIES       DRG. NO       SHT 01         J.B.G.       10/95       G. J. 5/95       Date	REVISION



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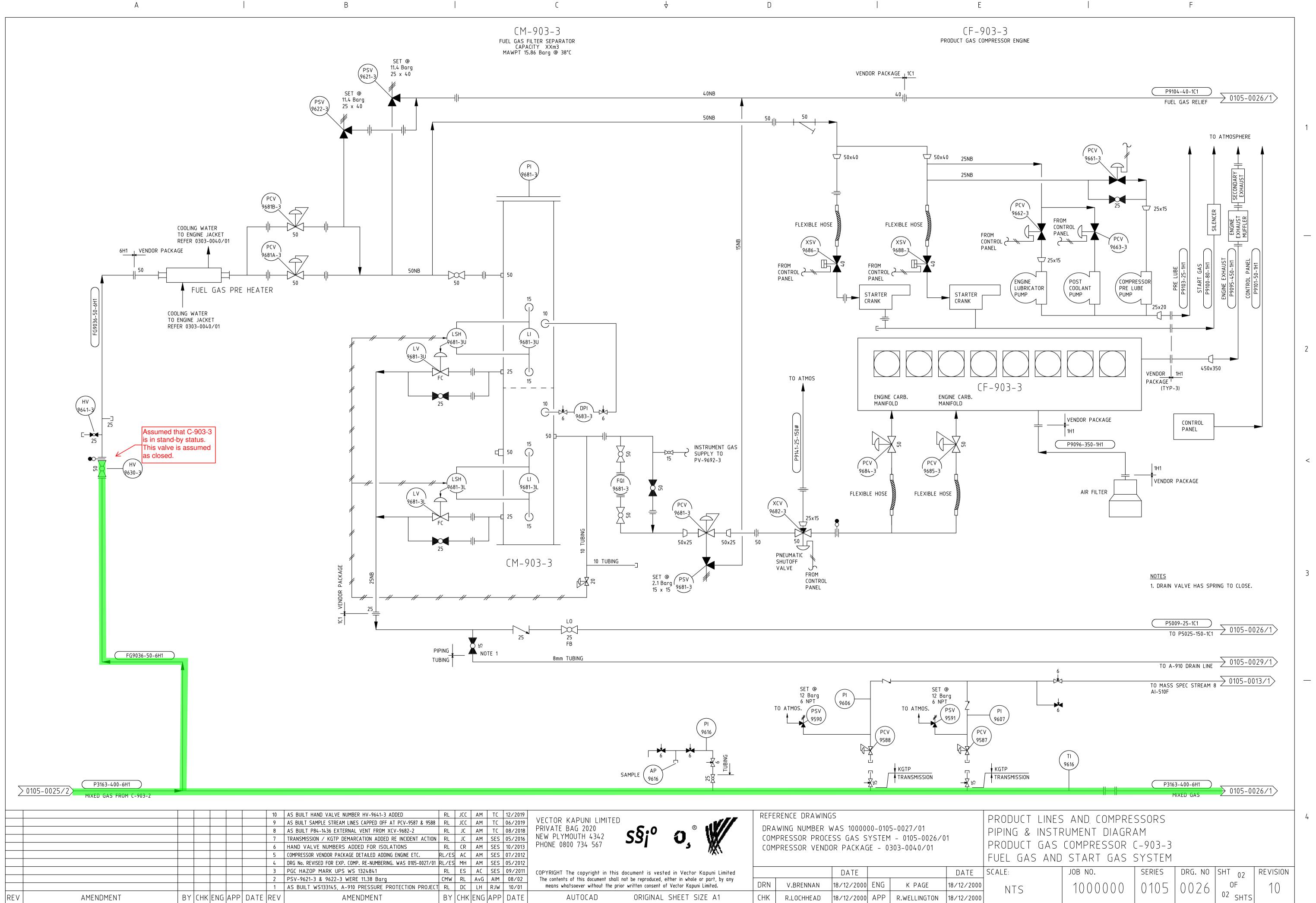
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0	AM	SES	07/2015		LOM	PRESSOR PROCE	SS GAS S	YSIEM	- 0105-0025/0	1	
)	AM	SES	10/2013	PHONE 0800 734 567	СОМ	PRESSOR VENDO	DR PACKAC	ie – 03	303-0040/01		Р
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ł	AM	SES	05/2012								I
	JS	SES	08/11	COPYRIGHT The copyright in this document is vested in Vector Kapuni Limited			DATE			DATE	SC
	AvG	AIM	08/02	The contents of this document shall not be reproduced, either in whole or part, by any							
	LH	RJW	10/01	means whatsoever without the prior written consent of Vector Kapuni Limited.	DRN	V.BRENNAN	18/12/2000	ENG	K.PAGE	18/12/2000	
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<sup>1000000-0105-0026-01.</sup>dwg

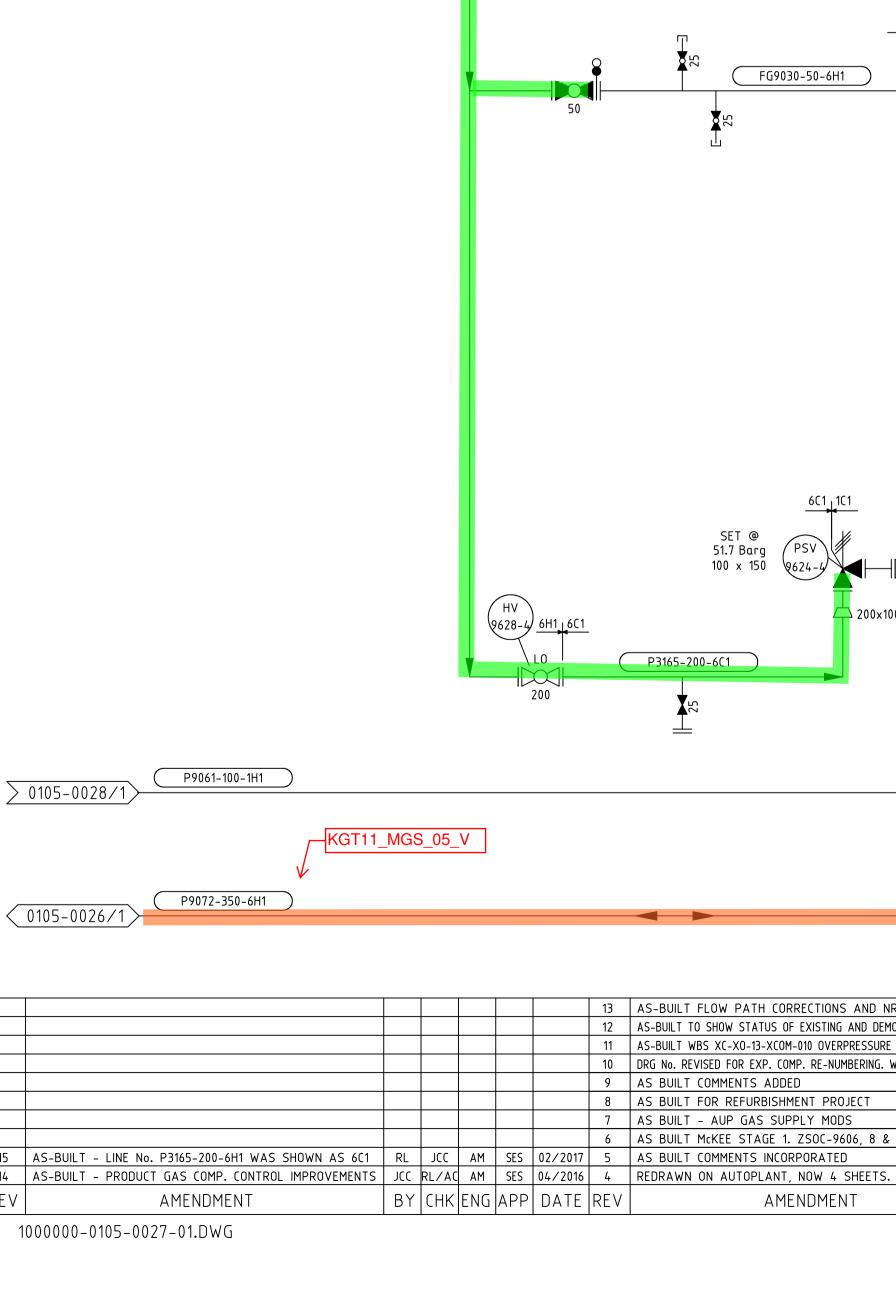
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	EJH	RS	11/98	NEW PLYMOUTH 4342 SSI O. W	FUEL GAS AND START GAS SYSTEM - 0105-0026/02		
				PHONE 0800 734 567	COOLING WATER, LUBE OIL, UTILITIES - 0105-0026/03		
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AC	AM	SES	04/2016	means whatsoever without the prior written consent of Vector Kapuni Limited.	DRN W.BAKER 02/12/1985 ENG		
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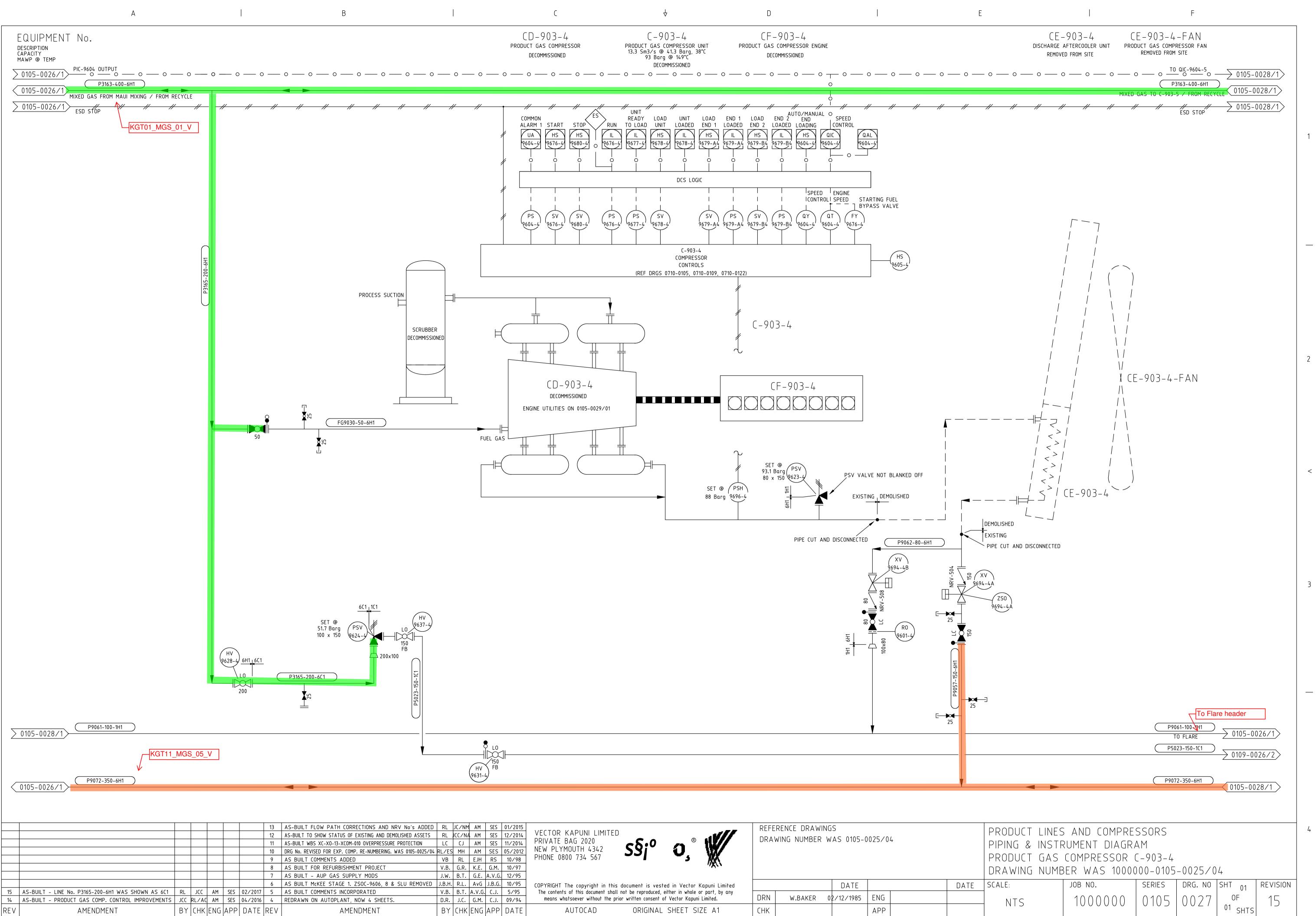


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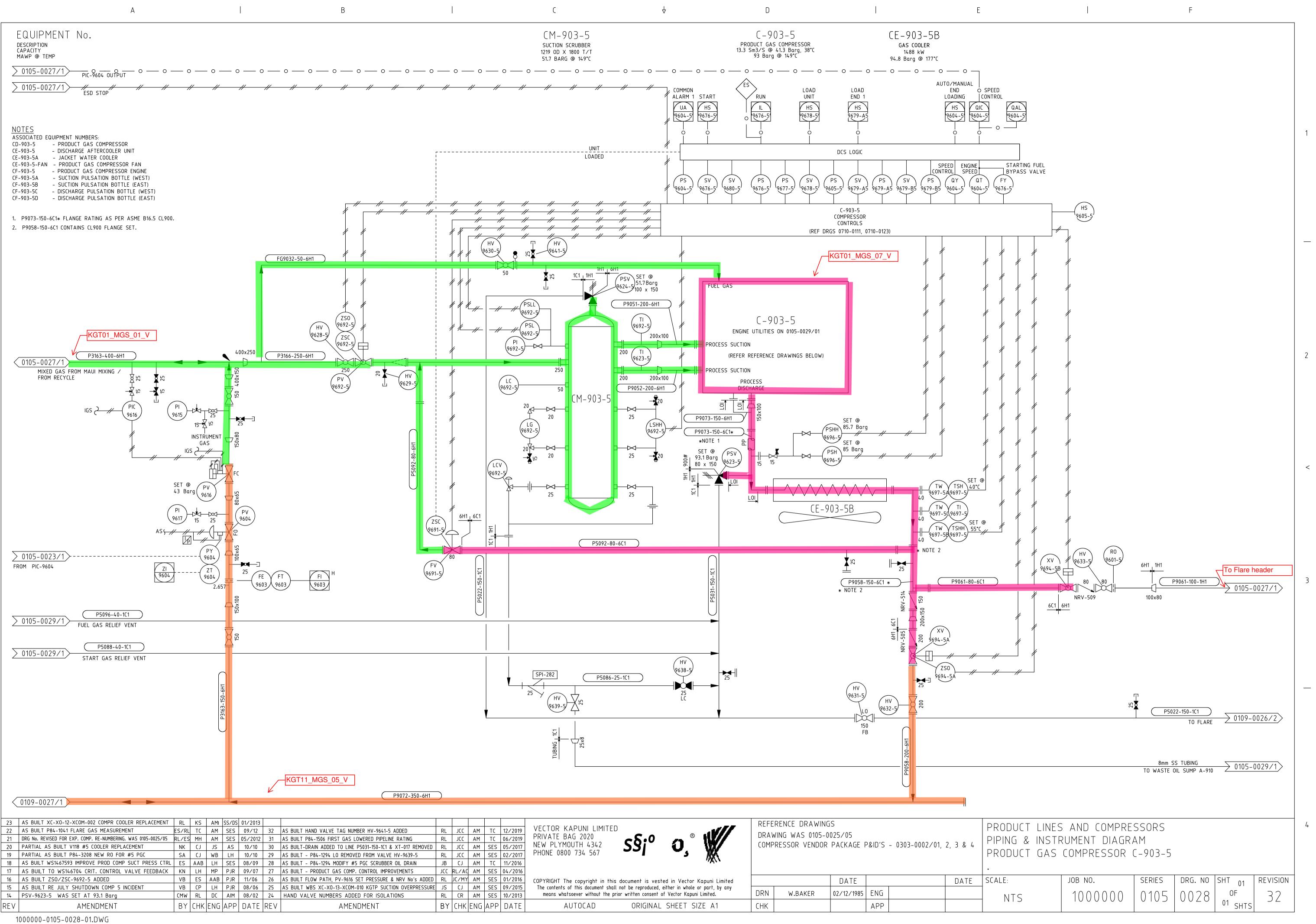
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LH	RJW	10/01	means whatsoever without the prior written consent of Vector Kapuni Limited.	DRN	V.BRENNAN	18/12/2000	ENG	k page	18/12/2000	
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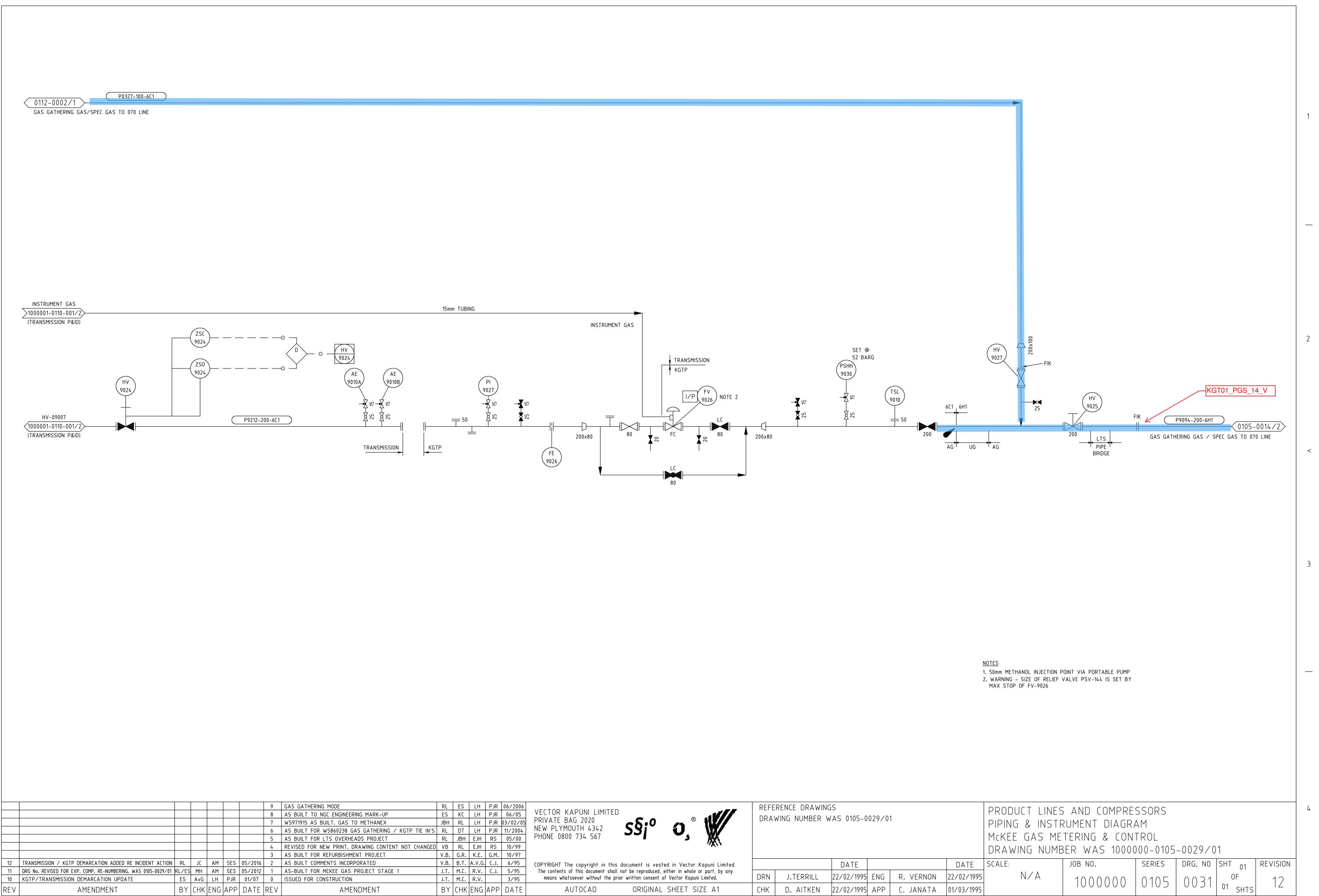




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EJH	RS	10⁄98	PHONE 0800 734 567							
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G.E.	A.V.G.	12/95								
AvG	J.B.G.	10⁄95	COPYRIGHT The copyright in this document is vested in Vector Kapuni Limited			DATE			DATE	
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G.M.	C.J.	09/94	means whatsoever without the prior written consent of Vector Kapuni Limited.	DRN	W.BAKER 0	2/12/1985	ENG			
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-	AM	TC	12/2019	VECTOR KAPUNI LIMITED							P
-	AM	TC	06/2019	PRIVATE BAG 2020		'ING WAS 0105-0					F
	AM	SES	05/2017	PRIVATE BAG 2020 NEW PLYMOUTH 4342 DUONE 0800 734 F(7)	COMPI	RESSOR VENDOR	PACKAGE F	P&ID'S	- 0303-0002/01,	2,3&4	
-	AM	SES	02/2017	PHONE 0800 734 567							
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1Y	AM	SES	01/2016	COPYRIGHT The copyright in this document is vested in Vector Kapuni Limited			DATE			DATE	S
	AM	SES	09/2015	The contents of this document shall not be reproduced, either in whole or part, by any							
	AM	SES	10/2013	means whatsoever without the prior written consent of Vector Kapuni Limited.	DRN	W.BAKER	02/12/1985	ENG			
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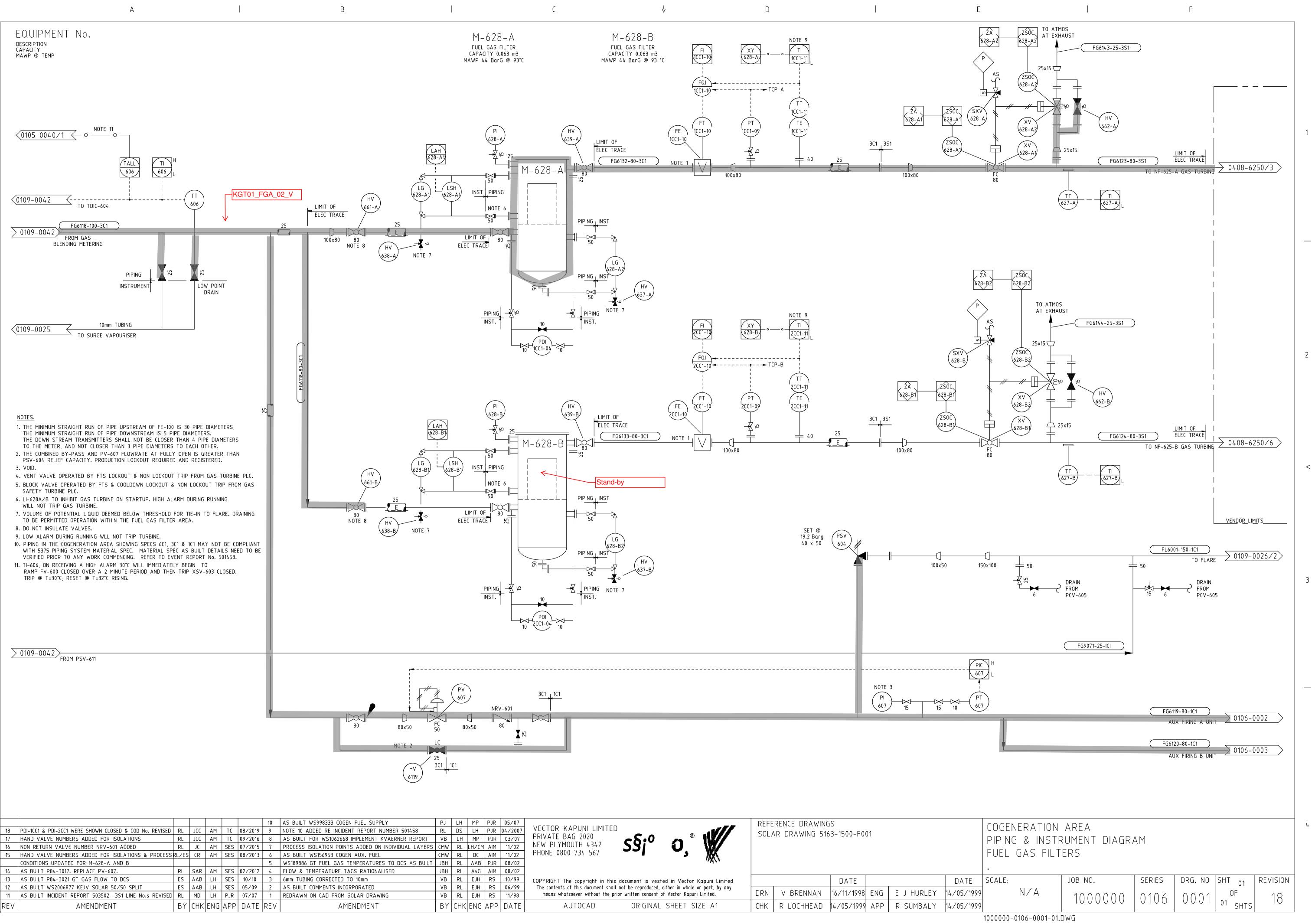
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	LH	PJR	06/2006		REFE	RENCE DRAWING	iS					
	LH	РJR	06/05	VECTOR KAPUNI LIMITED PRIVATE BAG 2020				020 /01				Ρ
	LH	PJR	03/02/05	PRIVATE BAG 2020 NEW PLYMOUTH 4342 DHONE 0800 72/ 547 SSi <sup>o</sup> O. <sup>®</sup>	URAV	wing number w	IAS 0105-0	029701				Ρ
	LH	PJR	11/2004	NEW PLYMOUTH 4342 SSi O. W								
ł	EJH	RS	05/00	PHONE 0800 734 567								
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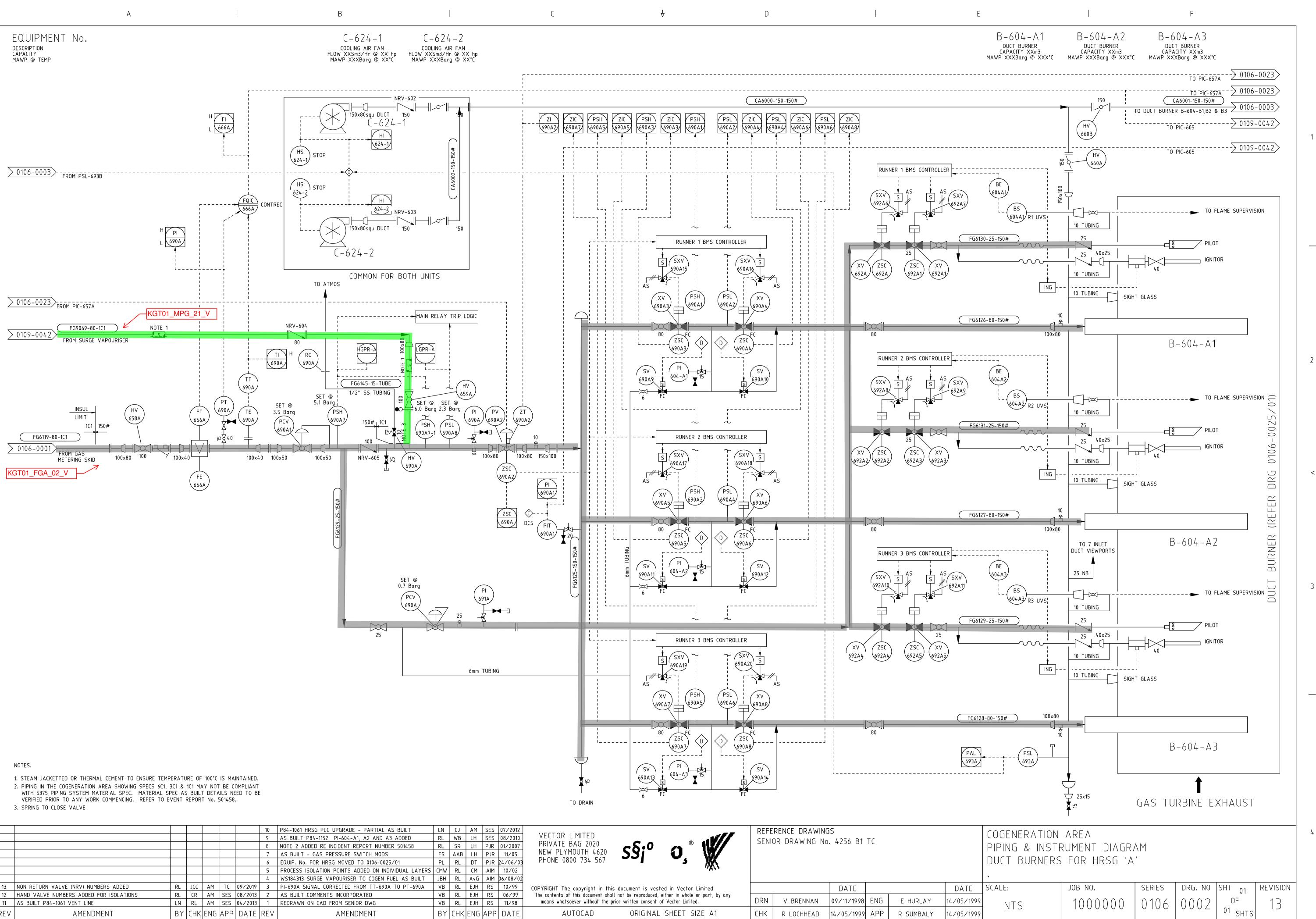
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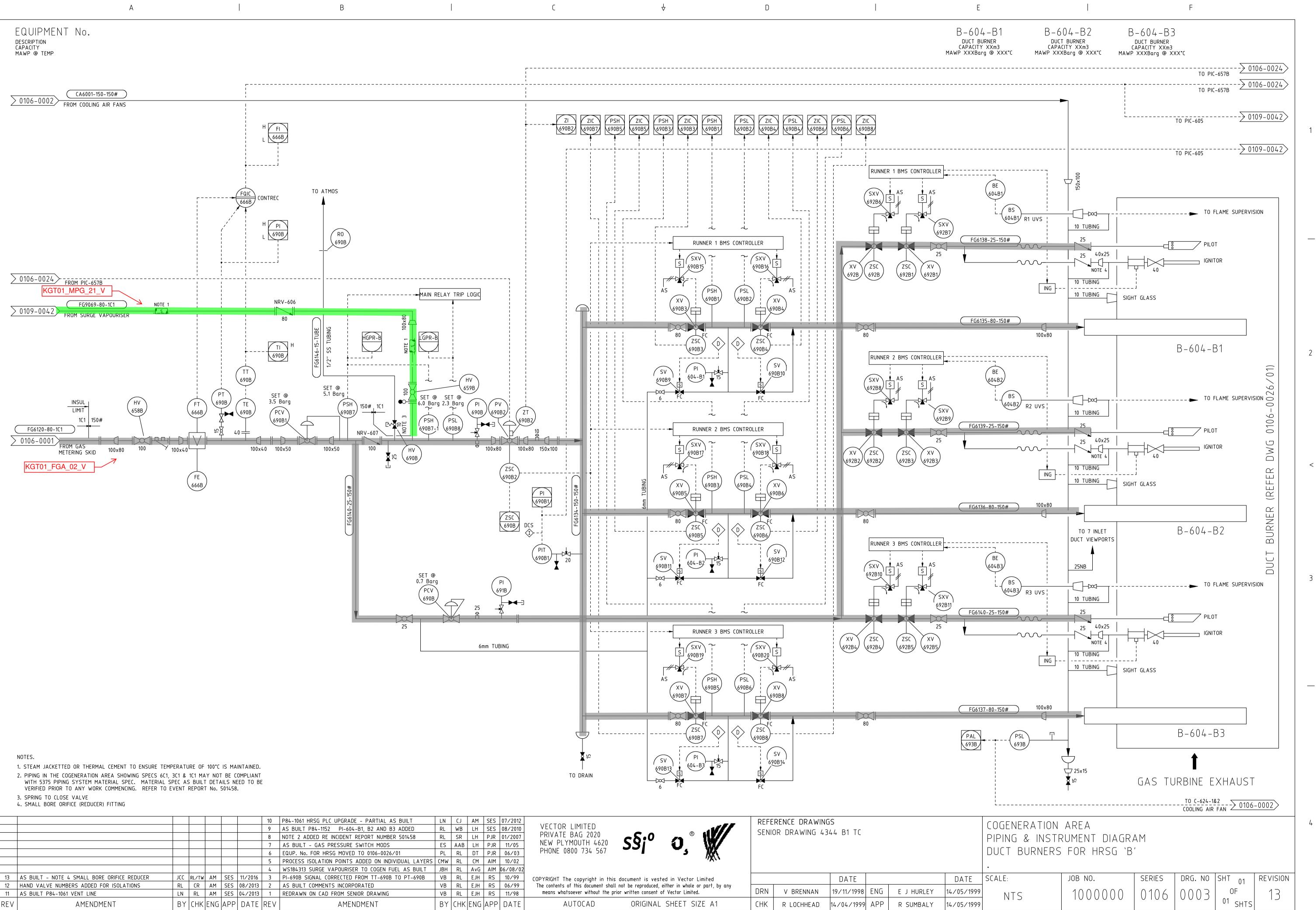
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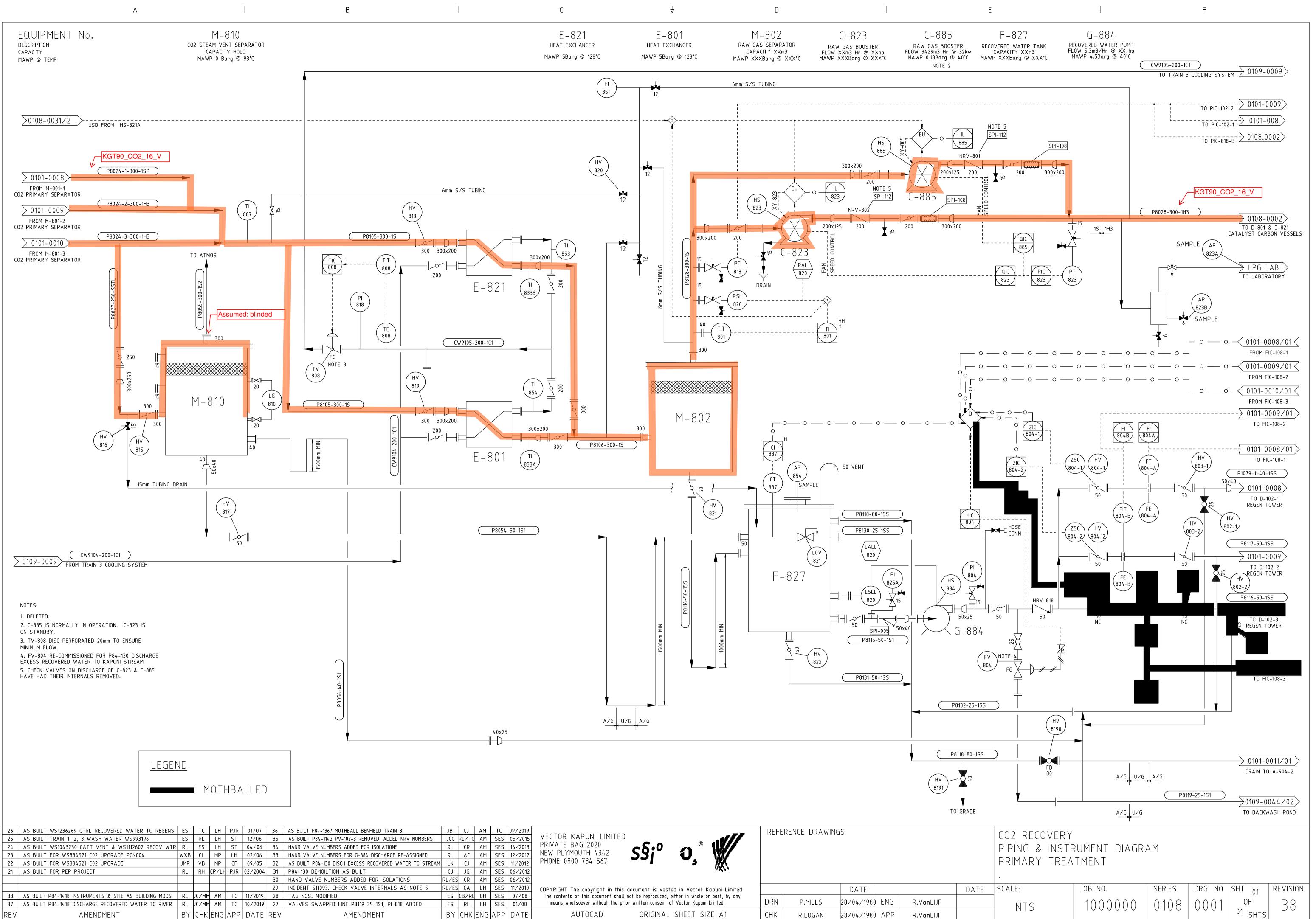
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	LH	РJR	04/2007	VECTOR KAPUNI LIMITED		R DRAWING 516		11			C
	MP	РJR	03/07	PRIVATE BAG 2020 NEW PLYMOUTH 4342 DHONE 0800 724 F47 SSi <sup>o</sup> 0 <sup>®</sup>	50LF	AN DRAWING JIO	101-0001-00	71			Ρ
Lł	⊣∕см	AIM	11/02	NEW PLYMOUTH 4342 SSI 0							' 
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	EJH	RS	11/98	means whatsoever without the prior written consent of Vector Kapuni Limited.	DRN	V BRENNAN	16/11/1998	ENG	E J HURLEY	14/05/1999	
×Ε	ING	APP	DATE	AUTOCAD ORIGINAL SHEET SIZE A1	СНК	R LOCHHEAD	14/05/1999	APP	R SUMBALY	14/05/1999	
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						10	0 P84-1061 HRSG PLC UPGRADE - PARTIAL AS BUILT	LN	1 (	CJ AM	SES 07/	/2012				REFE	RENCE DRAWIN	GS			
-						9	9 AS BUILT P84-1152 PI-604-A1, A2 AND A3 ADDED	RL	_   V	WB LH	SES 08/	/2010	VECTOR LIMITED	-			OR DRAWING No				COGENER
00						8	NOTE 2 ADDED RE INCIDENT REPORT NUMBER 50145	B RL		SR LH	PJR 01/	/2007	PRIVATE BAG 2020	c2.0	o ® ₩	JLINI	UK DKAWING NG	J. 42JU DI IC			PIPING 8
- -						7	7 AS BUILT - GAS PRESSURE SWITCH MODS	ES	5 A	AB LH	PJR 11	1/05	NEW PLYMOUTH 4620	S§;°	J W/						
-9(						6	6 EQUIP. No. FOR HRSG MOVED TO 0106-0025/01	Pl	L F	RL DT	PJR 24/	′06/03	PHONE 0800 734 567		- <u>5</u> MX						DUCT BL
)].0						5	5 PROCESS ISOLATION POINTS ADDED ON INDIVIDUAL	LAYERS CM	WF	RL CM	AIM 10	0/02			"X\\						
-						4	4 WS184313 SURGE VAPOURISER TO COGEN FUEL AS	BUILT JB	H F	RL AvG	AIM 06/	′08/02									•
2 2 13	NON RETURN VALVE (NRV) NUMBERS ADDED	RL	JCC	АМ   Т	C 09/2	019 3	3 PI-690A SIGNAL CORRECTED FROM TT-690A TO PT	690A VE	BF	RL EJH	RS 10	0/99	COPYRIGHT The copyright in this d	ocument is ves	ted in Vector Limited			DATE		DATE	SCALE:
3 12	HAND VALVE NUMBERS ADDED FOR ISOLATIONS	RL	CR	AM SE	S 08/2	013 2	2 AS BUILT COMMENTS INCORPORATED	VE	BI	RL EJH	RS 06	6/99	The contents of this document shall n	ot be reproduced,	either in whole or part, by any						-
₽ [11	AS BUILT P84-1061 VENT LINE	LN	RL	AM SE	S 04/2	013 1	1 REDRAWN ON CAD FROM SENIOR DWG	VE	BF	RL EJH	RS 11	1/98	means whatsoever without the prior	written consent	of Vector Limited.	DRN	V BRENNAN	09/11/1998 ENG	E HURLAY	14/05/1999	NTS
RE	V AMENDMENT	BY	CHK E	NG AF	P DA	TE RE	EV AMENDMENT	В	ΥC	HK ENG	APP D	ATE	AUTOCAD	ORIGINAL	. SHEET SIZE A1	CHK	R LOCHHEAD	14/05/1999 APP	R SUMBALY	14/05/1999	



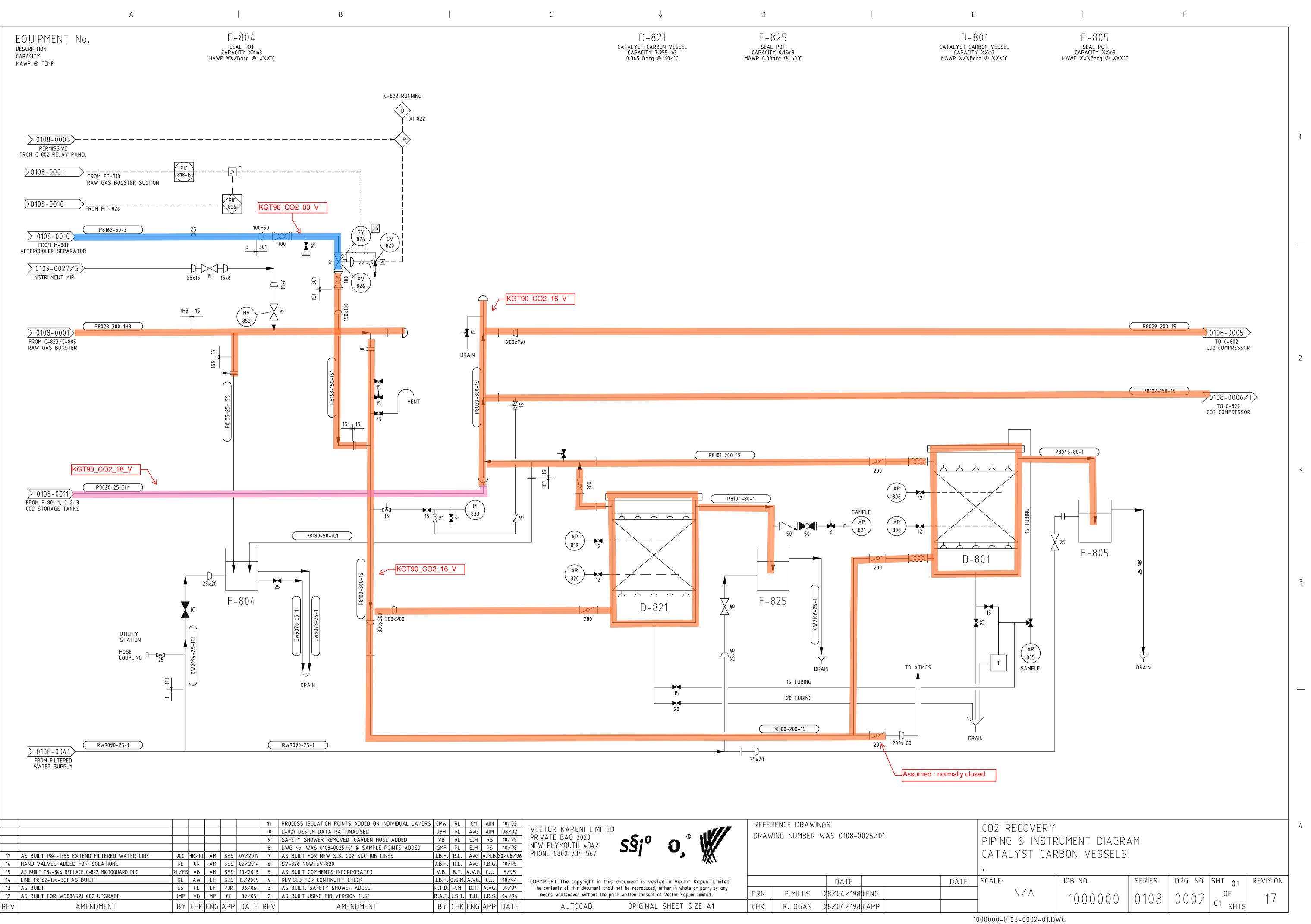
,													
								10	P84-1061 HRSG PLC UPGRADE - PARTIAL AS BUILT	LN	C)	AM	SES
, ,								9	AS BUILT P84-1152 PI-604-B1, B2 AND B3 ADDED	RL	WB	LH	SES
, ,								8	NOTE 2 ADDED RE INCIDENT REPORT NUMBER 501458	RL	SR	LH	РJR
, ,								7	AS BUILT – GAS PRESSURE SWITCH MODS	ES	AAB	LH	PJR
>								6	EQUP. No. FOR HRSG MOVED TO 0106-0026/01	PL	RL	DT	PJR
-								5	PROCESS ISOLATION POINTS ADDED ON INDIVIDUAL LAYERS	CMW	RL	CM	AIM
<b>,</b>								4	WS184313 SURGE VAPOURISER TO COGEN FUEL AS BUILT	JBH	RL	AvG	AIM
>	13	AS BUILT - NOTE 4 SMALL BORE ORIFICE REDUCER	JCC	RL/TW	AM	SES	11/2016	3	PI-690B SIGNAL CORRECTED FROM TT-690B TO PT-690B	VB	RL	EJH	RS
>	12	HAND VALVE NUMBERS ADDED FOR ISOLATIONS	RL	CR	AM	SES	08/2013	2	AS BUILT COMMENTS INCORPORATED	VB	RL	EJH	RS
-	11	AS BUILT P84-1061 VENT LINE	LN	RL	AM	SES	04/2013	1	REDRAWN ON CAD FROM SENIOR DRAWING	VB	RL	EJH	RS
	Rev	AMENDMENT	ΒY	СНК	ENG	APP	DATE	REV	AMENDMENT	BY	СНК	ENG	APF
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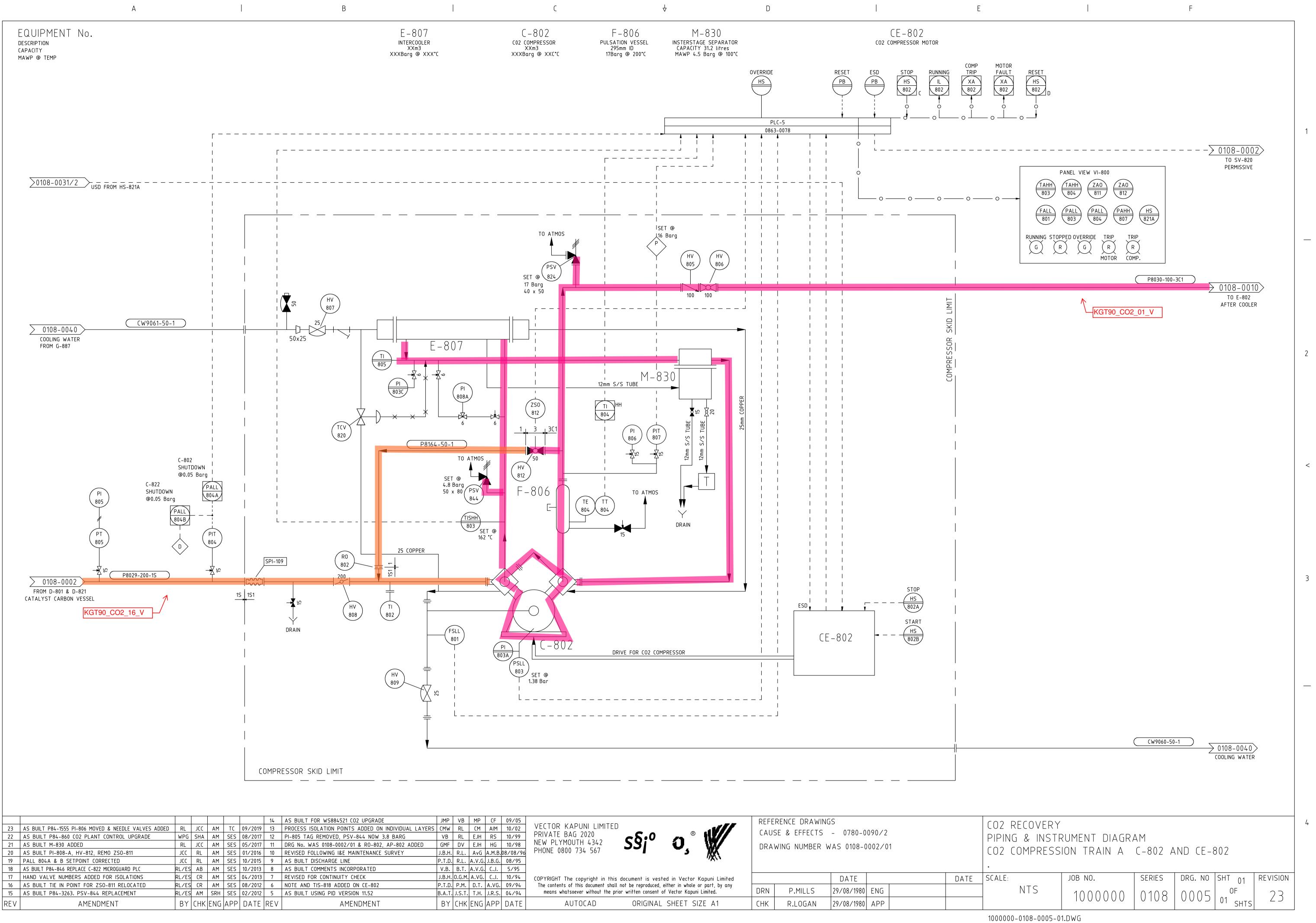
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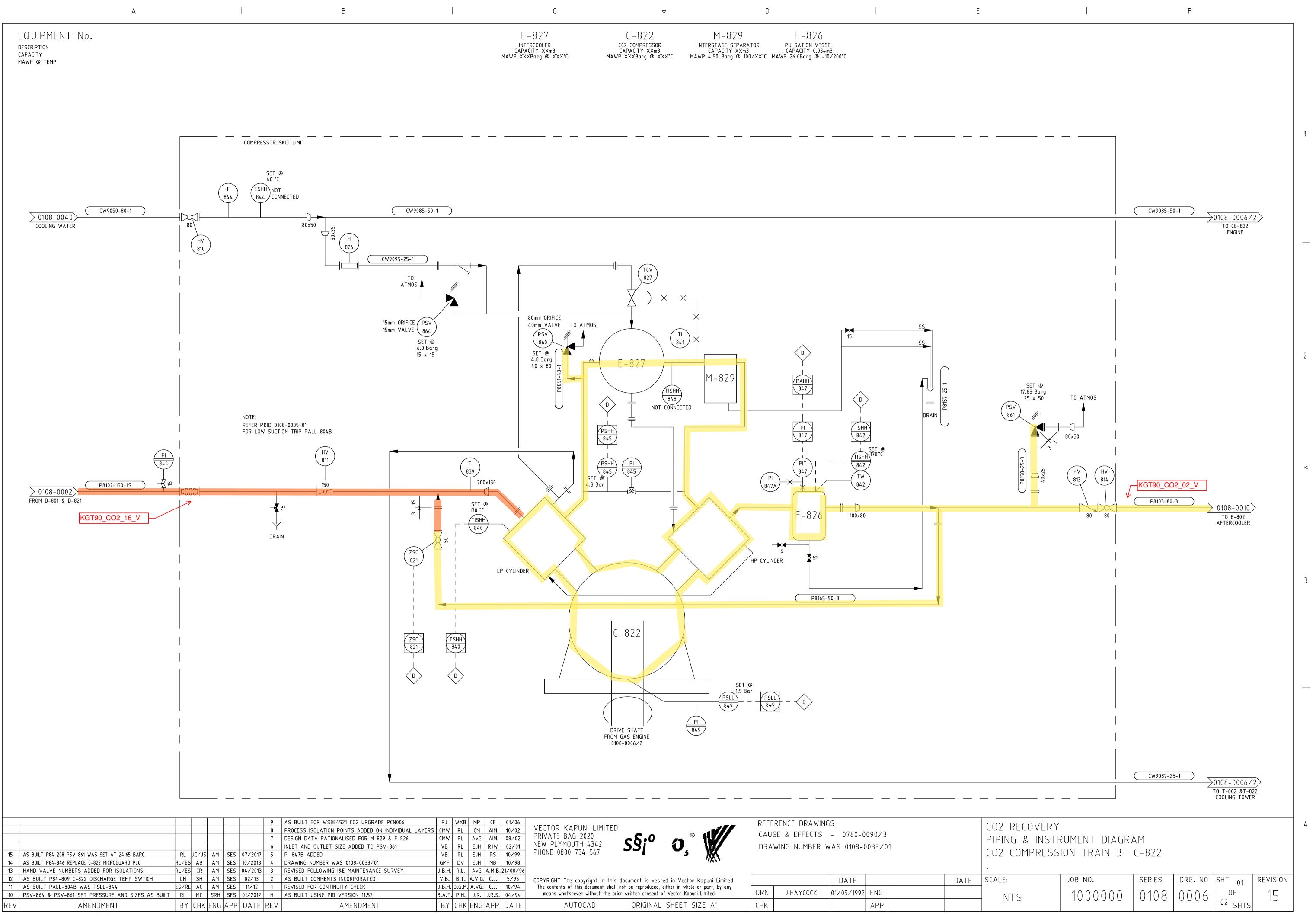


						10	D-821 DESIGN DATA RATIONALISED	JBH	RL
						9	SAFETY SHOWER REMOVED, GARDEN HOSE ADDED	VB	RL
						8	DWG No. WAS 0108-0025/01 & SAMPLE POINTS ADDED	GMF	RL
AS BUILT P84-1355 EXTEND FILTERED WATER LINE	JCC	MK/RL	AM	SES	07/2017	7	AS BUILT FOR NEW S.S. CO2 SUCTION LINES	J.B.H.	R.L.
HAND VALVES ADDED FOR ISOLATIONS	RL	CR	AM	SES	02/2014	6	SV-826 NOW SV-820	J.B.H.	R.L.
AS BUILT P84-846 REPLACE C-822 MICROGUARD PLC	RL/ES	AB	AM	SES	10/2013	5	AS BUILT COMMENTS INCORPORATED	V.B.	B.T.
LINE P8162-100-3C1 AS BUILT	RL	AW	LH	SES	12/2009	4	REVISED FOR CONTINUITY CHECK	J.B.H.	0.G.M
AS BUILT	ES	RL	LH	PJR	06/06	3	AS BUILT. SAFETY SHOWER ADDED	P.T.D.	. P.M.
AS BUILT FOR WS884521 C02 UPGRADE	JMP	VB	MP	CF	09/05	2	AS BUILT USING PID VERSION 11.52	B.A.T.	J.S.T
AMENDMENT	BY	СНК	ENG	APP	DATE	REV	AMENDMENT	ΒY	СНК
	HAND VALVES ADDED FOR ISOLATIONS AS BUILT P84-846 REPLACE C-822 MICROGUARD PLC LINE P8162-100-3C1 AS BUILT AS BUILT AS BUILT FOR WS884521 C02 UPGRADE	HAND VALVES ADDED FOR ISOLATIONSRLAS BUILT P84-846 REPLACE C-822 MICROGUARD PLCRL/ESLINE P8162-100-3C1 AS BUILTRLAS BUILTESAS BUILT FOR WS884521 C02 UPGRADEJMP	HAND VALVES ADDED FOR ISOLATIONSRLCRAS BUILT P84-846 REPLACE C-822 MICROGUARD PLCRL/ESABLINE P8162-100-3C1 AS BUILTRLAWAS BUILTESRLAS BUILT FOR WS884521 C02 UPGRADEJMPVB	HAND VALVES ADDED FOR ISOLATIONSRLCRAMAS BUILT P84-846 REPLACE C-822 MICROGUARD PLCRL/ESABAMLINE P8162-100-3C1 AS BUILTRLAWLHAS BUILTESRLLHAS BUILT FOR WS884521 C02 UPGRADEJMPVBMP	HAND VALVES ADDED FOR ISOLATIONSRLCRAMSESAS BUILT P84-846 REPLACE C-822 MICROGUARD PLCRL/ESABAMSESLINE P8162-100-3C1 AS BUILTRLAWLHSESAS BUILTESRLLHPJRAS BUILT FOR WS884521 C02 UPGRADEJMPVBMPCF	HAND VALVES ADDED FOR ISOLATIONSRLCRAMSES02/2014AS BUILT P84-846 REPLACE C-822 MICROGUARD PLCRL/ESABAMSES10/2013LINE P8162-100-3C1 AS BUILTRLAWLHSES12/2009AS BUILTESRLLHPJR06/06AS BUILT FOR WS884521 C02 UPGRADEJMPVBMPCF09/05	HAND VALVES ADDED FOR ISOLATIONS       RL       CR       AM       SES       02/2014       6         AS BUILT P84-846 REPLACE C-822 MICROGUARD PLC       RL/ES       AB       AM       SES       10/2013       5         LINE P8162-100-3C1 AS BUILT       RL       AW       LH       SES       12/2009       4         AS BUILT FOR WS884521 C02 UPGRADE       JMP       VB       MP       CF       09/05       2	Image: state of the state o	ManualManu<

СМ	AIM	10/02		REFE	RENCE DRAWING	iS			ł
AvG	AIM	08/02	VECTOR KAPUNI LIMITED		VING NUMBER W		025 /01		l
EJH	RS	10/99	VECTOR KAPUNI LIMITED PRIVATE BAG 2020	DRAV	WING NUMBER W	AS 0100-0	025701		l
EJH	RS	10/98	PRIVATE BAG 2020 NEW PLYMOUTH 4342 DHONE 0800 72/ 547						l
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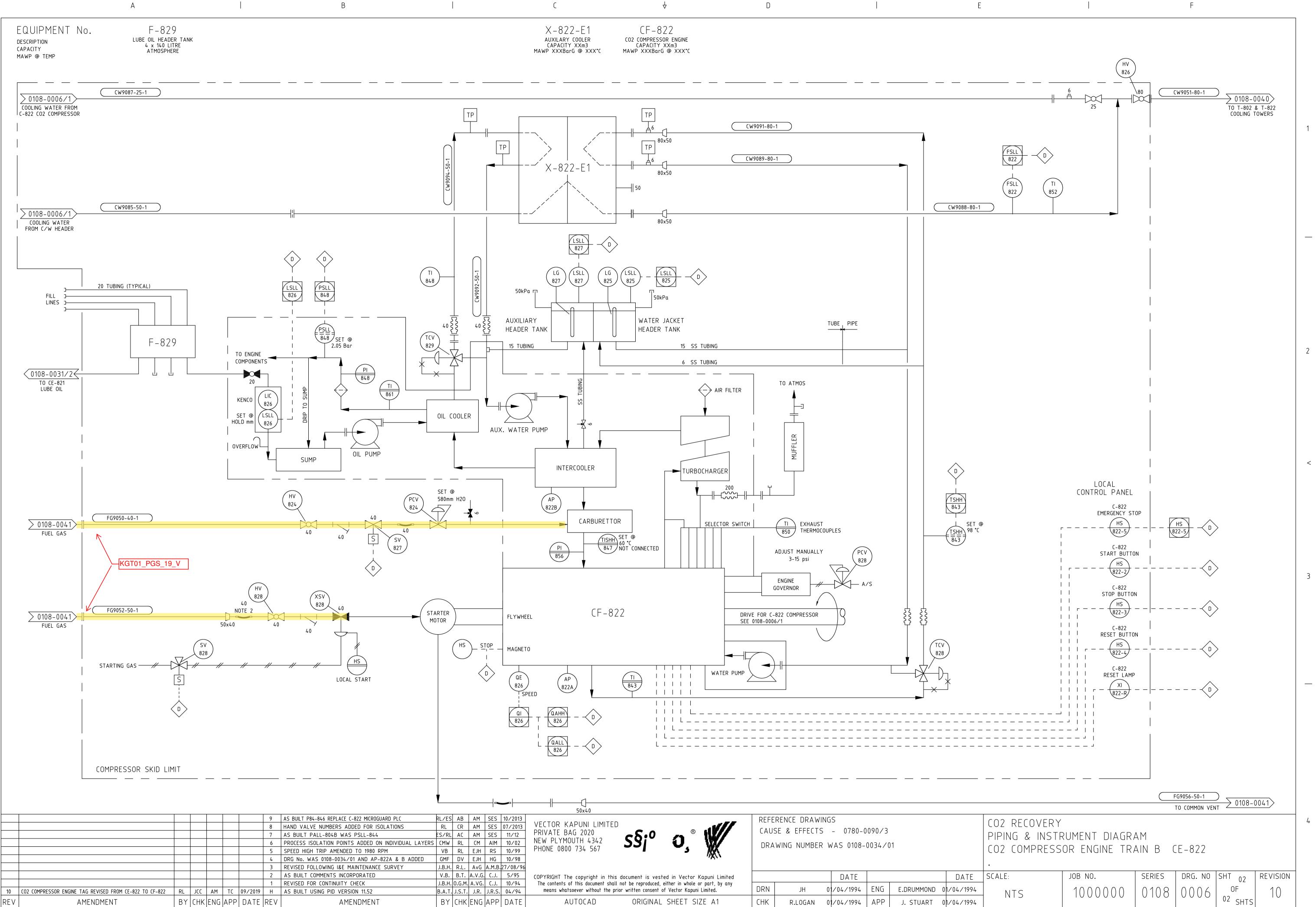
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ORIGINAL SHEET SIZE A1 CHK R.LOGAN 29/08/1980 AP	
the prior written consent of Vector Kapuni Limited. DRN P.MILLS 29/08/1980 EN	D



<sup>1000000-0108-0006-01.</sup>DWG

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E-827 INTERCOOLER CAPACITY XXm3 MAWP XXXBarg @ XXX*C	C-822 co2 compressor capacity xxm3 mawp xxxBarg @ xxx*c	M-829 INTERSTAGE SEPARATOR CAPACITY XXm3 MAWP 4.50 Barg @ 100/XX°C	F-826 PULSATION VESSEL CAPACITY 0.034m3 MAWP 26.0Barg @ -10/200°C		

3	MP	CF	01/06		REFE	RENCE DRAWING	ĩS			
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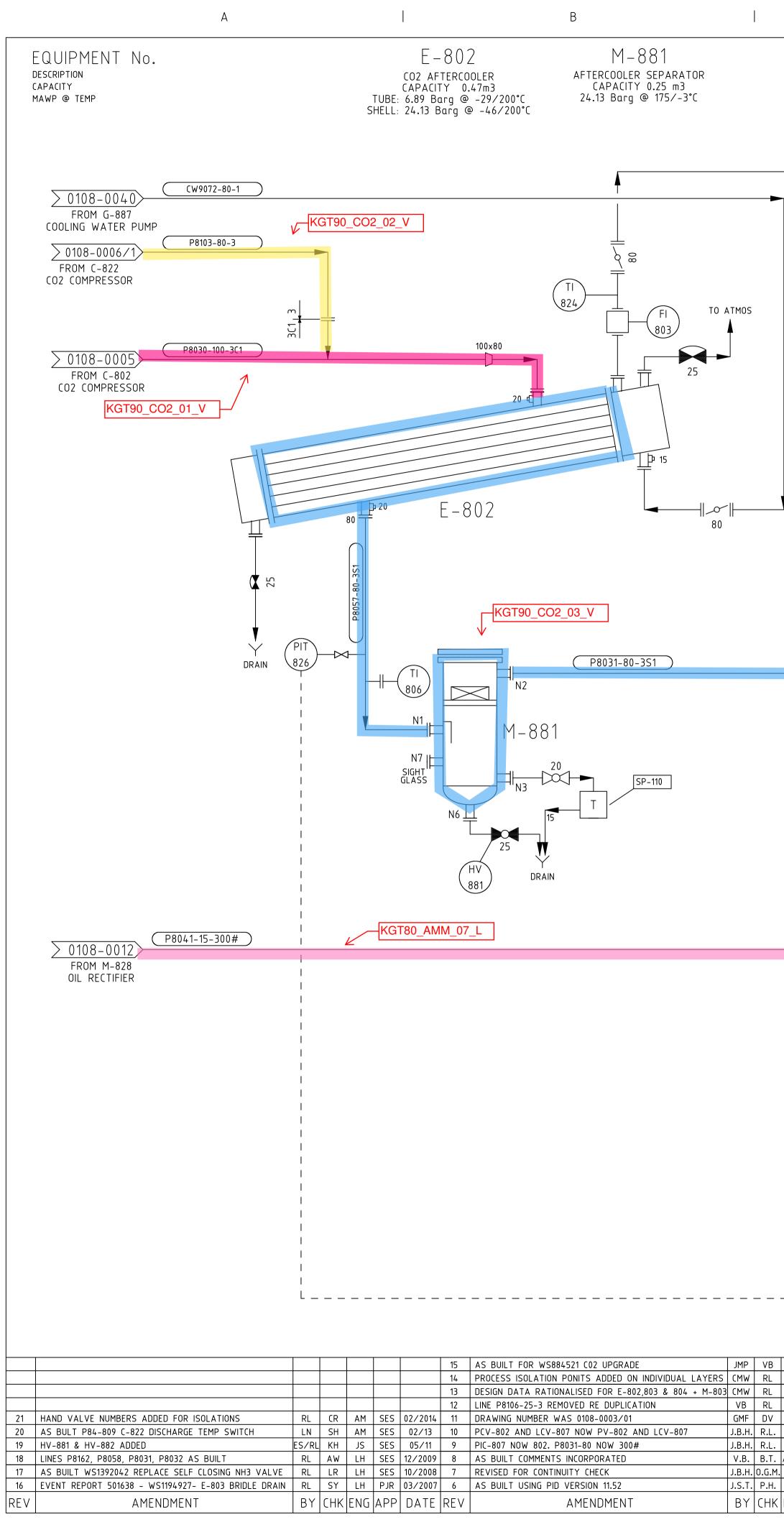


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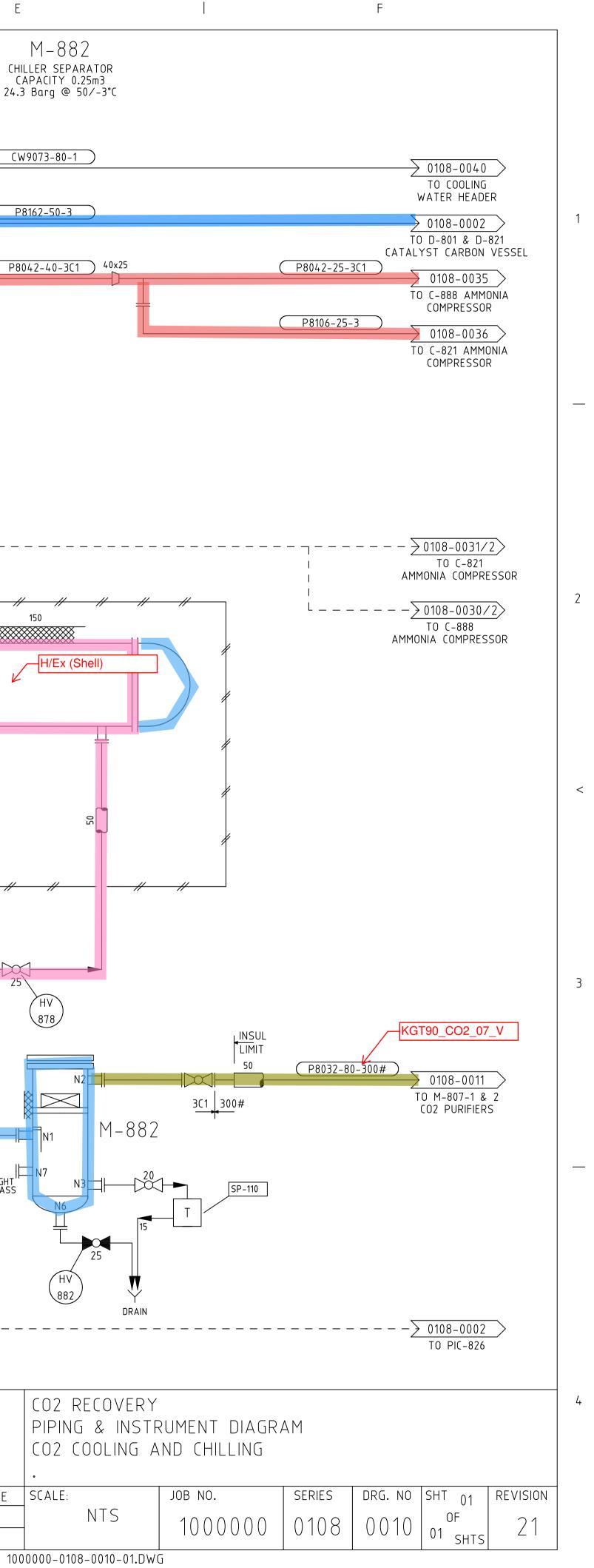
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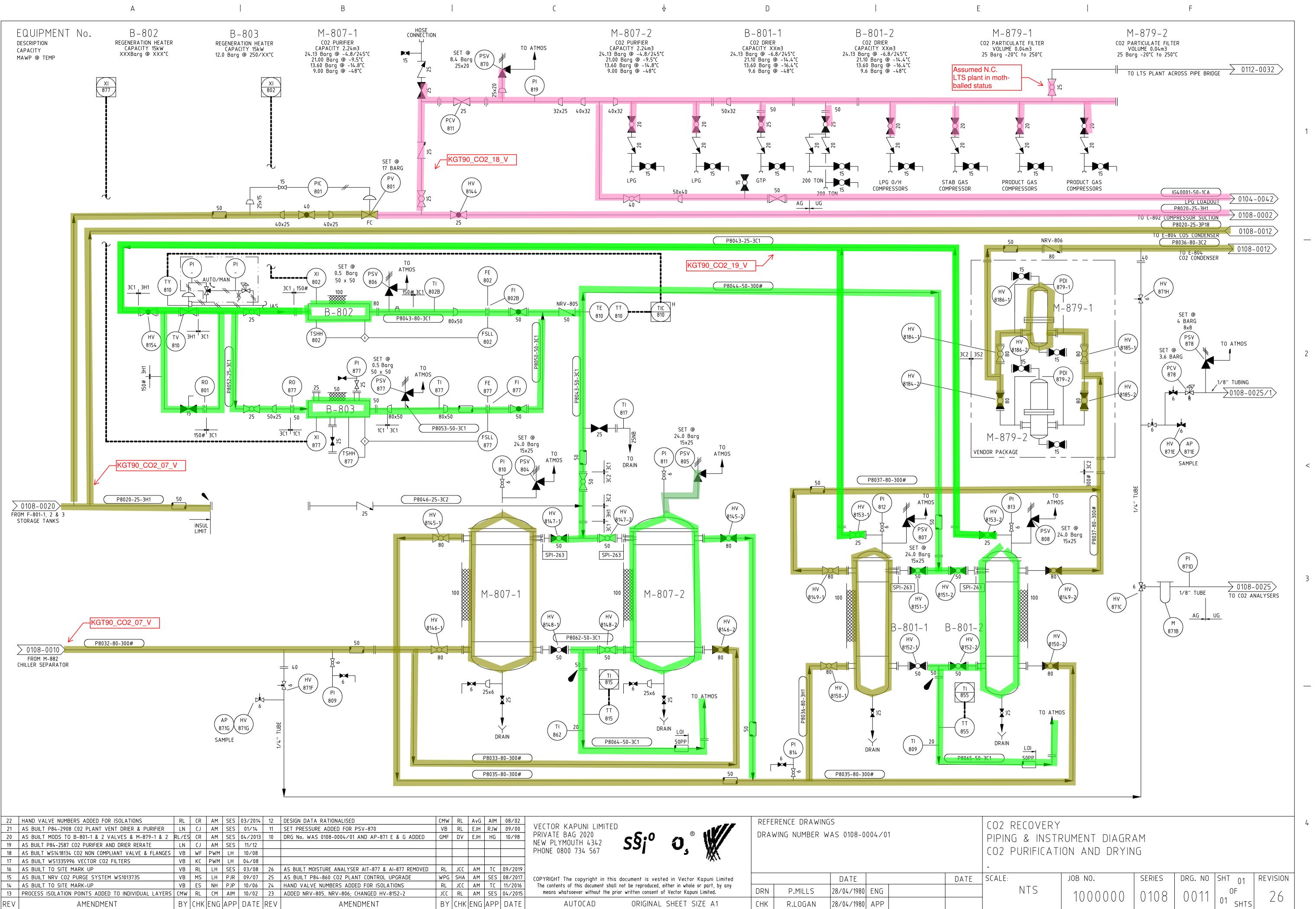
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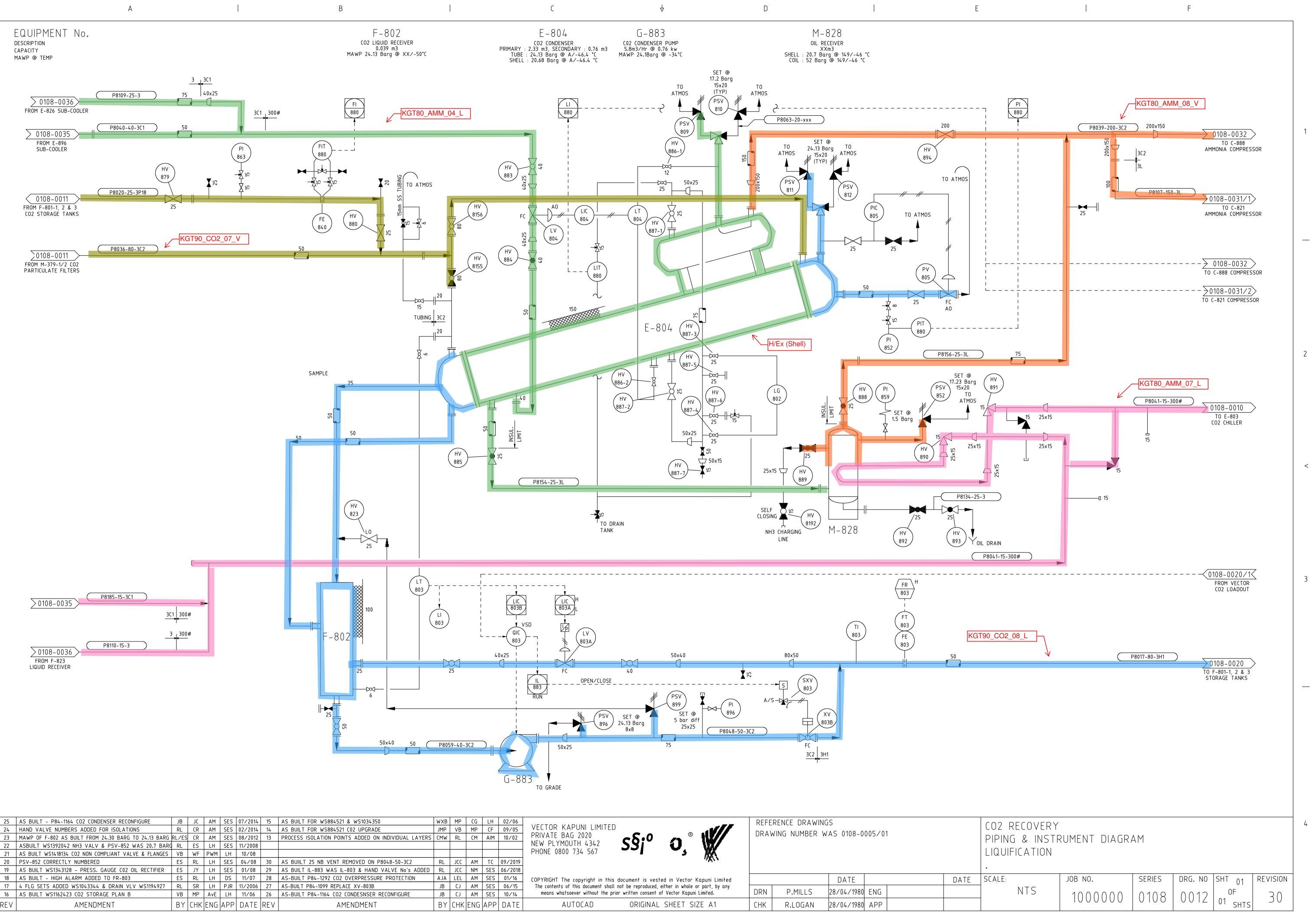
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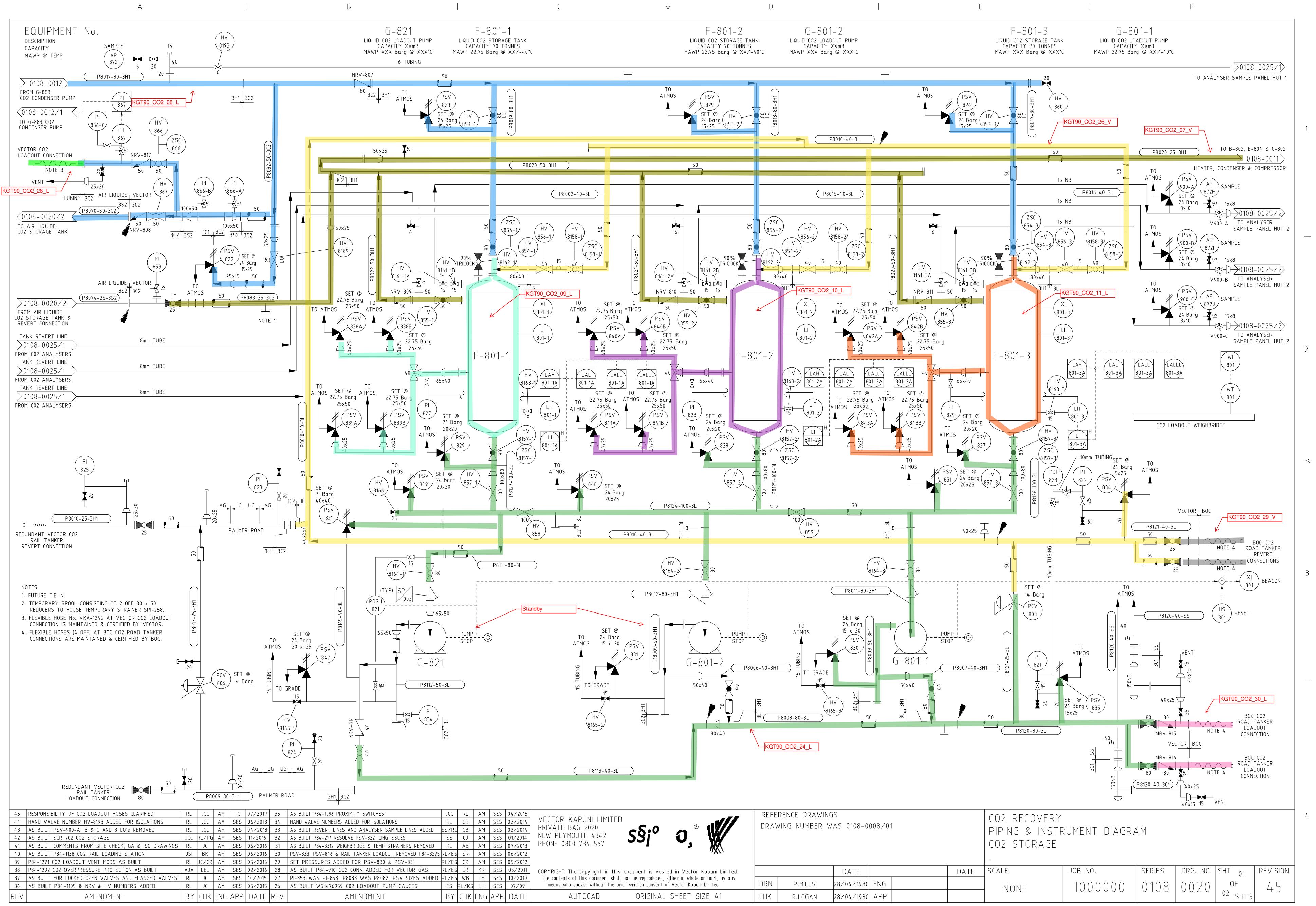
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	AS BUILT – P84–1164 CO2 CONDENSER RECONFIGURE HAND VALVE NUMBERS ADDED FOR ISOLATIONS	JB RL	JC CR			07/201		AS B		OR WS8							K W	(B M P V	р ( 3 М	IP C		)2/06 )9/05	VECTOR KAPUNI LIMITE	D						ERENCE						
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22	ASBUILT WS1392042 NH3 VALV & PSV-852 WAS 20.7 BAR	G RL	ES	LH	SES	11/200	8																NEW PLYMOUTH 4342	33	31	- (										
21	AS BUILT WS1418134 CO2 NON COMPLIANT VALVE & FLANGES	VB	WF	PWM	LH	10/08																	PHONE 0800 734 567				- 5	Ж.								
20	PSV-852 CORRECTLY NUMBERED	ES	RL	LH	SES	04/08	30	AS B	BUIILT	25 NB V	ENT R	REMOVED	D ON P	28048-	-50-302	2	R	_ JC	C A	M T	C 09	9/2019						77 N								
19	AS BUILT WS1343128 - PRESS. GAUGE C02 OIL RECTIFIER	ES	JY	LH	SES	01/08	29	AS B	BUILT I	883 W	AS IL:	-803 &	HAND	VALV	'E No's	s ADDI	ED R	_ JC	C N	IM SE	ES 06	6/2018														•
18	AS BUILT – HIGH ALARM ADDED TO FR-803	ES	RL	LH	DS	11/07	28	AS-B	BUILT F	°84–1292	C02	OVERPR	RESSUR	RE PRO	DTECTIO	ON	A.	A LE	L A	M SE	ES C	01/16	COPYRIGHT The copyright in thi	is documer	nt is ve	sted in	n Vector K	Kapuni Limited					DATE		DATE	SC
17	4 FLG SETS ADDED WS1043344 & DRAIN VLV WS1194927	RL	SR	LH	РJR	11/200	6 27	AS-B	UILT P	84-1099	REPLA	CE XV-	803B				J	з   с.	JA	M SE	es   o	06/15	The contents of this document sha	ıll not be r	reproduced	d, either	in whole or	r part, by any								-
16	AS BUILT WS1162423 CO2 STORAGE PLAN B	VB	MP	AvE	LH	11/06	26	AS-B	BUILT F	984–1164	C02	CONDES	NSER F	RECONF	FIGURE	-	J	3 C.		M SE			means whatsoever without the p						DRN	P.M	1ILLS		28/04/1980 ENG			
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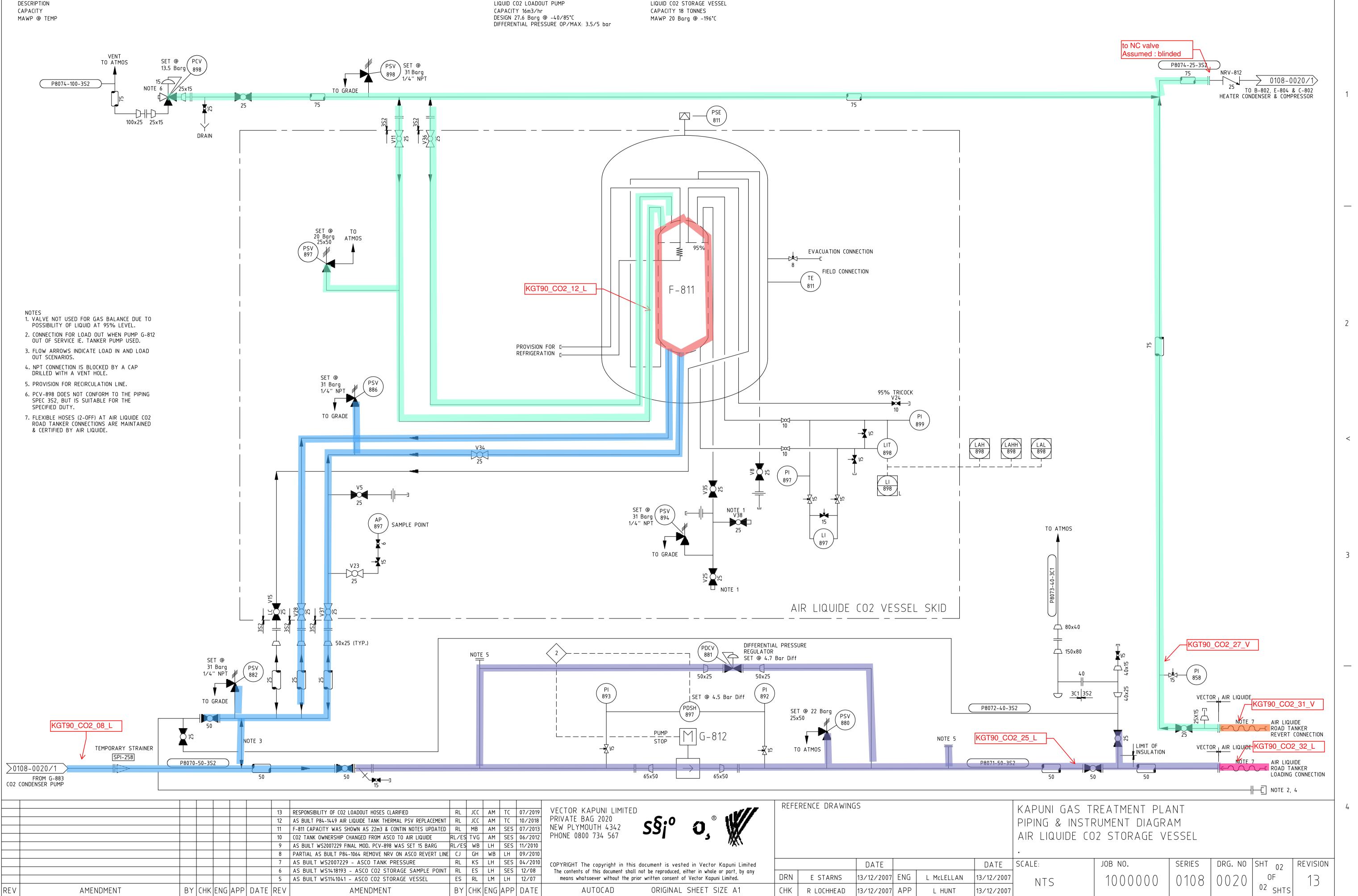
SWITCHES		RL	AM	SES	04/2015		REF
FOR ISOLATIONS	RL	CR	AM	SES	02/2014		DRA
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SV-822 ICING ISSUES	SE	CJ	AM	SES	01/2014		
GE & TEMP STRAINERS REMOVED	RL	AB	AM	SES	07/2013	PHONE 0800 734 567	
NKER LOADOUT REMOVED P84-3275	RL/ES	SR	AM	SES	06/2012	<b>2X</b> \\	
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P.MILLS	28/04/1980	ENG		NONE	1000000	0108	
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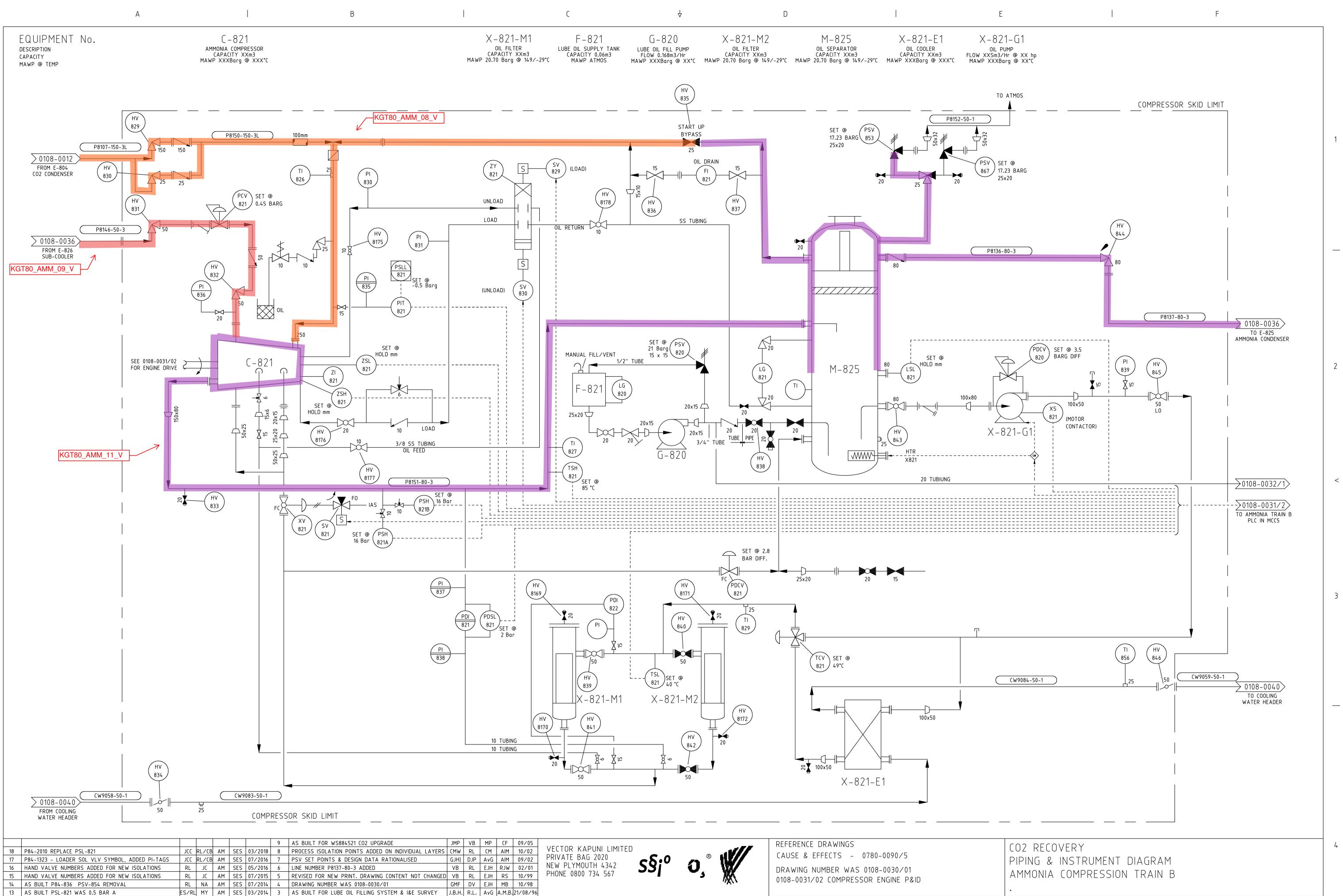
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G-812 LIQUID CO2 LOADOUT PUMP

F-811 LIQUID CO2 STORAGE VESSEL

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10 AS BUILT

REV

12 HAND VALVE NUMBERS ADDED FOR ISOLATIONS

AMENDMENT

RL AC AM SES 10/2013 2 AS BUILT COMMENTS INCORPORATED

ES RL LH PJR 06/06 D AS BUILT USING PID VERSION 11.52

AMENDMENT

11 AS BUILT DRAIN RELOCATED ON P8151 & P8152 WAS P1852 ES RL AM SES 12/2012 1 REVISED FOR CONTINUITY CHECK

BY CHK ENG APP DATE REV

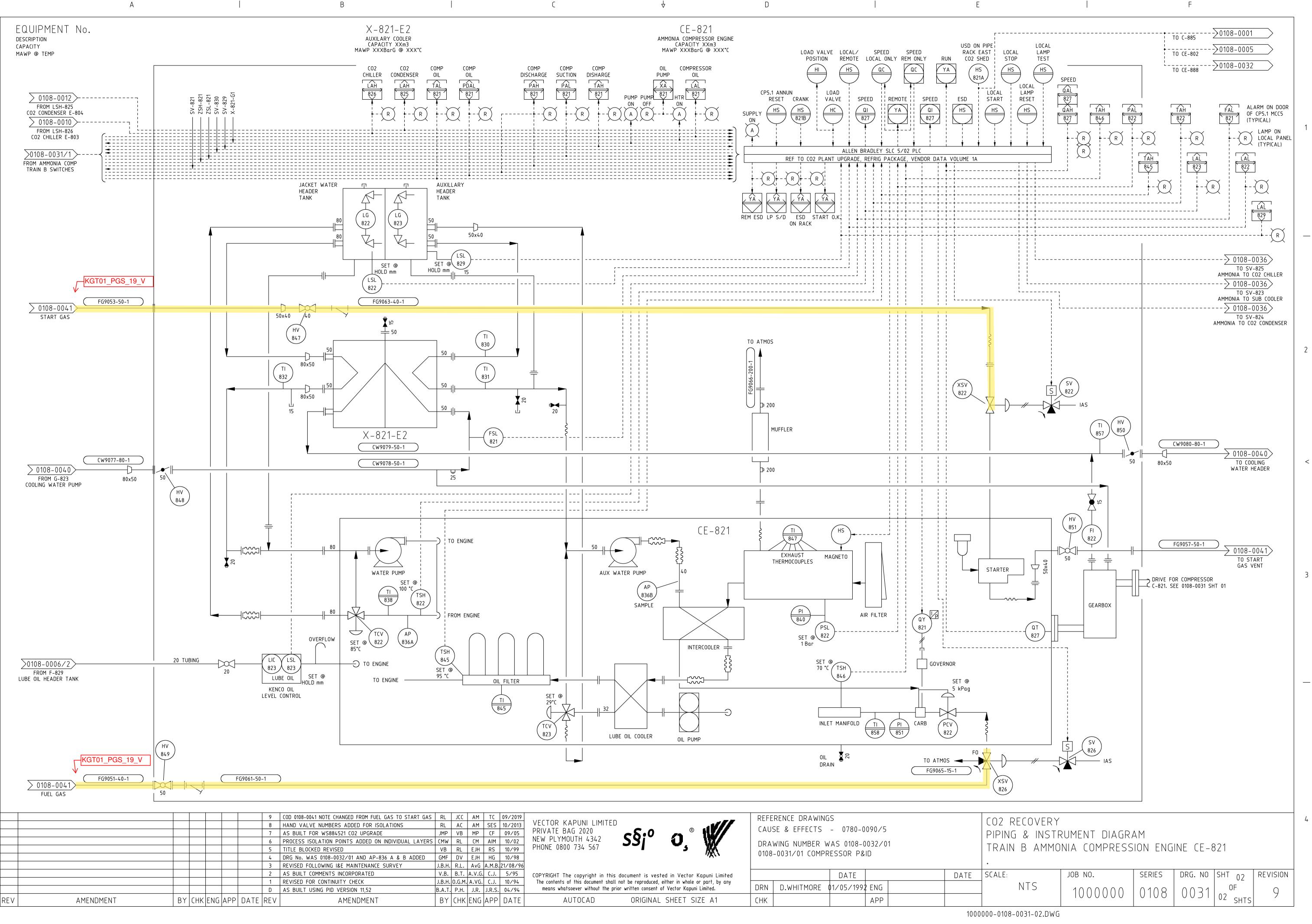
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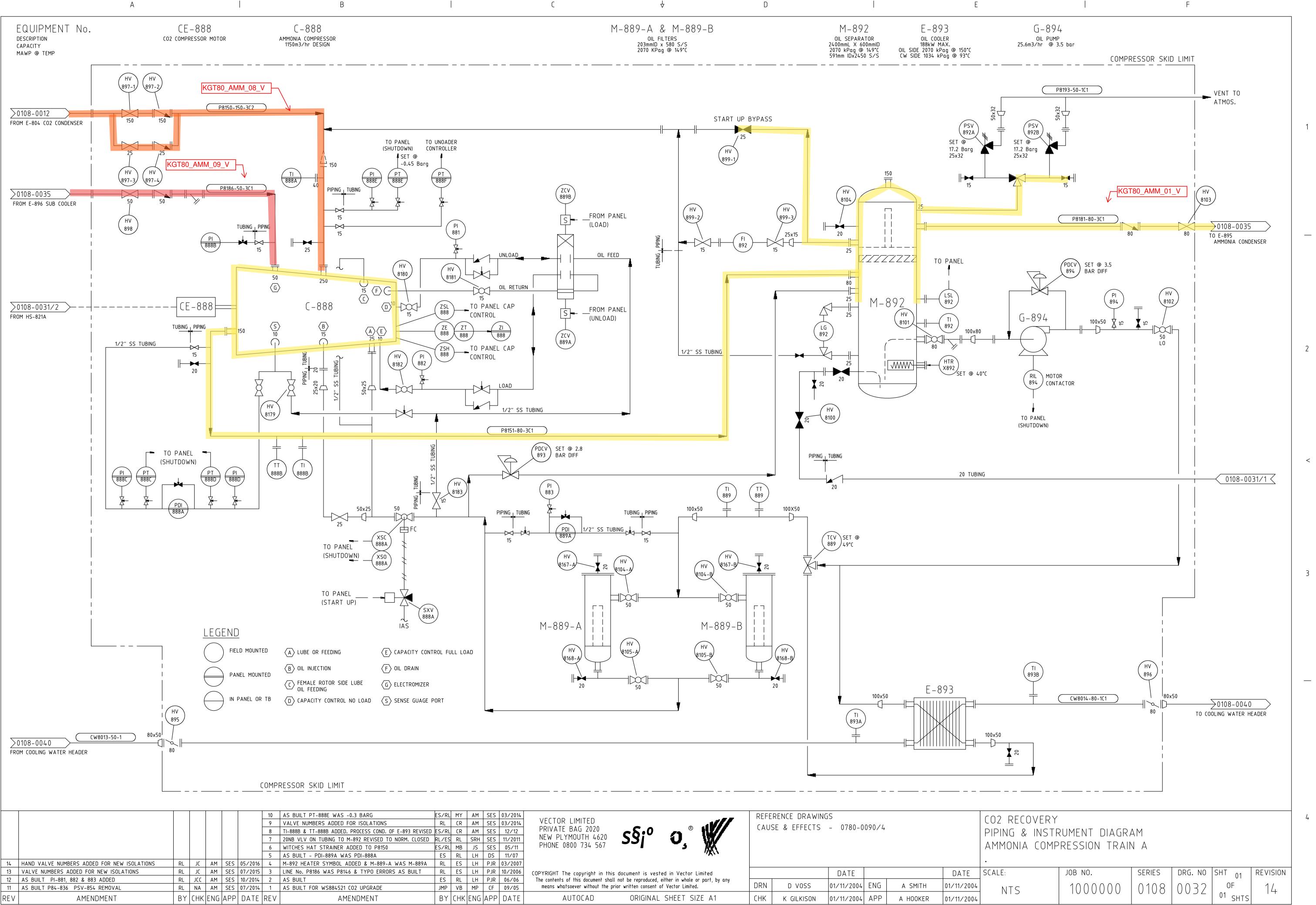
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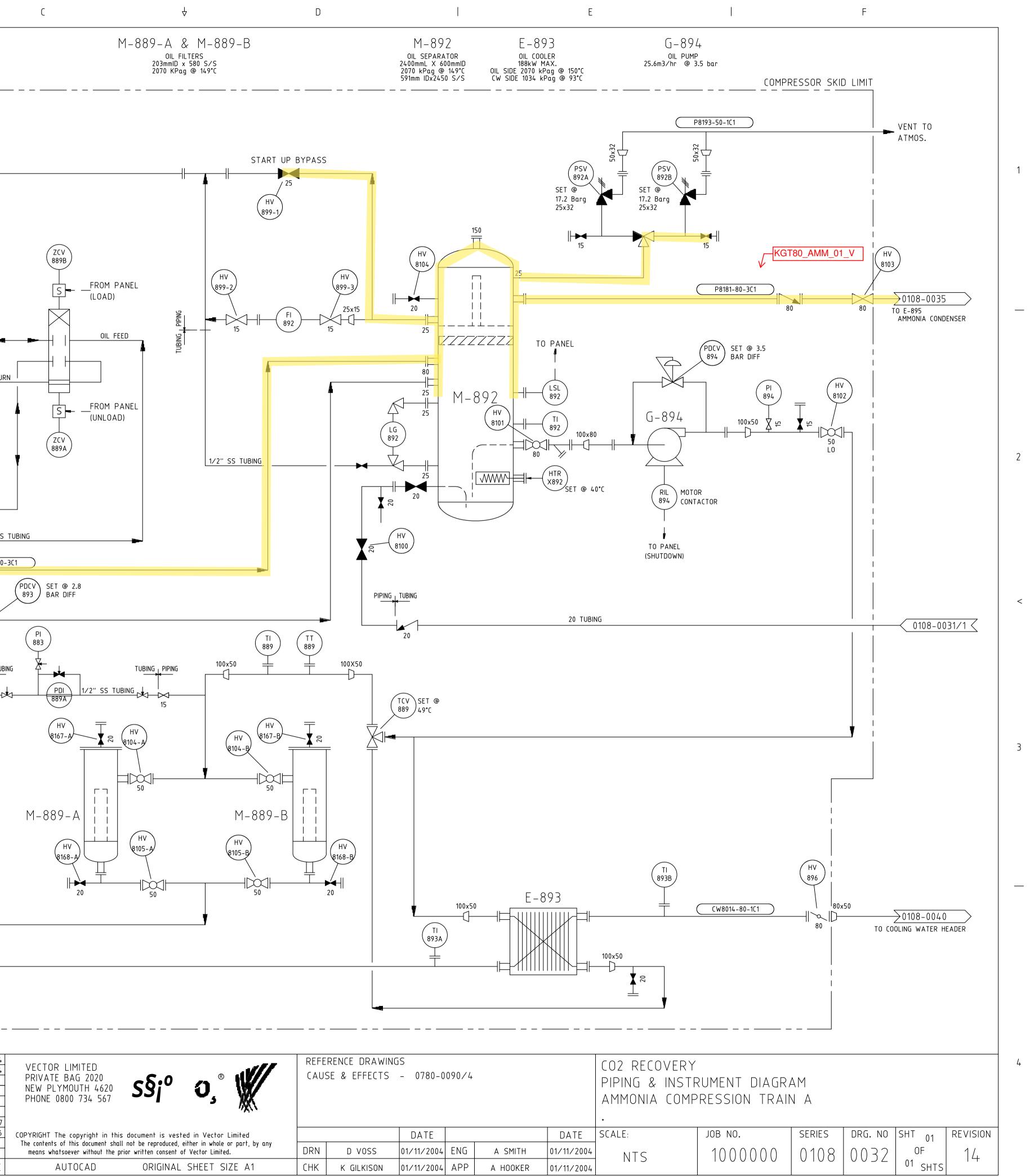




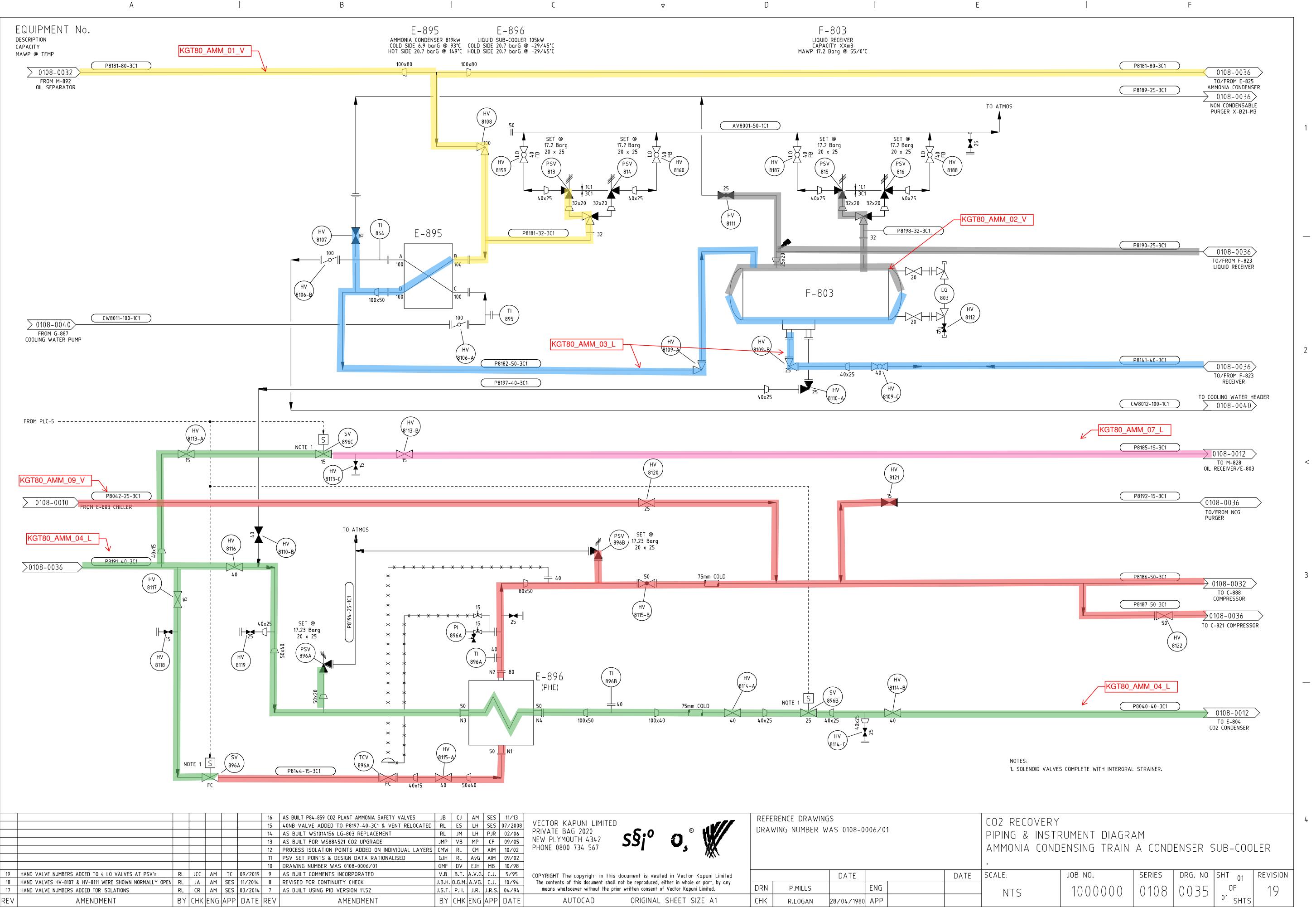
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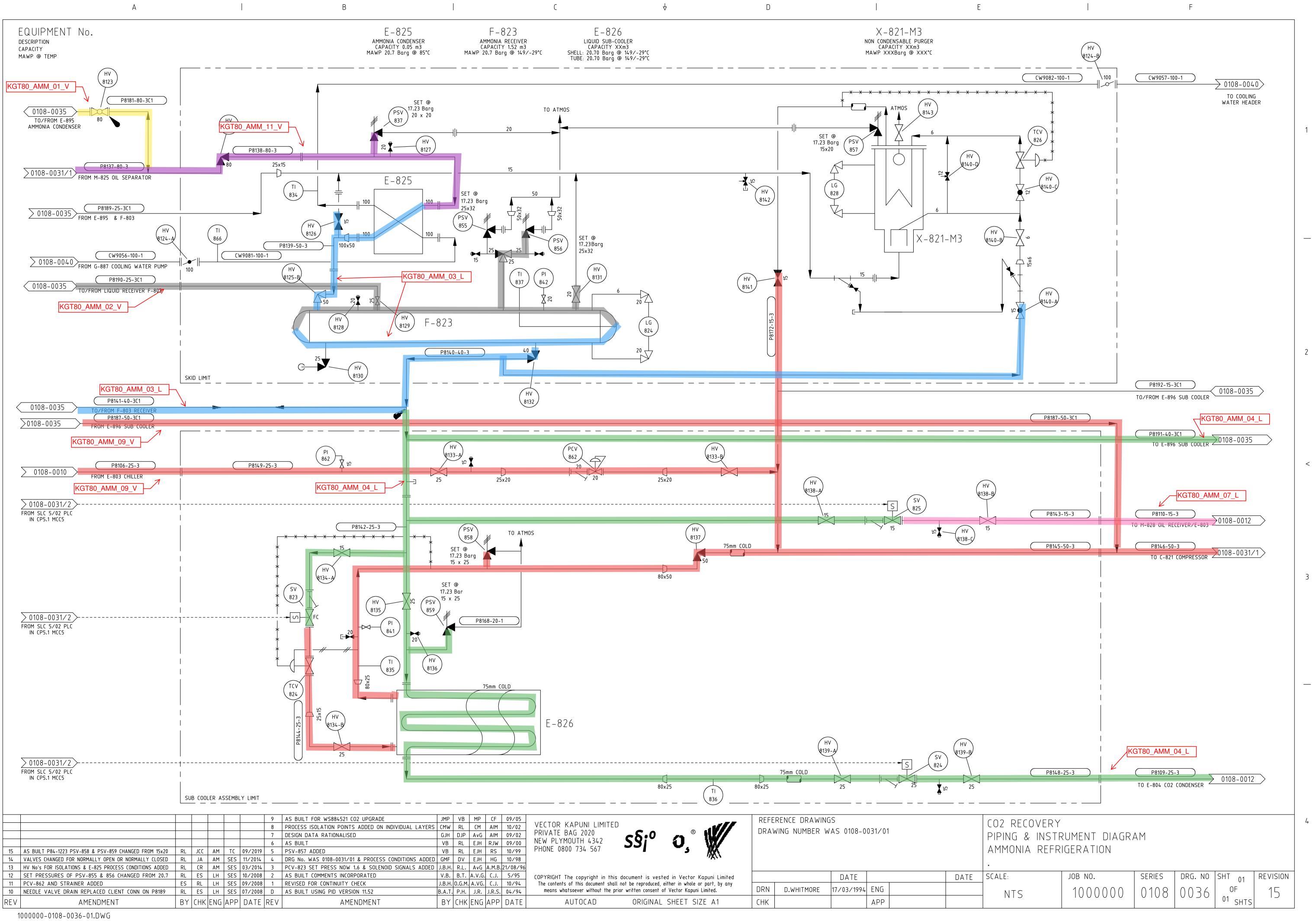


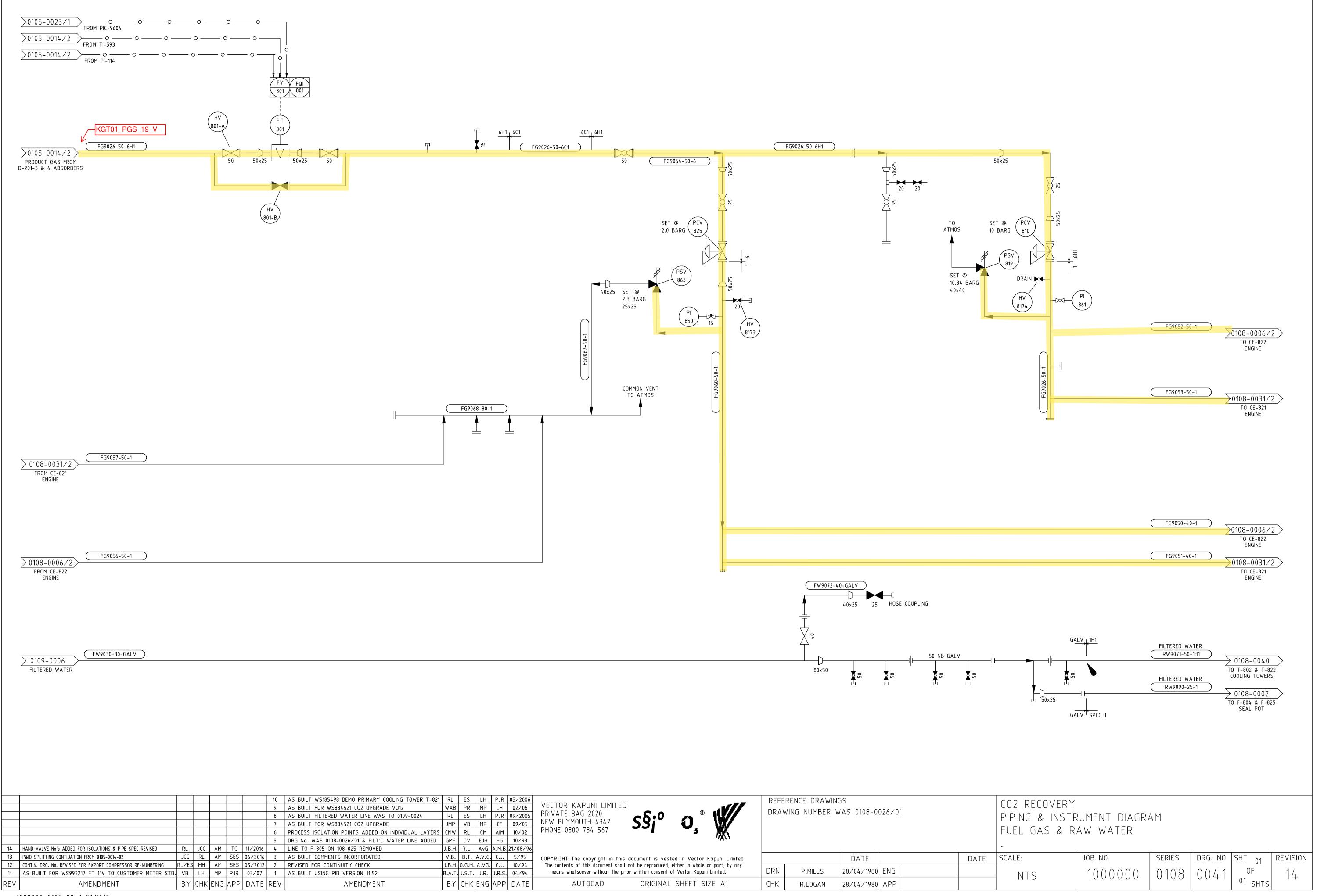
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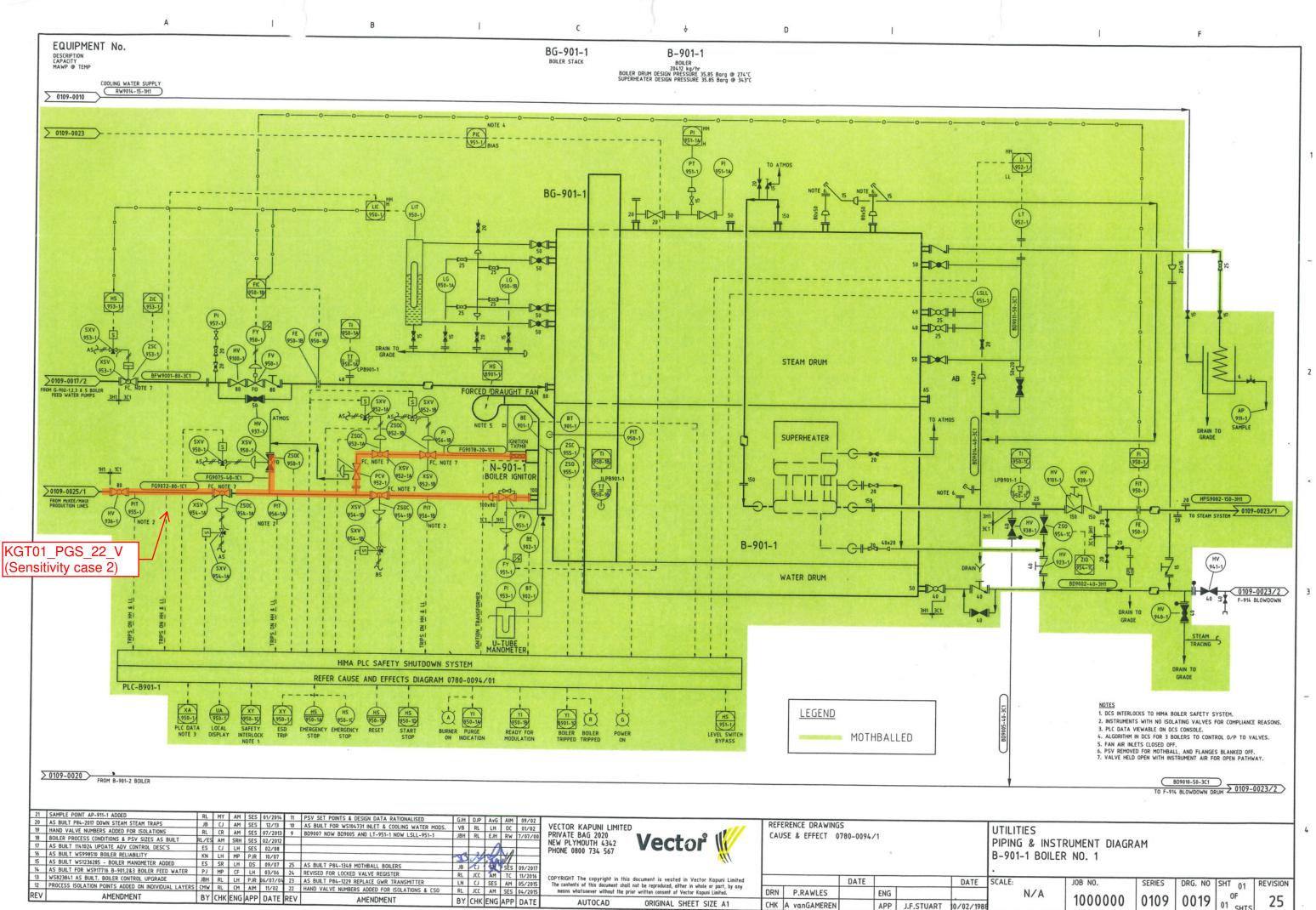
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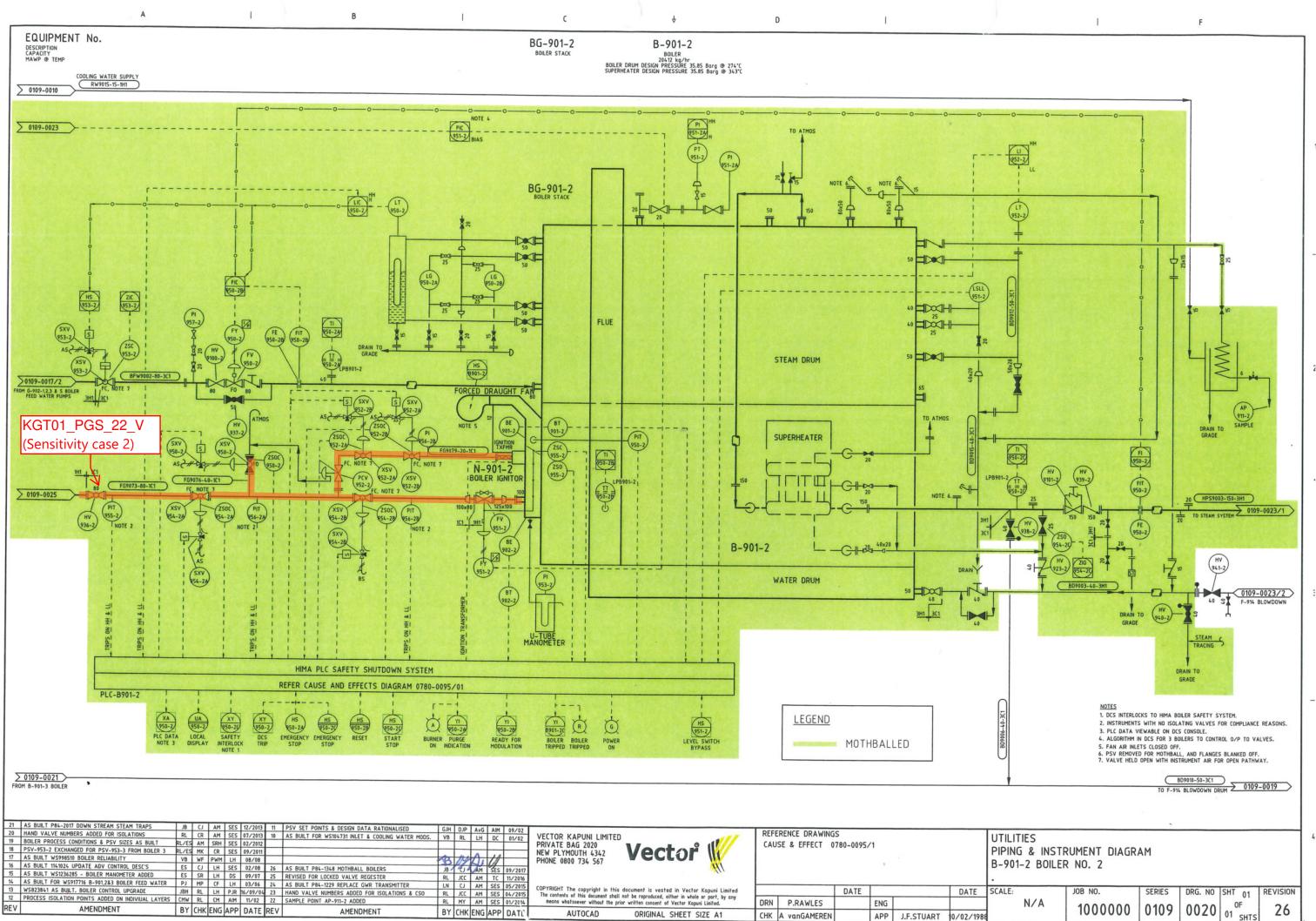
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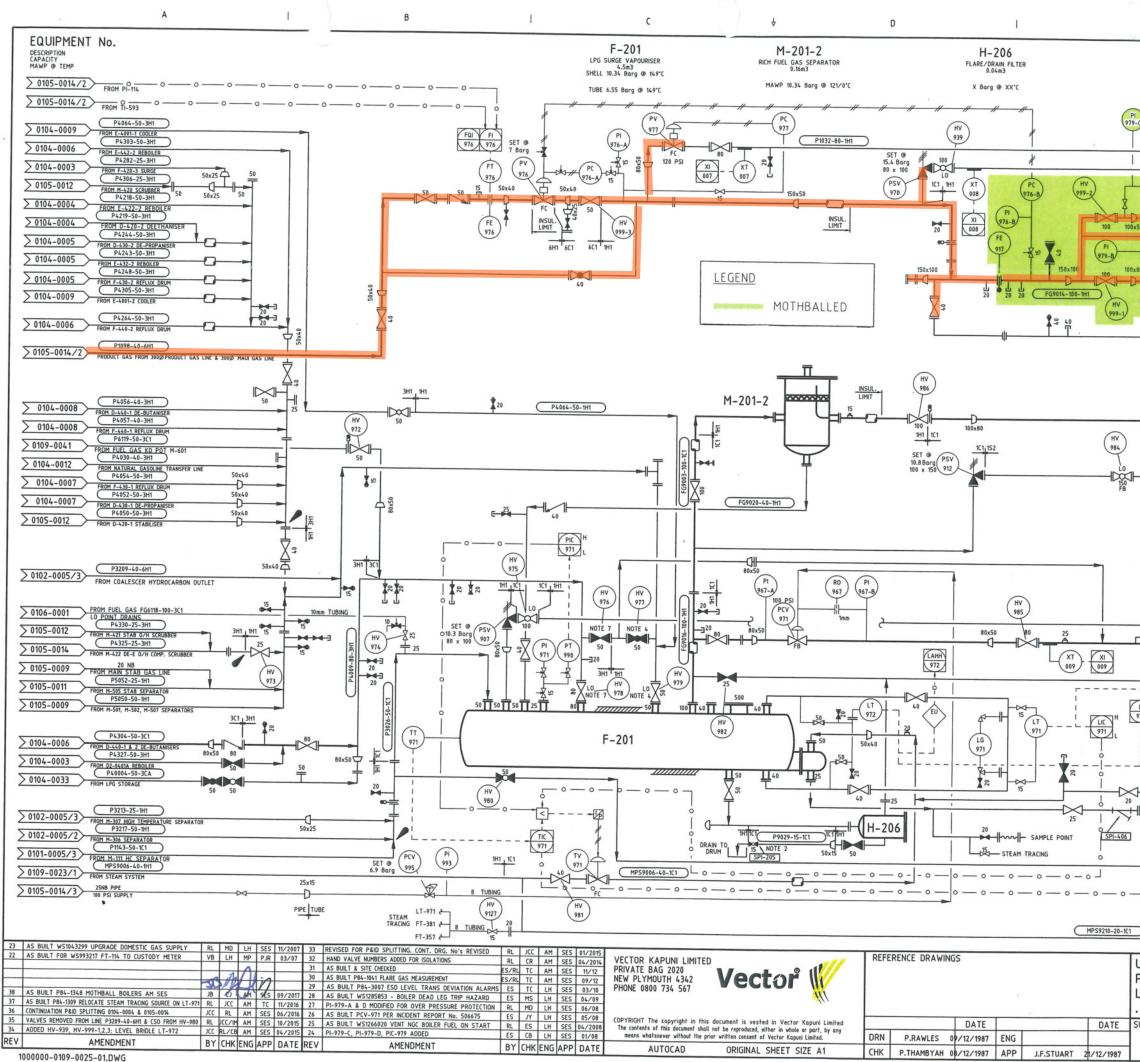


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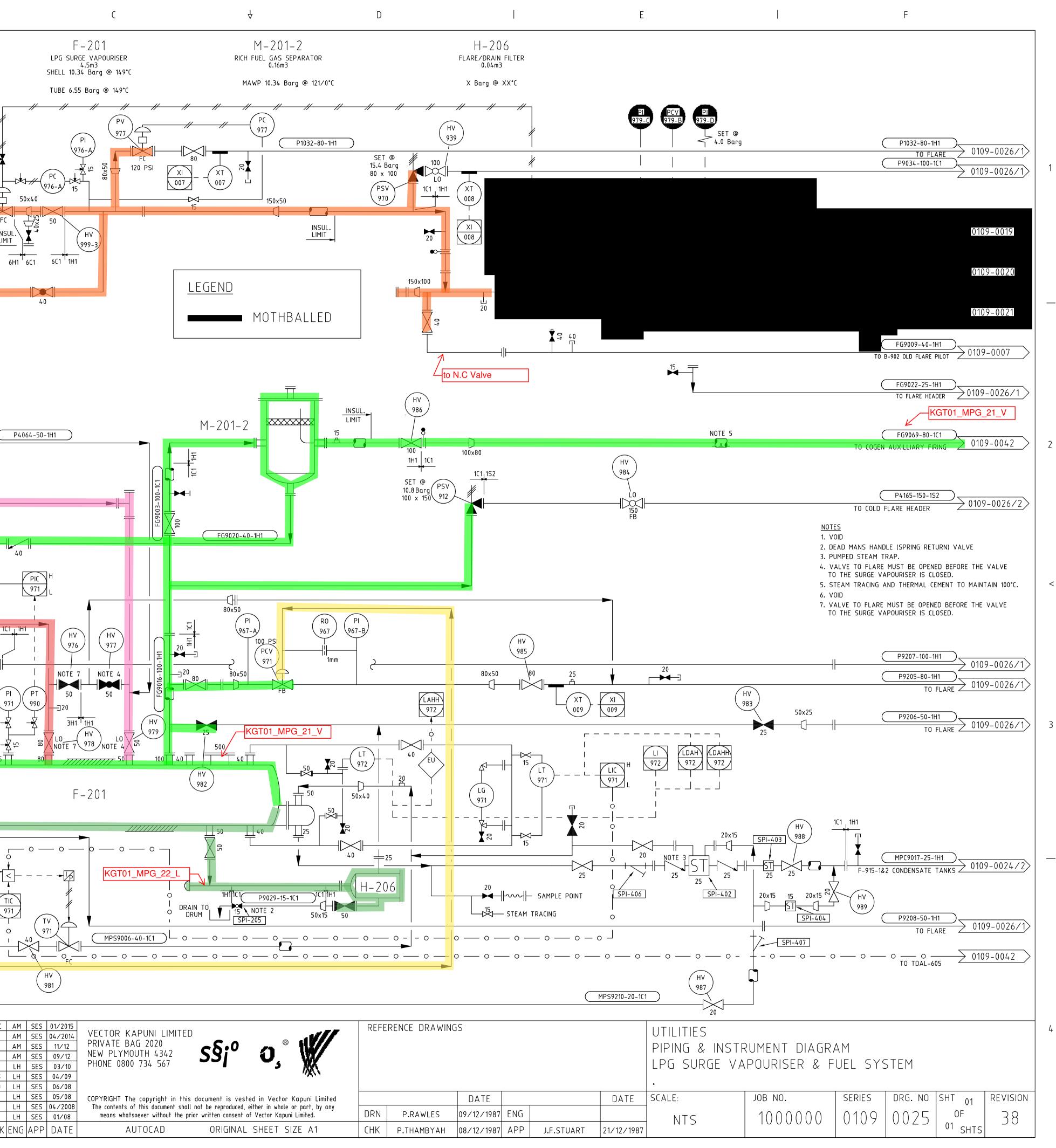
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	hballed.		FG9022-25 TO FLARE H FG9069-80 N AUXILLIARY F	-1C1	09-0026/1	2
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	3. 1 4. v 5. 5 6. v 7. v	DEAD MANS HAN PUMPED STEAM VALVE TO FLAR 'O THE SURGE V STEAM TRACING VOID VALVE TO FLAR O THE SURGE V	TRAP. E MUST BE OPE APOURISER IS ( AND THERMAL E MUST BE OPEI	NED BEFORE TH CLOSED. CEMENT TO MAIL	NTAIN 100°C.	<
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	SPI-403 (HV 988)	<u>1ст 1н1</u> Т			2	
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	From NC valve	FROM E-4001-1 COOLER P4303-50-3H1									FQI FI 976 976	SET @	
	> 0104-0006 From NC valve	FROM E-442-2 REBOILER				Δεειι	med : N	ormall	N .			7 Barg	
	> 0104-0003	FROM F-420-3 SURGE	50x25	<b>5</b> ↓			low (NN		y		(FT 976)	976	
	> 0105-0012 From NC valve	P4306-25-3H1		<b>↓</b> >5 50						50		×40	Ý
	> 0104-0004	FROM E-422-2 REBOILER							4				FC
	From NC valve	P4219-50-3H1 FROM D-420-2 DEETHANISER		-From N	IC va	lve					(FE 976)	Ē ļ	INSU LIMIT
	> 0104-0005	← ← P4244-50-3H1 ← FR <u>OM D-430-2 DE-PROPANI</u> SER ←		}			]				$\bigcirc$		6
	> 0104-0005	FROM E-432-2 REBOILER		C valve									
	> 0104-0005	P4248-50-3H1	om NC	valve									
	From NC valve	P4305-50-3H1 FROM E-4001-2 COOLER		)					20×40				
	From NC valve	┣╮		•	1 2	0							
	0104-0006	FROM F-440-2 REFLUX DRUM		}	2		50×40						
		P1098-40-6H1											
	> 0105-0014/2	PRODUCT GAS FROM 300ØPRODUCT	GAS LINE	& 300Ø MA	UI GAS	LINE	$\stackrel{-}{\bigtriangledown}$		K		PGS_22_V		
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		(P4056-40-3H1)	From N	IC valve		∽	–   ↓	,		3H1 1H1	20		
	0104-0008	FROM D-440-1 DE-BUTANISER (P4057-40-3H1)	From	NC valv	e		<b>2</b> 5 L		HV	∞ 50	Τ		
	0104-0008	FROM F-440-1 REFLUX DRUM	<u>الــــــ</u>						972	Assumed : No Flow (N			
	> 0109-0041	P6119-50-3C1 FROM FUEL GAS KO POT M-601	Fr@	om NC v	alve	<b>–</b> – –	_				,		
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	> 0105-0012	P4050-50-3H1 FROM D-420-1 STABILISER	Fror	n NC val	ve			3H1		,	L		
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	> 0106-0001	From NC	valve		/	15		10mm	ТUBING	<u>ш</u>	о Ц 		
Assumed : NN	JF 0105-0012	LO POINT DRAINS P4330-25-3H1		3H'	1 <sub>1</sub> 1H1	<b>▶</b> ◀−				22	SET @ PSV O10.3 Barg		$\sim$
Assumed : N	NF	FROM M-421 STAB 0/H SCRUBBER				25		<b>← ▶</b> ← ¢	ヨ 田 HV 974	25	80 × 100 907	<u>↓</u> \$	PI
	> 0105-0014	TROM M-422 DE-E 0/H COMP. SCRUBB	<sup>ER</sup> NC va	alve 🧹				•	-08-600 Hd	•	ō		
F	<u>&gt; 0105-0009</u> rom NC valve	FROM MAIN STAB GAS LINE				(HV 973					0		
	KGT01_RCS_01_L	FROM M-505 STAB SEPARATOR								Į			
KGTO	> 0105-0009 5 DBT_11_V	FROM M-501, M-502, M-507 SEPARATO	IRS	3C1	<sub>1</sub> 3H1				P3026-50-1C1				
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	> 0104-0006												
		FROM D-440-1 & 2 DE-BUTANISERS	80	x50 80				80		971			
	> 0104-0003	P4327-50-3H1 FROM D2-0401A REBOILER	80	×50 80			50		80×50			50	
	> 0104-0003 > 0104-0033	P4327-50-3H1				•						50	
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	D104-0033          From NC valve         0102-0005/3         From LC valve         0102-0005/2         0101-0005/3         0109-0023/1         0105-0014/3	P4327-50-3H1 FROM D2-0401A REBOILER P40004-50-3CA FROM LPG STORAGE P3213-25-1H1 FROM M-307 HIGH TEMPERATURE SEP P3217-50-1H1 FROM M-306 SEPARATOR P1143-50-1C1 FROM M-111 HC SEPARATOR MPS9006-40-1H1 FROM STEAM SYSTEM 25NB PIPE 100 PSI SUPPLY	ARATOR	50 50		MPG SES PJR	23_L 21	2 50×25 25×15 25×15 25×15 25×15 33 32	SET C 6.9 BO	PCV PCV 995 LT-97 STEAM TRACING FT-38 FT-35 PLITTING. CONT. ADDED FOR ISOL	PI 993 1H 993 8 TUBIN 993 8 TUBIN 9127 81 2 8 TUBING 9127 9127 9127 9127 9127 9127 9127 9127	) - O	JCC CR
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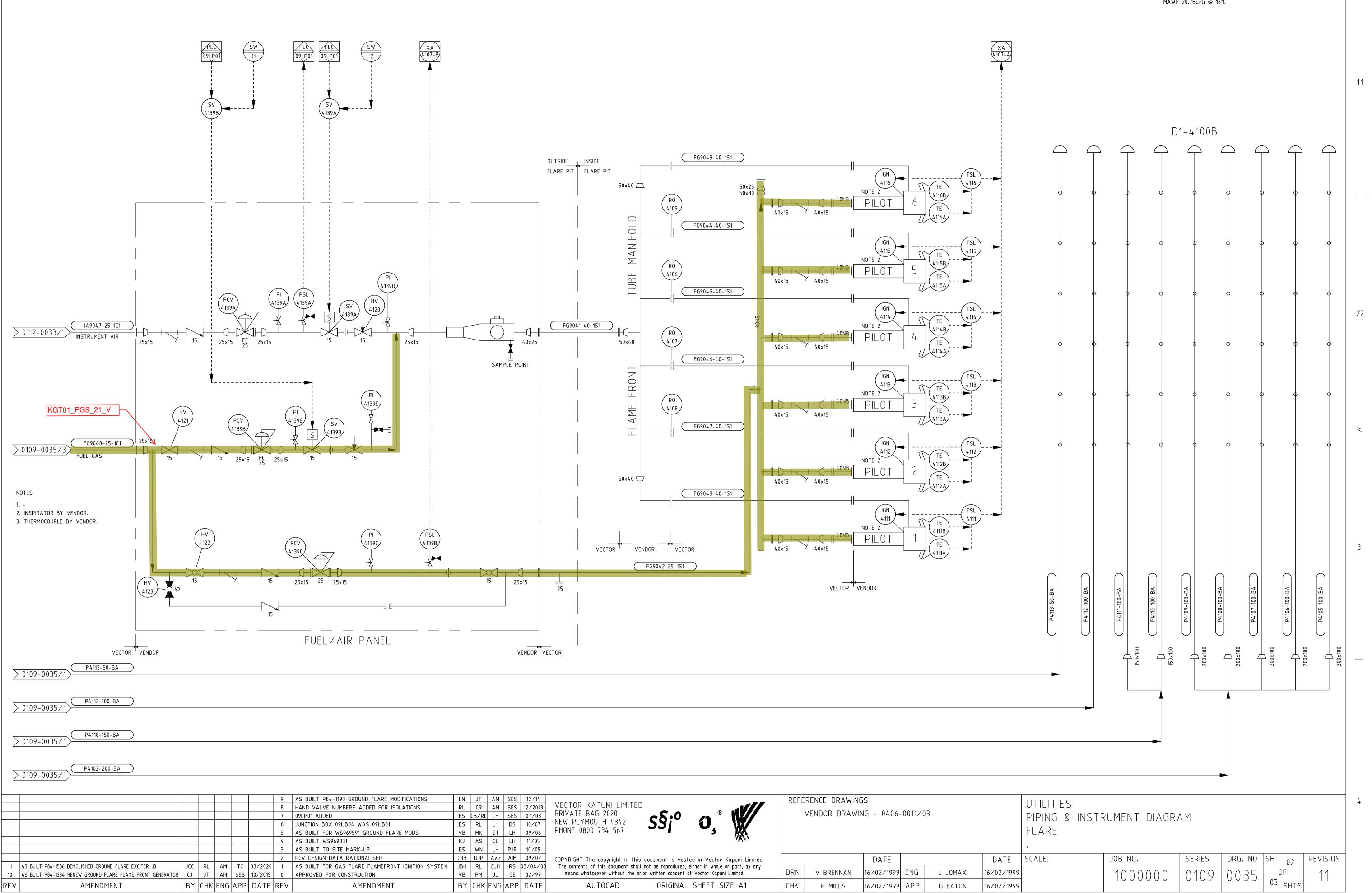
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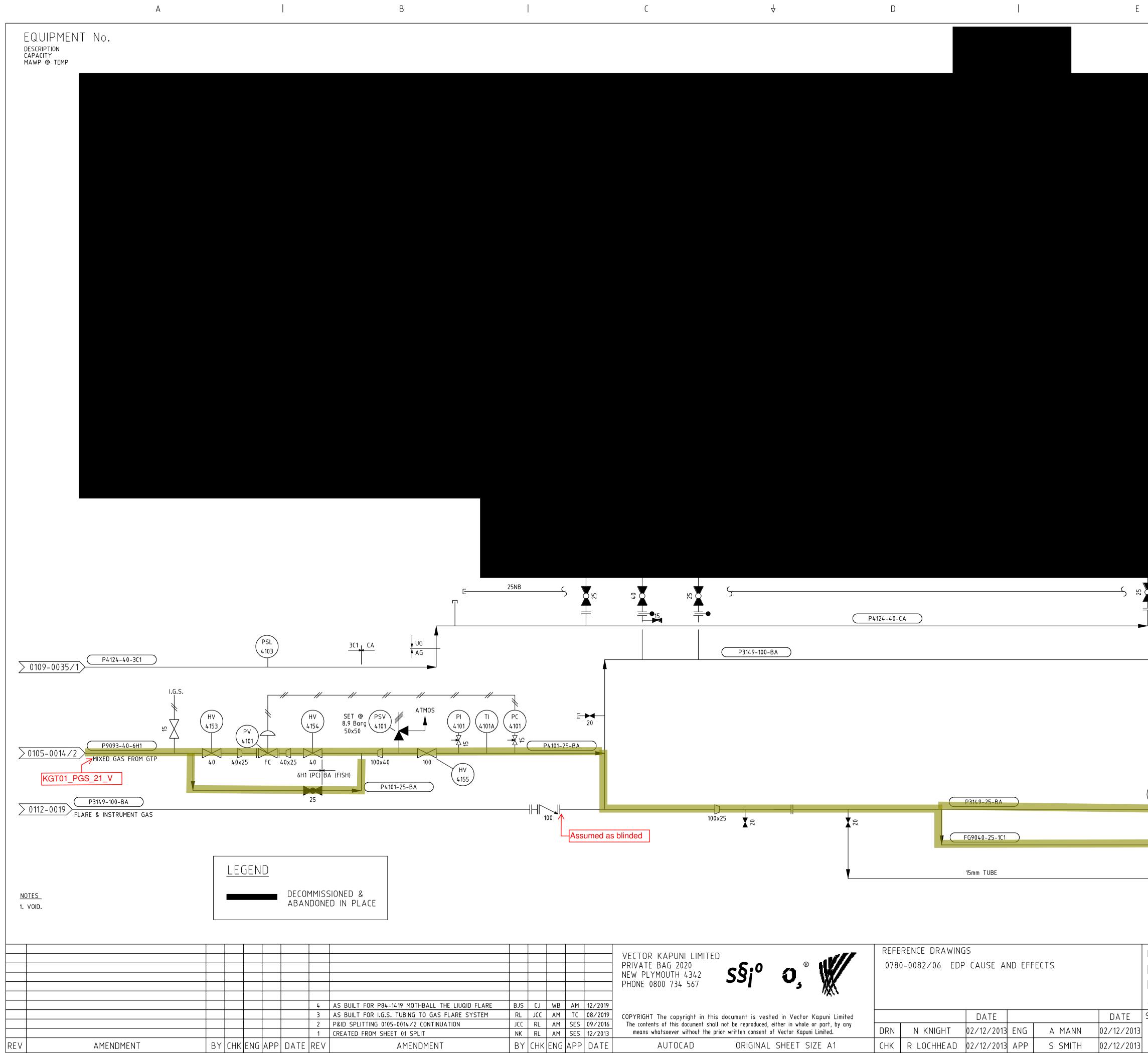


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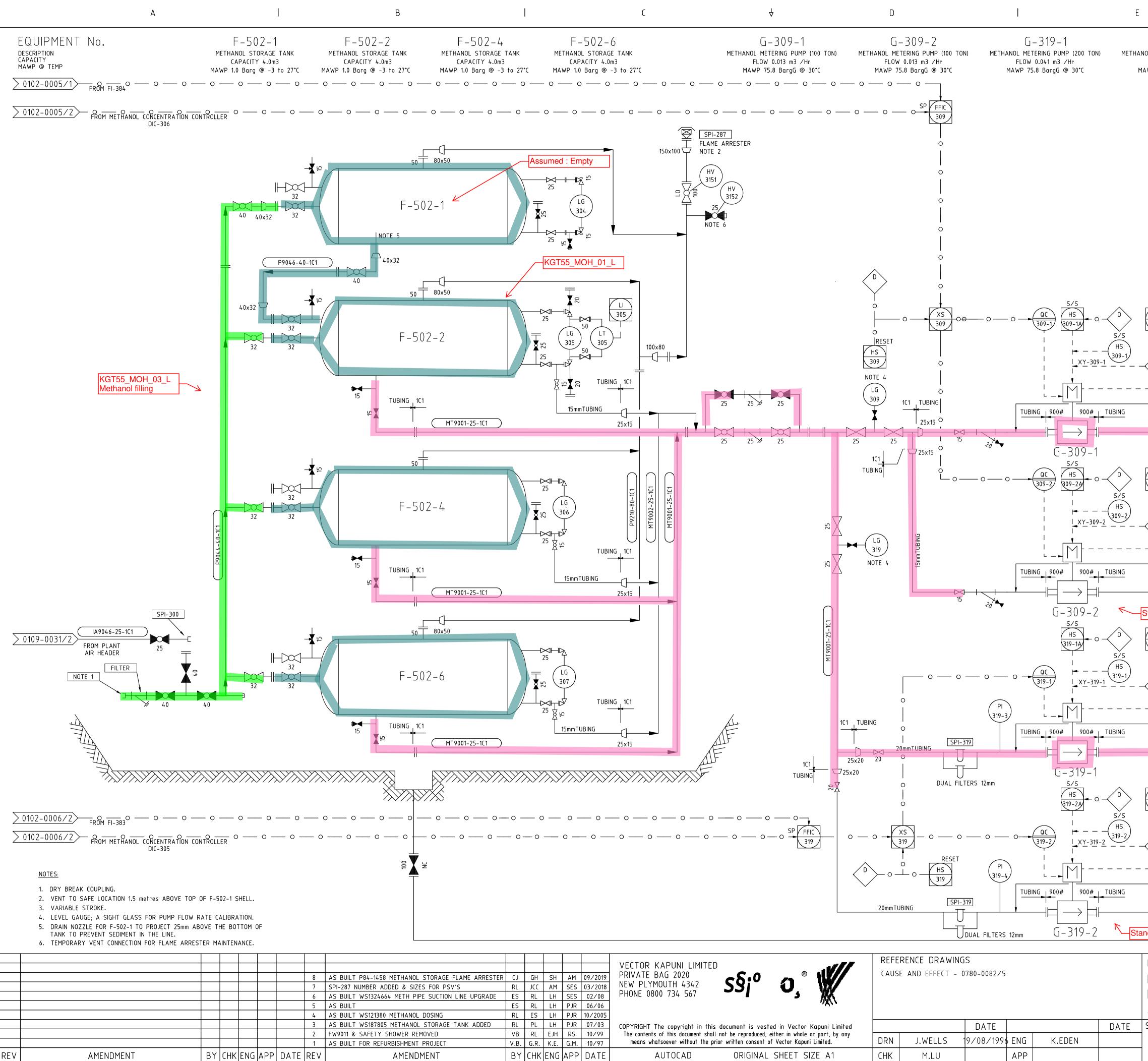


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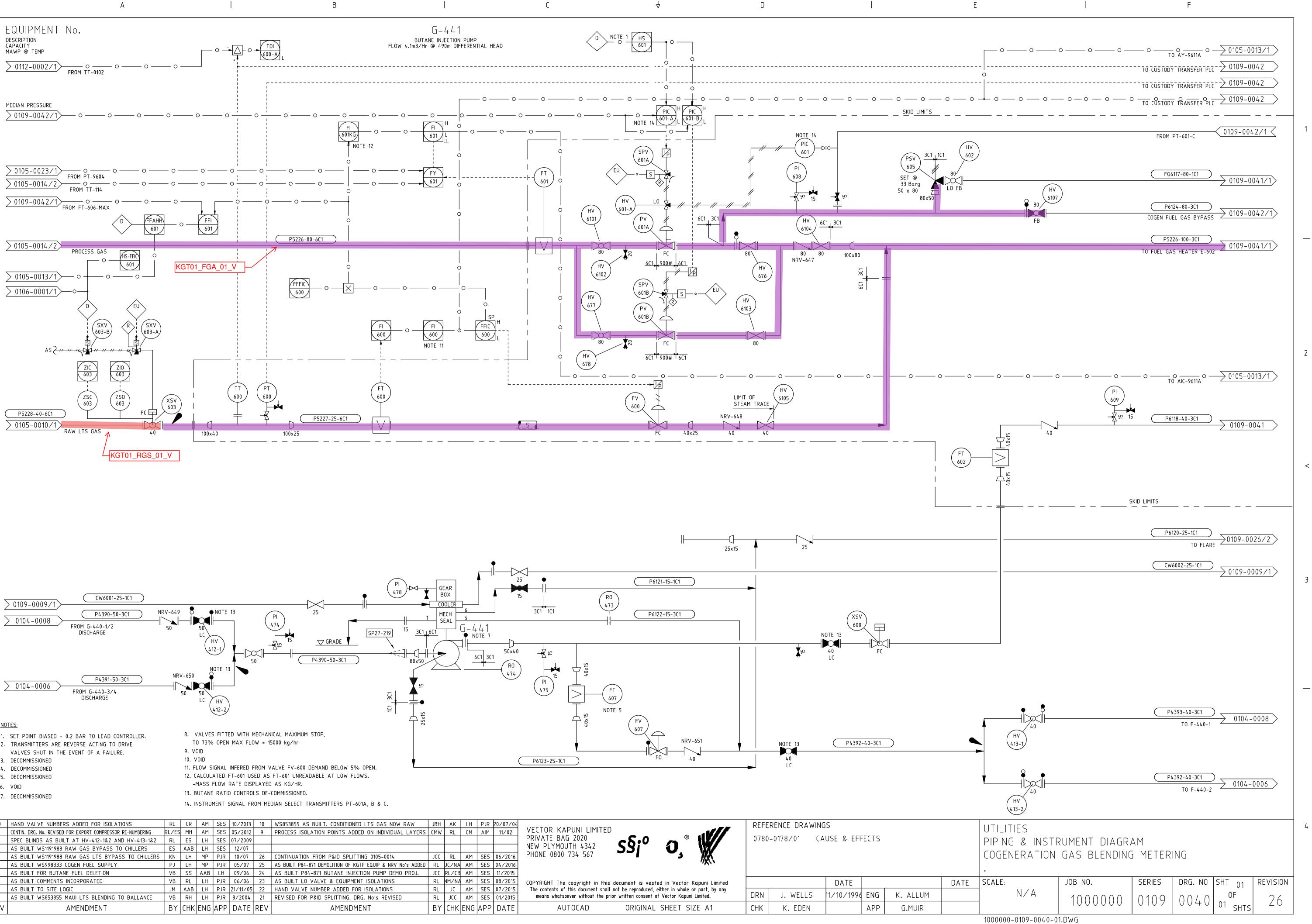


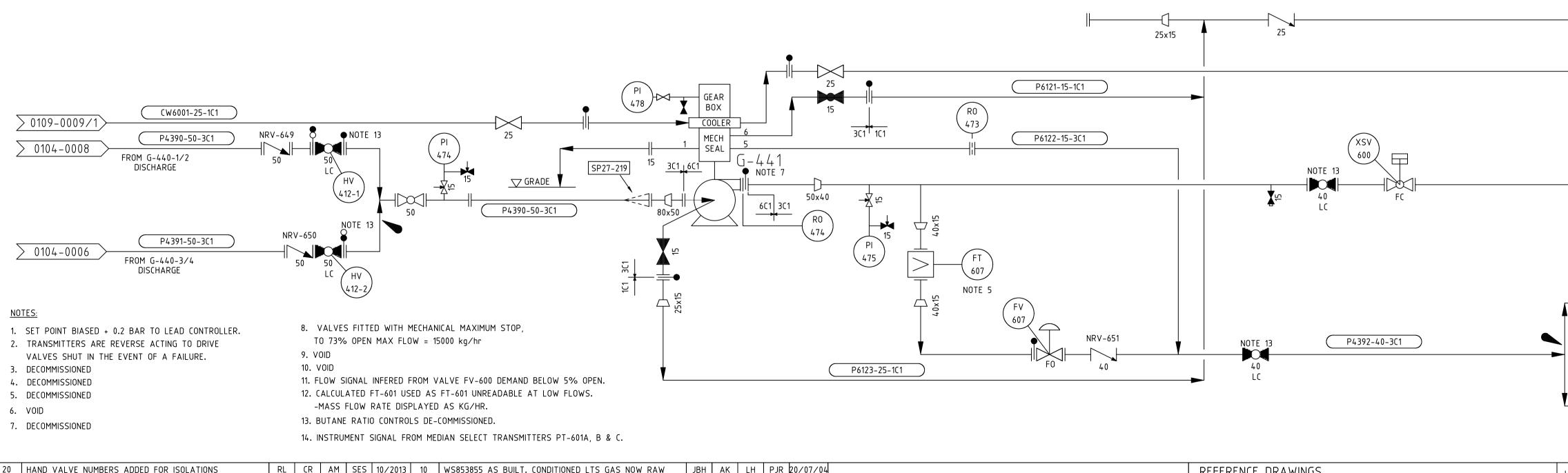
SET @	
PI KGT55 MOH 02 L	
15 15 TO E-303-1/2 GAS GAS	
HEAT EXCHANGERS (100 TON)	
O ES SET @ T/ Data	
74 Barg     15mm TUBING     0104-0004       8 x 8     PI     309-2       10 DE-ETHANISER OVERHEAD     P4208-100-3H1	
TO E-304 GAS LIQUID HEAT EXCHANGER	
ES SET @ 8 x 8	
- J PSV 319-1	
15 15 TO E-313-1/2 GAS GAS HEAT EXCHANGERS (200 TON)	
$\left[\begin{array}{c} IL\\ \hline 319-2 \end{array}\right] \circ - \left[\begin{array}{c} D\\ \hline \end{array}\right]$	
SET @ FS 74 Barg 8 x 8	
L ES 74 Barg	
FS     74 Barg       8 x 8     Pl       319-2     319-2	
PSV 319-2 15 15 15 100NB 0109-0030/2	
PSV 319-2 15 15 100NB	
Ind-by     100NB       TO CATCH BASIN A-706       UTILITIES       PIPING & INSTRUMENT DIAGRAM       METHANOL STORAGE AND METERING       .	
VTILITIES PIPING & INSTRUMENT DIAGRAM METHANOL STORAGE AND METERING	

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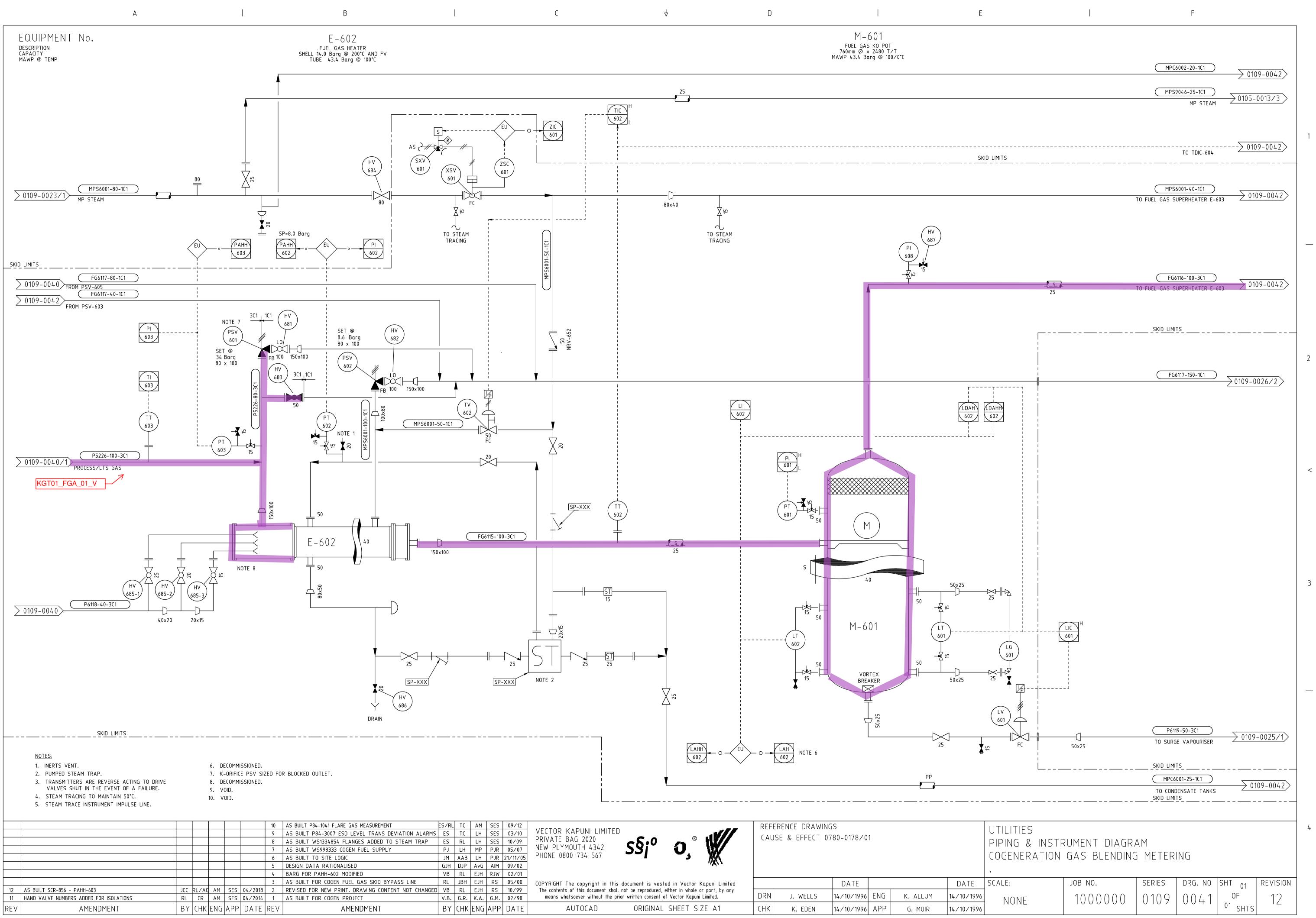
G - 319 - 2 METHANOL METERING PUMP (200 TON) FLOW 0.041 m3 /Hr MAWP 75.8 BargG @ 30°C F



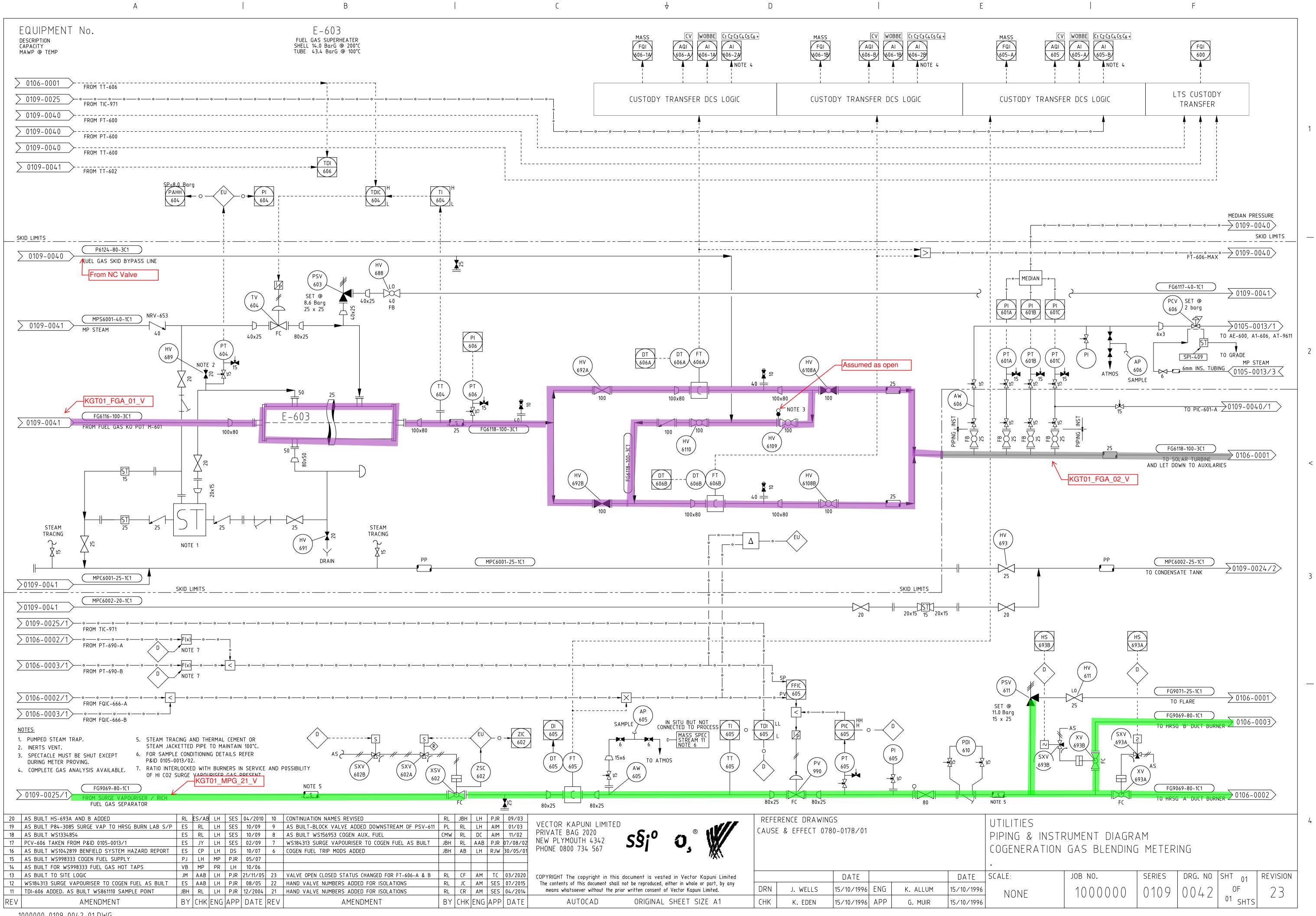


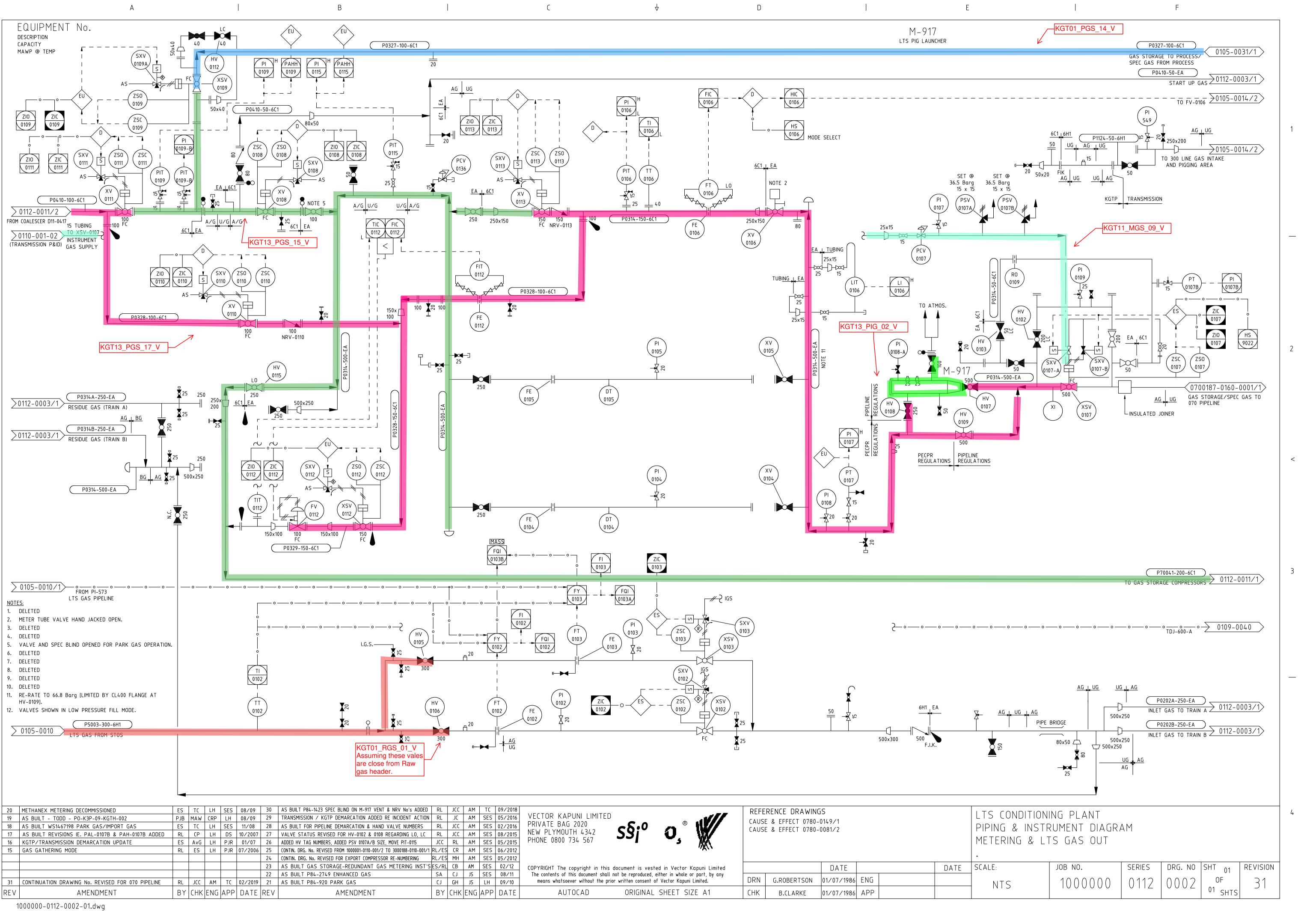


20	HAND VALVE NUMBERS ADDED FOR ISOLATIONS	RL	CF	AM	SES	10/20	13 10	WS	853855 AS	BUILT. (	ONDITIC	DNED LTS	S GAS I	NOW RAW	√ JBł	H AK	LH	H PJF	R 20/07/0	4						REFE	ERENCE DF		īS				<b> </b>   -
19	CONTIN. DRG. No. REVISED FOR EXPORT COMPRESSOR RE-NUMBERING	RL/E	S Mł	AM I	SES	05/20	12 9	PRO	OCESS ISOL	ATION PC	DINTS A	DDED ON	N INDIVI	IDUAL LA	YERS (M)	√ RL	CN	M AIM	1 11/02		KAPUNI LIN		-		® 11								
18	SPEC BLINDS AS BUILT AT HV-412-1&2 AND HV-413-1&2	RL	ES	LH	SES	07/20	09														BAG 2020	~	S§;°	-	®	0780	)-0178/01	CΑ	USE & EFF	-ECTS			ΡI
17	AS BUILT WS1191988 RAW GAS BYPASS TO CHILLERS	ES	AA	3 LH	SES	12/0	7														MOUTH 4342	2	221	U									
16	AS BUILT WS1191988 RAW GAS LTS BYPASS TO CHILLERS	KN	LH	MP	PJR	10/0	7 26	CON	NTINUATION	FROM P	&ID SPL	ITTING C	0105-00	14	JC	RL	A١	M SES	5 06/2016	, PHONE 08	800 734 567	/		-	5 MK								
15	AS BUILT WS998333 COGEN FUEL SUPPLY	PJ	LH	MP	PJR	05/0	7 25	AS	BUILT P84-8	J71 DEMOL	ITION OF	KGTP EQ	QUIP & N	NRV No's A	ADDED RL	JC/N	A AN	M SES	5 04/2016	5					77.								
14	AS BUILT FOR BUTANE FUEL DELETION	VB	SS	AAE	S LH	09/0	6 24	AS	BUILT P84	-871 BU7	ANE IN	JECTION	PUMP [	DEMO PRO	טו. וכנ	: RL/C	B AN	M SES	5   11/2015														۰
13	AS BUILT COMMENTS INCORPORATED	VB	RL	LH	PJR	06/0	6 23	AS	BUILT LO	VALVE 8	, EQUIPI	MENT IS	OLATION	NS	RL	NM/N	A AN	M SES	5 08/2015		The copyright	in this de	ocument is ves	sted in Ve	ector Kapuni Limited				DATE			DATE	SC
12	AS BUILT TO SITE LOGIC	JM	AA	3 LH	PJR	21/11/	05 22	I HAI	ND VALVE	NUMBER	ADDED	FOR ISO	DLATION	S	RL	JC	AN	M SES	5 07/2015	The content	ts of this documer	ent shall no	t be reproduced	, either in <sup>.</sup>	whole or part, by any								-
11	AS BUILT WS853855 MAUI LTS BLENDING TO BALLANCE	VB	RH		_				VISED FOR						RL	JCC			5 01/2015		hatsoever without					DRN	J. WEI	LLS	11/10/1996	ENG	K. ALLUM		
REV	V AMENDMENT	BY	′СН	K ENC	i apf	DAT	e rev	/		/	AMENE	DMENT			B`	r Chr	EN	IG API	P DATE		AUTOCAD		ORIGINAI	L SHEE	T SIZE A1	СНК	K.ED	JEN		APP	G.MUIR		
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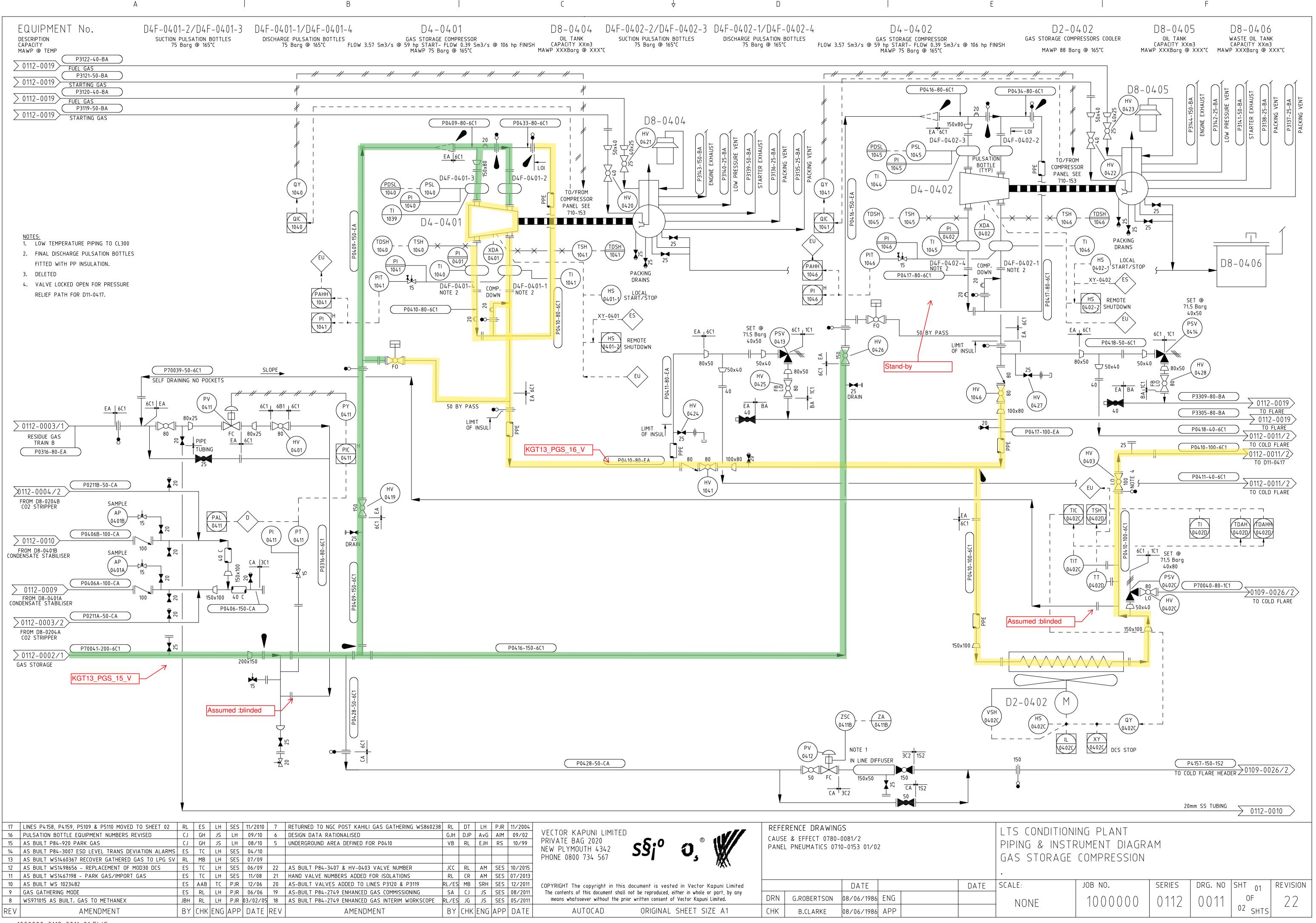






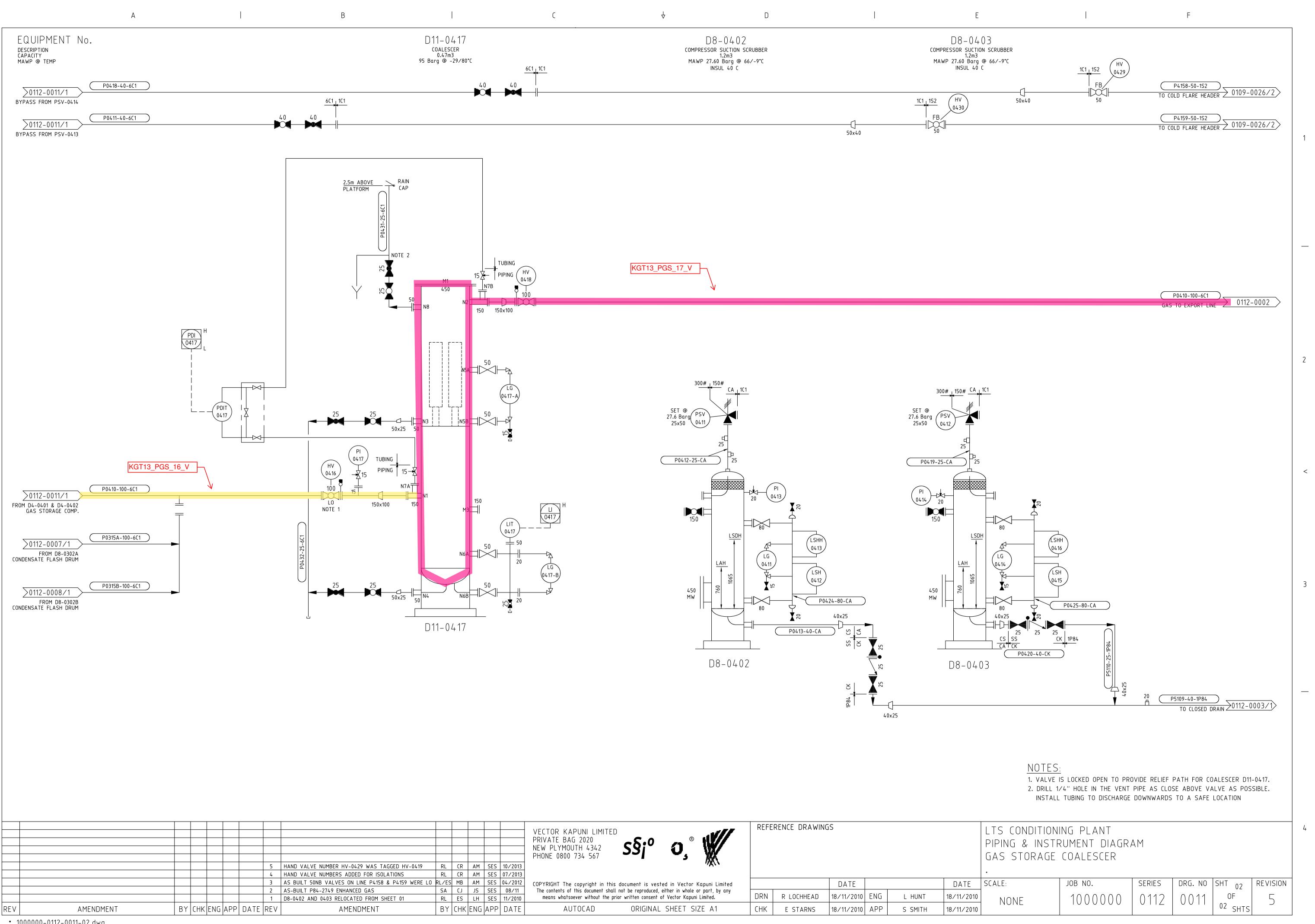


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-	AM	SES	02/2016	PRIVATE BAG 2020 NEW PLYMOUTH 4342 DHONE ARAD 734 F(7) SSi <sup>o</sup> O. <sup>®</sup>		E & EFFECT 0780-				P
-	AM	SES	08/2015	NEW PLYMOUTH 4342 SSi O W			0001/2			
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	JS	LH	09/10	means whatsoever without the prior written consent of Vector Kapuni Limited.	DRN	G.ROBERTSON	01/07/1986	ENG		
K	ENG	APP	DATE	AUTOCAD ORIGINAL SHEET SIZE A1	СНК	B.CLARKE	01/07/1986	APP		



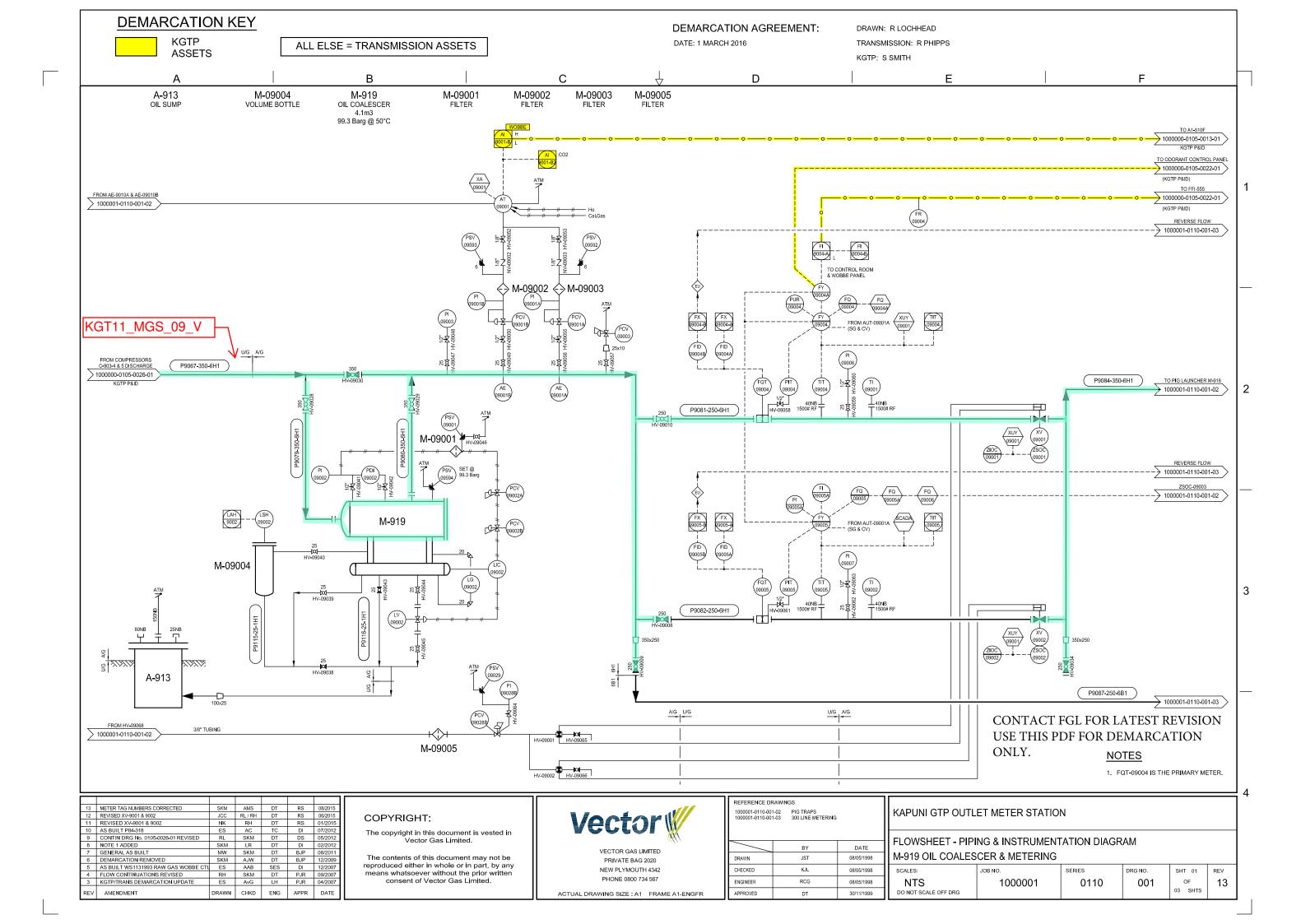
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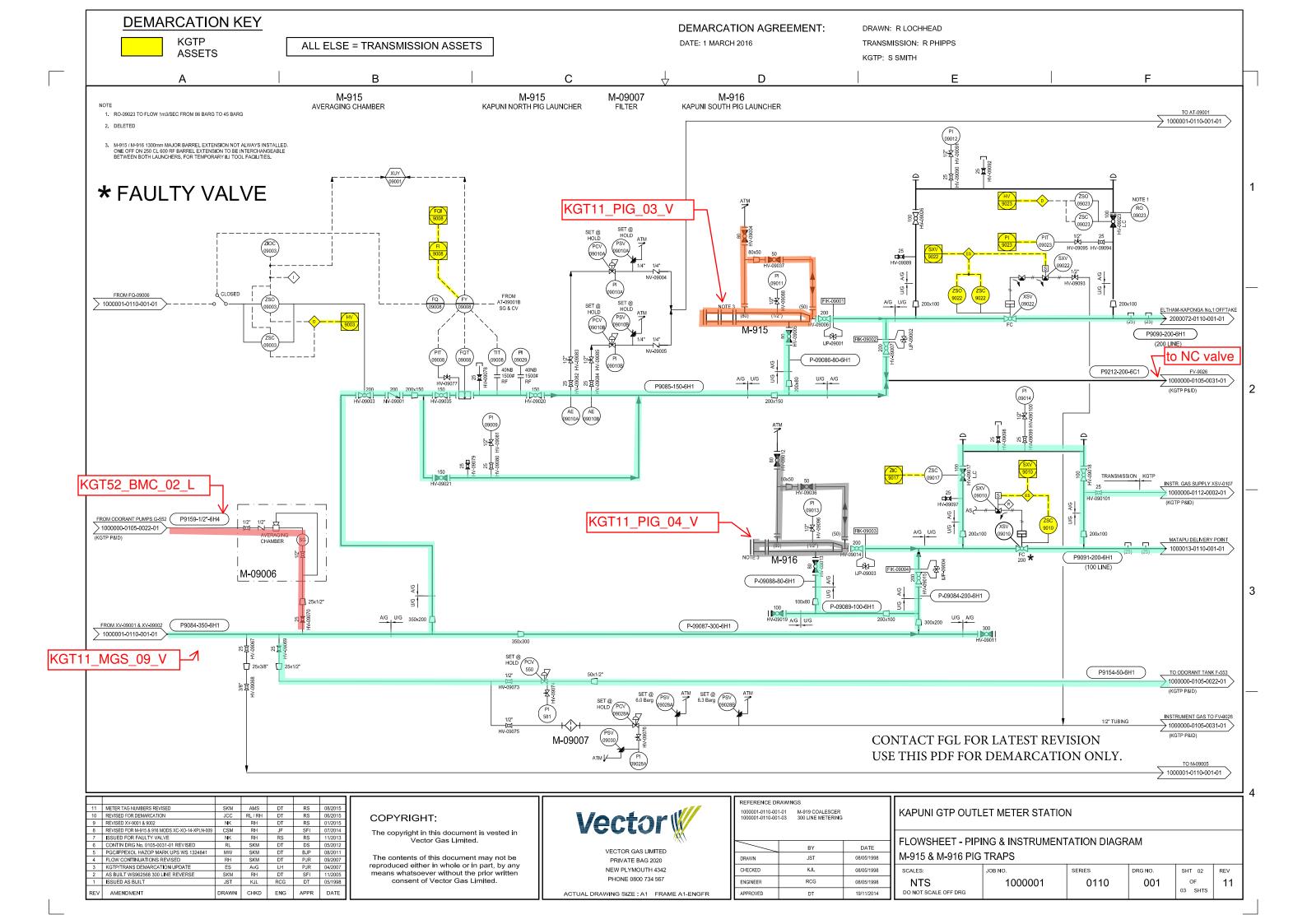
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<	ENG	APP	DATE	AUTOCAD ORIGINAL SHEET SIZE A1	СНК	E STARNS	18/11/2010	APP	S SMITH	18/11/2010	









Appendix 2. Parts Count Sheets

## Raw Gas and Maui Gas Lines

Equipment	Size	KGT01_RGS_01_V	KGT01_RCS_01_L	KGT01_MAU_01_V	KGT01_MAU_02_V
Process Pipe	0-2"	0	0	0	0
	3"-6"	0	0	0	63
	7"-12"	0	0	0	0
	13"-18"	0	0	0	0
	19"-24"	0	0	0	0
	25"-36"	0	0	0	0
Process Pipe (Inter-unit)	0-2"	0	0	0	0
	3"-6"	0	218	0	0
	7"-12"	0	0	0	0
	13"-18"	0	0	0	0
	19"-24"	259	0	111	0
	25"-36"	0	0	0	0
Flange	0-2"	13	16	8	8
5	3"-6"	29	2	25	24
	7"-12"	41	0	22	0
	13"-18"	10	0	0	0
	19"-24"	2	0	1	0
	25"-36"	0	0	0	0
Manual Valves	0-2"	34	21	23	3
	3"-6"	10	1	9	9
	7"-12"	14	0	8	0
	13"-18"	3	0	0	0
	19"-24"	0	0	2	0
	25"-36"	0	0	0	0
Actuated Valves	0-2"	5	2	1	1
Actualed valves	3"-6"	2	0	4	0
	3 -0 7"-12"	0	0	0	0
	13"-12	0	0	0	0
	19"-24"	0	0	1	0
	25"-36"	0	0	0	0
Small Bore Fittings	25 - 30	19	2	18	10
Process Vessel	<= 6"	1	0.5	0	0
Process vesser	<= 0 > 6 "			0	0
Questify and Dumm		0.5	0	0	0
Centrifugal Pump	<= 6" > 6 "	0	0	0	0
Reciprocating Pump	<= 6"	0	0	0	0
Reciprocating Pump	<= 6 > 6 "	0	0	0	0
Centrifugal Compressor	<= 6"	0	0	0	0
Centinugai Compressoi	> 6 "	0	0	0	0
Reciprocating Compressor	<= 6"	0	0	0	0
Recipiocating Compressor	> 6 "	0	0	0	0
Shell Side Heat Exchanger	<= 6"	0	0	0	0
Shell Side Heat Exchanger	> 6 "	0	0	0	0
Tubo Sido Host Evelop	<= 6"		0	0	
Tube Side Heat Exchanger	<= 6" > 6 "	0		0	0
Plate Heat Evaluation	> 6 " <= 6"	0	0	0	0
Plate Heat Exchanger					
Air Ceeled Heat Fushar	> 6 "	0	0	0	0
Air Cooled Heat Exchanger	<= 6"	0	0	0	0
<b>F</b> 10	> 6 "	0	0	0	0
Filters	<= 6"	0	0	0	1
D' T	> 6 "	0	0	0	0
Pig Trap	<= 6"	0	0	0	0
	> 6 "	0	0	0	0

## CO2 Removal

Equipment	Size	KGT02_TGS_01_V	KGT03_TGS_04_V	KGT05_RGS_07_V	KGT05_TGS_16_V
Process Pipe	0-2"	0	0	0	0
	3"-6"	0	0	0	0
	7"-12"	15	15	15	15
	13"-18"	0	0	0	0
	19"-24"	0	0	0	0
	25"-36"	0	0	0	0
Process Pipe (Inter-unit)	0-2"	0	0	0	0
	3"-6"	0	0	0	0
	7"-12"	0	0	0	0
	13"-18"	0	0	0	0
	19"-24"	0	0	0	0
	25"-36"	0	0	0	0
lange	0-2"	9	9	2	19
	3"-6"	15	18	8	19
	7"-12"	4	4	17	12
	13"-18"	0	0	0	0
	19"-24"	0	0	0	0
	25"-36"	0	0	0	0
Manual Valves	0-2"	5	5	5	10
	3"-6"	1	3	0	3
	7"-12"	0	0	4	0
	13"-18"	0	0	0	0
	19"-24"	0	0	0	0
	25"-36"	0	0	0	0
Actuated Valves	0-2"	2	2	0	2
Actualed valves	3"-6"	3	3	2	2
	3-0 7"-12"	0	0	0	0
	13"-12	0	0	0	0
	13"-18" 19"-24"		0	0	
		0	0	0	0
Den all Danas Eittin an	25"-36"	12		7	
Small Bore Fittings	2"		11		19
Process Vessel	<= 6"	0.5	0	0	0
	> 6 "	0.5	1	0	
Centrifugal Pump	<= 6" > 6 "	0	0	0	0
De siene setie e Denne	<= 6"	0	0	0	0
Reciprocating Pump	<= 6 "	0	0	0	0
Centrifugal Compressor	<= 6" > 6 "	0	0	0	0
Reciprocating Compressor	<= 6"	0	0	0	0
	> 6 "	0	0	0	0
Shell Side Heat Exchanger	<= 6"	0	0	0	0
	> 6 "	0	0	1	0
Tube Side Heat Exchanger	<= 6"	1	1	0	0
	> 6 "	0	0	0	1
Plate Heat Exchanger	<= 6"	0	0	0	0
	> 6 "	0	0	0	0
Air Cooled Heat Exchanger	<= 6"	0	0	0	0
	> 6 "	0	0	0	0
Filters	<= 6"	0	0	0	0
	> 6 "	0	0	0	0
Pig Trap	<= 6"	0	0	0	0
	> 6 "	0	0	0	0

## Dehydration and Dewpoint Control

Equipment	Size	KGT01_TGS_07_V	KGT01_TGS_10_V	KGT01_TGS_12_V	KGT01_PGS_02_V	KGT04_PGS_07_V	KGT01_MPG_01_L	KGT04_MPG_03_L
Process Pipe	0-2"	0	0	0	0	0	0	0
	3"-6"	0	0	0	0	15	15	35
	7"-12"	48	48	49	15	0	0	0
	13"-18"	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0
Process Pipe (Inter-unit)	0-2"	0	0	0	0	0	0	0
	3"-6"	0	0	0	0	0	0	0
	7"-12"	0	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0
Flange	0-2"	17	4	1	3	2	6	12
	3"-6"	28	2	20	10	9	5	12
	7"-12"	29	13	8	6	0	0	0
	13"-18"	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0
Manual Valves	0-2"	17	3	5	1	1	3	8
	3"-6"	9	1	8	0	2	0	4
	7"-12"	7	3	0	0	0	0	0
	13"-18"	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0
Actuated Valves	0-2"	2	0	0	0	1	1	0
/ lotation Farros	3"-6"	2	0	1	3	1	0	0
	7"-12"	0	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0
Small Bore Fittings	2"	20	12	7	8	5	5	1
Process Vessel	<= 6"	0.5	0	0	0.5	0.5	1	0
	> 6 "	0.5	0	0	0.5	0	0	0
Centrifugal Pump	<= 6"	0.0	0	0	0	0	0	0
<u>oonunagarranp</u>	> 6 "	0	0	0	0	0	0	0
Reciprocating Pump	<= 6"	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0
Centrifugal Compressor	<= 6"	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0
Reciprocating Compressor	<= 6"	0	0	0	0	0	0	0
····· · · · · · · · · · · · · · · · ·	> 6 "	0	0	0	0	0	0	0
Shell Side Heat Exchanger	<= 6"	0	0	0	0	0	0	1
	> 6 "	0	0	0	2	0	0	0
Tube Side Heat Exchanger	<= 6"	0	0	0	0	0	0	0
- Side Float Excitaliger	> 6 "	0	3	1	0	0	0	0
Plate Heat Exchanger	<= 6"	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0
Air Cooled Heat Exchanger	<= 6"	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0
Filters	<= 6"	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0
Pig Trap	<= 6"	0	0	0	0	0	0	0
· · · · · · · · · · · · · · · · · · ·		0	, v	v	U U	U U		

Equipment	Size	KGT04_MPG_04_L	KGT04_MPG_05_L	KGT04_MPG_06_L	KGT01_TGS_11_V	KGT01_PGS_03_V	KGT01_MPG_02_L
Process Pipe	0-2"	0	0	0	0	0	v
	3"-6"	15	15	15	0	15	15
	7"-12"	0	0	0	43	0	0
	13"-18"	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	v
Process Pipe (Inter-unit)	0-2"	0	0	0	0	0	0
	3"-6"	0	0	0	0	0	0
	7"-12"	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0
Flange	0-2"	2	9	10	0	5	6
	3"-6"	7	7	14	13	7	2
	7"-12"	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0
Manual Values		2	2	7	1	2	3
Manual Valves	0-2"			2	2		
	3"-6"	2	3			0	0
	7"-12"	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0
Actuated Valves	0-2"	0	0	3	0	2	1
	3"-6"	0	0	1	0	1	0
	7"-12"	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0
Small Bore Fittings	2"	2	1	9	7	11	4
Process Vessel	<= 6"	0.5	0	1	0	0.5	0.5
	> 6 "	0	0	0	0	0	0
Centrifugal Pump	<= 6"	0	1	0	0	0	0
	> 6 "	0	0	0	0	0	0
Reciprocating Pump	<= 6"	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0
Centrifugal Compressor	<= 6"	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0
Reciprocating Compressor	<= 6"	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0
Shell Side Heat Exchanger	<= 6"	0	0	0	0	2	0
	> 6 "	0	0	0	0	0	0
Tube Side Heat Exchanger	<= 6"	0	0	0	3	0	0
	> 6 "	0	0	0	0	0	0
Plate Heat Exchanger	<= 6"	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0
Air Cooled Heat Exchanger	<= 6"	0	0	0	0	0	0
All Source Heat Exchanger	> 6 "	0	0	0	0	0	0
Filters	<= 6"	1	0	0	0	0	0
FILLEIS		0			0		
Dia Tran	> 6 "		0	0		0	0
Pig Trap	<= 6"	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0

## Product Gas Lines and Compressors

Equipment	Size	KGT01_PGS_01_V	KGT01_PGS_13_V	KGT01_PGS_14_V	KGT13_PGS_15_V	KGT13_PGS_16_V	KGT13_PGS_17_V	KGT01_MGS_01_V
Process Pipe	0-2"	0	0	0	0	0	0	0
	3"-6"	0	15	0	0	51	0	0
	7"-12"	0	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0	91
	19"-24"	0	0	0	56	0	51	0
	25"-36"	0	0	0	0	0	0	0
Process Pipe (Inter-unit)	0-2"	0	0	0	0	0	0	0
	3"-6"	0	0	0	0	0	0	0
	7"-12"	0	0	274	0	0	0	0
	13"-18"	229	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0
Flange	0-2"	24	20	3	4	6	0	45
	3"-6"	28	1	3	32	28	25	11
	7"-12"	46	0	7	4	0	20	31
	13"-18"	0	0	0	0	0	0	6
	19"-24"	0	0	0	0	0	1	0
	25"-36"	0	0	0	0	0	0	0
Manual Valves	0-2"	34	10	1	10	3	6	34
	0-2 3"-6"	12	0	1	5	5	3	2
				2	3		4	
	7"-12"	13	0			0		5
	13"-18"	0	0	0	0	0	0	2
	19"-24"	0	0	0	0	0	2	0
	25"-36"	0	0	0	0	0	0	0
Actuated Valves	0-2"	3	4	0	0	2	0	16
	3"-6"	2	0	1	1	1	5	2
	7"-12"	0	0	0	0	0	1	3
	13"-18"	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	1	0
	25"-36"	0	0	0	0	0	0	0
Small Bore Fittings	2"	26	6	2	6	10	17	33
Process Vessel	<= 6"	0	0.5	0	2	2	1	1
	> 6 "	0	0	0	0	0	0	3
Centrifugal Pump	<= 6"	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0
Reciprocating Pump	<= 6"	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0
Centrifugal Compressor	<= 6"	0	0	0	0	1	0	0
	> 6 "	0	0	0	0	0	0	0
Reciprocating Compressor	<= 6"	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0
Shell Side Heat Exchanger	<= 6"	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0
Tube Side Heat Exchanger	<= 6"	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0
Plate Heat Exchanger	<= 6"	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0
Air Cooled Heat Exchanger	<= 6"	0	0	0	0	1	0	0
	> 6 "	0	0	0	0	0	0	0
Filters	<= 6"	0	0	0	1	0	0	1
	> 6 "	0	0	0	0	0	0	2
Pig Trap	<= 6"	0	0	0	0	0	0	0
гупар				0				
	> 6 "	0	0	U	0	0	0	0

Equipment	Size	KGT01_MGS_03_V	KGT01_MGS_07_V	KGT11_MGS_05_V	KGT11_MGS_08_V	KGT11_MGS_09_V
Process Pipe	0-2"	0	0	0	0	0
	3"-6"	0	0	0	0	0
	7"-12"	15	15	0	0	0
	13"-18"	0	0	91	0	0
	19"-24"	0	0	0	0	0
	25"-36"	0	0	0	0	0
Process Pipe (Inter-unit)	0-2"	0	0	0	251	0
	3"-6"	0	0	0	0	0
	7"-12"	0	0	0	0	0
	13"-18"	0	0	0	0	278
	19"-24"	0	0	0	0	0
	25"-36"	0	0	0	0	0
Flange	0-2"	0	0	1	37	2
	3"-6"	12	13	8	0	26
	7"-12"	4	3	8	0	23
	13"-18"	0	0	6	0	8
	19"-24"	0	0	0	0	0
	25"-36"	0	0	0	0	0
Manual Valves	0-2"	0	2	12	24	29
	3"-6"	0	1	1	0	10
	7"-12"	1	1	4	0	11
	13"-18"	0	0	2	0	3
	19"-24"	0	0	0	0	0
	25"-36"	0	0	0	0	0
Actuated Valves	0-2"	0	0	0	9	13
	3"-6"	3	3	2	0	1
	7"-12"	1	1	0	0	4
	13"-18"	0	0	0	0	0
	19"-24"	0	0	0	0	0
	25"-36"	0	0	0	0	0
Small Bore Fittings	20 00	13	4	5	5	31
Process Vessel	<= 6"	1	0	0	0	0
1100033 703301	> 6 "	1	0	0	0	1
Centrifugal Pump	<= 6"	0	0	0	0	0
ochundgarr ump	> 6 "	0	0	0	0	0
Reciprocating Pump	<= 6"	0	0	0	0	0
recipiocating rump	> 6 "	0	0	0	0	0
Centrifugal Compressor	<= 6"	1	1	0	0	0
ochinidgai oompressor	> 6 "	0	0	0	0	0
Reciprocating Compressor	<= 6"	0	0	0	0	0
Recipiocating Compressor	> 6 "	0	0	0	0	0
Shell Side Heat Exchanger	<= 6"	0	0	0	0	0
onon olue neat Exchanger	<= 6 "	0	0	0	0	0
Tube Side Heat Exchanger	<= 6"	0	0	0	0	0
rube olde meat Exchanger	<= 6" > 6 "	0	0	0	0	0
Plate Heat Exchanger	<= 6"	0	0	0	0	0
riale meat Excitatiget	<= 6" > 6 "	0	0	0	0	0
Air Cooled Heat Evolution	<= 6"	0	1	0	0	0
Air Cooled Heat Exchanger	<= 6" > 6 "	1	0	0	0	0
Filtere						
Filters	<= 6"	0	0	0	0	0
	> 6 " <= 6"	0	0	0	0	0
Pig Trap						

# Pigging

Equipment	Size	KGT01_PIG_01_V	KGT13_PIG_02_V	KGT11_PIG_03_V	KGT11_PIG_04_V
Process Pipe	0-2"	0	0	0	0
	3"-6"	0	0	0	0
	7"-12"	0	0	0	0
	13"-18"	0	0	0	0
	19"-24"	0	0	0	0
	25"-36"	0	0	0	0
Process Pipe (Inter-unit)	0-2"	0	0	0	0
	3"-6"	0	0	0	0
	7"-12"	0	0	0	0
	13"-18"	0	0	0	0
	19"-24"	0	0	0	0
	25"-36"	0	0	0	0
Flange	0-2"	2	1	3	3
	3"-6"	2	1	3	3
	7"-12"	1	1	1	1
	13"-18"	0	0	0	0
	19"-24"	0	0	0	0
	25"-36"	0	0	0	0
Manual Valves	0-2"	3	3	1	1
	3"-6"	1	1	1	1
	7"-12"	0	0	0	0
	13"-18"	0	0	0	0
	19"-24"	0	0	0	0
	25"-36"	0	0	0	0
Actuated Valves	0-2"	0	0	0	0
	3"-6"	0	0	0	0
	7"-12"	0	0	0	0
	13"-18"	0	0	0	0
	19"-24"	0	0	0	0
	25"-36"	0	0	0	0
Small Bore Fittings	20 00	2	1	1	1
Process Vessel	<= 6"	0	0	0	0
100033 103301	> 6 "	0	0	0	0
Centrifugal Pump	<= 6"	0	0	0	0
	> 6 "	0	0	0	0
Reciprocating Pump	<= 6"	0	0	0	0
tooproodding r dinp	> 6 "	0	0	0	0
Centrifugal Compressor	<= 6"	0	0	0	0
Johanagai Gompressor	> 6 "	0	0	0	0
Reciprocating Compressor	<= 6"	0	0	0	0
tooiprobating bomproboor	> 6 "	0	0	0	0
Shell Side Heat Exchanger	<= 6"	0	0	0	0
ender noar Exonanger	> 6 "	0	0	0	0
Tube Side Heat Exchanger	<= 6"	0	0	0	0
and the reat Exchanger	> 6 "	0	0	0	0
Plate Heat Exchanger	<= 6"	0	0	0	0
ato nout Exonangoi	> 6 "	0	0	0	0
Air Cooled Heat Exchanger	<= 6"	0	0	0	0
an ooolou noar Exchanger	> 6 "	0	0	0	0
Filters	<= 6"	0	0	0	0
11013	> 6 "	0	0	0	0
Pig Trap	<= 6"	0	0	0	0
iy i ap	~-0	0	0	0	0

## Utilities and Cogen Unit

Equipment	Size	KGT01_MPG_21_V	KGT01_MPG_22_L	KGT01_MPG_23_L	KGT01_FGA_01_V	KGT01_FGA_02_V	KGT01_PGS_19_V	KGT01_PGS_21_V	KGT01_PGS_22_V
Process Pipe	0-2"	0	15	50	0	0	0	0	0
	3"-6"	78	0	0	38	0	0	0	50
	7"-12"	0	0	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0	0
Process Pipe (Inter-unit)	0-2"	0	0	0	0	0	154	0	0
	3"-6"	0	0	0	0	138	0	274	0
	7"-12"	0	0	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0	0
Flange	0-2"	12	8	13	21	27	25	36	27
	3"-6"	33	0	0	51	89	2	1	41
	7"-12"	0	0	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0	0
Manual Valves	0-2"	7	2	5	9	35	15	17	17
	3"-6"	8	0	0	16	23	1	1	7
	7"-12"	0	0	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0	0
Actuated Valves	0-2"	4	0	1	2	19	9	5	9
	3"-6"	4	0	0	3	15	0	0	10
	7"-12"	0	0	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0	0
Small Bore Fittings	2"	13	0	1	20	56	7	9	13
Process Vessel	<= 6"	1.5	0.5	0.25	1	1	0	0	0
	> 6 "	0	0	0	0	0	0	0	0
Centrifugal Pump	<= 6"	0	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0	0
Reciprocating Pump	<= 6"	0	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0	0
Centrifugal Compressor	<= 6"	0	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0	0
Reciprocating Compressor	<= 6"	0	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0	0
Shell Side Heat Exchanger	<= 6"	0	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0	0
Tube Side Heat Exchanger	<= 6"	0	0	0	2	0	0	0	0
, in the second se	> 6 "	0	0	0	0	0	0	0	0
Plate Heat Exchanger	<= 6"	0	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0	0
Air Cooled Heat Exchanger	<= 6"	0	0	0	0	0	0	0	0
J J	> 6 "	0	0	0	0	0	0	0	0
Filters	<= 6"	1	1	0	0	2	4	8	0
	> 6 "	0	0	0	0	0	0	0	0
Pig Trap	<= 6"	0	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0	0

## LPG Production Facility - Stabiliser, De-C2

Equipment	Size	KGT01_MPG_07_L	KGT01_DET_01_V	KGT01_PGS_04_V	KGT01_PGS_05_V	KGT01_DEX_01_L	KGT01_DEB_01_L	KGT01_MPG_09_L
Process Pipe	0-2"	0	0	0	0	0	0	0
	3"-6"	0	15	0	0	15	15	22
	7"-12"	0	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0
Process Pipe (Inter-unit)	0-2"	0	0	0	0	0	0	0
	3"-6"	194	0	110	0	0	0	0
	7"-12"	0	0	0	143	0	0	0
	13"-18"	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0
Flange	0-2"	3	3	8	22	30	5	9
5	3"-6"	18	19	5	15	1	18	36
	7"-12"	0	0	0	7	0	0	0
	13"-18"	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0
Manual Valves	0-2"	7	6	6	9	19	9	14
	3"-6"	8	4	2	5	0	6	14
	7"-12"	0	0	0	2	0	0	0
				-				
	13"-18"	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0
Actuated Valves	0-2"	2	3	1	3	1	1	0
	3"-6"	0	1	0	1	0	0	2
	7"-12"	0	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0
Small Bore Fittings	2"	5	7	7	10	5	10	11
Process Vessel	<= 6"	0	1	2	1	0.5	0.5	0.5
	> 6 "	0	0	0	0	0	0	0
Centrifugal Pump	<= 6"	0	0	0	0	1	0	0
	> 6 "	0	0	0	0	0	0	0
Reciprocating Pump	<= 6"	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0
Centrifugal Compressor	<= 6"	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0
Reciprocating Compressor	<= 6"	0	0	0	1	0	0	0
	> 6 "	0	0	0	0	0	0	0
Shell Side Heat Exchanger	<= 6"	0	0	0	0	0	1	0
	> 6 "	0	0	0	0	0	0	0
Tube Side Heat Exchanger	<= 6"	1	1	0	0	0	0	0
5	> 6 "	0	0	0	0	0	0	0
Plate Heat Exchanger	<= 6"	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0
Air Cooled Heat Exchanger	<= 6"	0	0	0	1	0	0	0
	> 6 "	0	0	0	0	0	0	0
Filters	<= 6"	0	0	0	0	1	0	0
	> 6 "	0	0	0	0	0	0	0
Pig Tran	<= 6"	0	0	0	0	0	0	0
Pig Trap								
	> 6 "	0	0	0	0	0	0	0

Equipment	Size	KGT01_MPG_10_V	KGT01_MPG_13_L	KGT01_STT_01_V	KGT01_PGS_10_V	KGT01_PGS_11_V	KGT01_STB_01_L
Process Pipe	0-2"	0	0	0	0	0	0
	3"-6"	15	0	15	90	15	15
	7"-12"	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0
Process Pipe (Inter-unit)	0-2"	0	0	0	0	0	0
/	3"-6"	0	144	0	0	0	0
	7"-12"	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0
Flange	0-2"	22	6	4	9	13	18
i lango	3"-6"	1	10	16	17	21	4
	7"-12"	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0
				0		0	
	25"-36"	0	0		0		0
Manual Valves	0-2"	11	4	3	6	8	9
	3"-6"	0	2	2	7	8	0
	7"-12"	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0
Actuated Valves	0-2"	2	2	2	1	2	1
	3"-6"	0	0	1	0	0	0
	7"-12"	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0
Small Bore Fittings	2"	4	2	19	12	3	20
Process Vessel	<= 6"	0.5	0	1.5	2	1	0.5
	> 6 "	0	0	0	0	0	0
Centrifugal Pump	<= 6"	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0
Reciprocating Pump	<= 6"	0	0	0	0	0	0
ricoiprobating r amp	> 6 "	0	0	0	0	0	0
Centrifugal Compressor	<= 6"	0	0	0	0	0	0
Contantagui Compressor	> 6 "	0	0	0	0	0	0
Reciprocating Compressor	<= 6"	0	0	0	0	1	0
rtooiprocaung Compressor	> 6 "	0	0	0	0	0	0
Shell Side Heat Exchanger	<= 6"	0	0	0	0	0	1
Shell Side Heat Exchanger	<= 6 > 6 "	0	0	0	0	0	0
Tube Side Lleet Evebourge				0	0	0	
Tube Side Heat Exchanger	<= 6" > 6 "	0	0				0
Dista Lie at Evaluar na		0	0	0	0	0	0
Plate Heat Exchanger	<= 6"	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0
Air Cooled Heat Exchanger	<= 6"	0	0	0	0	1	0
	> 6 "	0	0	0	0	0	0
Filters	<= 6"	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0
Pig Trap	<= 6"	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0

## LPG Production Facility - De-C3

Equipment	Size	KGT01_DPT_11_V	KGT01_DPX_11_L	KGT01_PC3_02_L	KGT01_DPB_11_L	KGT01_DPT_01_V	KGT01_DPX_01_L	KGT01_PC3_01_L	KGT01_DPB_01_L
Process Pipe	0-2"	0	0	15	0	0	0	22	0
	3"-6"	15	15	0	56	15	15	0	44
	7"-12"	0	0	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0	0
Process Pipe (Inter-unit)	0-2"	0	0	0	0	0	0	0	0
	3"-6"	0	0	0	0	0	0	0	0
	7"-12"	0	0	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0	0
Flange	0-2"	11	16	30	44	15	22	25	36
	3"-6"	12	21	1	11	11	11	0	4
	7"-12"	0	0	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0	0
Manual Valves	0-2"	6	10	17	29	8	10	13	21
	3"-6"	0	7	0	4	0	5	0	0
	7"-12"	0	0	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0	0
Actuated Valves	0-2"	2	1	3	2	2	1	2	2
Actualed valves	3"-6"	3	0	1	0	3	0	0	0
	7"-12"	0	0	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0	0
Small Bore Fittings	25 - 36	8	8	8	12	26	10	5	16
Process Vessel	<= 6"	0	0.5	0	0.5	1	0.5	0	0.5
FIDCESS VESSEI	> 6 "	0	0.5	0	0.5	0	0.5	0	0.5
Centrifugal Pump	<= 6"		1	0	0		1		0
Centrilugal Pump	> 6 "	0	0	0	0	0	0	0	0
De sinne estin a Dema					0				
Reciprocating Pump	<= 6" > 6 "	0	0	0	0	0	0	0	0
Contrifuent Commences	<= 6"	0	0	0	0	0	0	0	0
Centrifugal Compressor									
Pooipropoting Compression	> 6 " <= 6"	0	0	0	0	0	0	0	0
Reciprocating Compressor	<= 6 "	0	0	0	0	0	0		0
Chall Cide Llast Euclide	-							0	
Shell Side Heat Exchanger	<= 6"	0	0	1	1	0	0	1	1
Tuba Oida Usat Fush	> 6 "	0	0	0	0	0	0	0	0
Tube Side Heat Exchanger	<= 6"	0	0	0	0	0	0	0	0
Dista Lis et Evels en nor	> 6 "	0	0	0	0	0	0	0	0
Plate Heat Exchanger	<= 6"	0	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0	0
Air Cooled Heat Exchanger	<= 6"	1	0	0	0	1	0	0	0
	> 6 "	0	0	0	0	0	0	0	0
Filters	<= 6"	0	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0	0
Pig Trap	<= 6"	0	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0	0

## LPG Production Facility - De-C4

Equipment	Size	KGT01_DBT_11_V	KGT01_DBX_11_L	KGT01_NGL_01_L	KGT01_NGL_02_L	KGT01_DBT_01_V	KGT01_DBX_01_L	KGT01_DBB_01_L
Process Pipe	0-2"	0	0	0	0	0	0	0
	3"-6"	0	15	42	23	15	15	15
	7"-12"	0	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0
Process Pipe (Inter-unit)	0-2"	0	0	0	0	0	0	0
	3"-6"	168	0	0	0	0	0	0
	7"-12"	0	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0
Flange	0-2"	31	49	33	32	21	30	12
- intering o	3"-6"	18	6	4	1	6	6	4
	7"-12"	0	0	0	0	0	0	0
	13"-12	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0
Manual Valves	0-2"	26	28	18	15	10	18	7
	3"-6"	3	2	0	0	0	2	0
	7"-12"	0	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0
Actuated Valves	0-2"	2	4	2	5	2	2	1
3"-6 7"-12	3"-6"	3	0	0	0	2	0	0
	7"-12"	0	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0
Small Bore Fittings	2"	8	15	16	14	15	12	9
Process Vessel	<= 6"	1	0.5	0.5	0	1	0.5	0.5
	> 6 "	0	0	0	0	0	0	0
Centrifugal Pump	<= 6"	0	1	0	0	0	1	0
	> 6 "	0	0	0	0	0	0	0
Reciprocating Pump	<= 6"	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0
Centrifugal Compressor	<= 6"	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0
Reciprocating Compressor	<= 6"	0	0	0	0	0	0	0
Compressor	> 6 "	0	0	0	0	0	0	0
Shall Sida Haat Evaborer	<= 6"	0	0	1	1	0	0	1
Shell Side Heat Exchanger	<= 6" > 6 "	0	0	0	0	0	0	0
Tube Olds Use 1 Tube								-
Tube Side Heat Exchanger	<= 6"	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0
Plate Heat Exchanger	<= 6"	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0
Air Cooled Heat Exchanger	<= 6"	1	0	0	1	1	0	0
	> 6 "	0	0	0	0	0	0	0
Filters	<= 6"	0	1	0	1	0	0	0
	> 6 "	0	0	0	0	0	0	0
Pig Trap	<= 6"	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0

Equipment	Size	KGT01_PC4_12_L	KGT01_PC3_13_L	KGT01_LPG_04_L
Process Pipe	0-2"	0	15	0
	3"-6"	41	0	0
	7"-12"	0	0	0
	13"-18"	0	0	0
	19"-24"	0	0	0
	25"-36"	0	0	0
Process Pipe (Inter-unit)	0-2"	0	0	232
	3"-6"	0	0	0
	7"-12"	0	0	0
	13"-18"	0	0	0
-	19"-24"	0	0	0
	25"-36"	0	0	0
Flange	0-2"	14	9	36
	3"-6"	0	0	0
	7"-12"	0	0	0
	13"-18"	0	0	0
	19"-24"	0	0	0
	25"-36"	0	0	0
Manual Valves	0-2"	13	10	23
	3"-6"	0	0	0
	7"-12"	0	0	0
	13"-12	0	0	0
	13 - 16	0	0	0
			-	
A	25"-36"	0	0	0
Actuated Valves	0-2"	6	5	6
	3"-6"	0	0	0
	7"-12"	0	0	0
	13"-18"	0	0	0
	19"-24"	0	0	0
	25"-36"	0	0	0
Small Bore Fittings	2"	5	3	11
Process Vessel	<= 6"	0	0	0
	> 6 "	0	0	0
Centrifugal Pump	<= 6"	0	0	0
	> 6 "	0	0	0
Reciprocating Pump	<= 6"	0	0	0
	> 6 "	0	0	0
Centrifugal Compressor	<= 6"	0	0	0
	> 6 "	0	0	0
Reciprocating Compressor	<= 6"	0	0	0
	> 6 "	0	0	0
Shell Side Heat Exchanger	<= 6"	0	0	0
	> 6 "	0	0	0
Tube Side Heat Exchanger	<= 6"	1	0	0
	> 6 "	0	0	0
Plate Heat Exchanger	<= 6"	0	0	0
	> 6 "	0	0	0
Air Cooled Heat Exchanger	<= 6"	0	0	0
	> 6 "	0	0	0
Filters	<= 6"	0	0	0
	> 6 "	0	0	0
Pig Trap	<= 6"	0	0	0
	> 6 "	0	0	0

#### LPG Production Facility - Product Export and Loadout

Equipment	Size	KGT32_NGL_05_L	KGT33_NGL_06_L	KGT34_NGL_07_L	KGT35_NGL_09_L	KGT36_NGL_10_L	KGT36_NGL_11_L	KGT37_PC3_05_L	KGT39_PC3_07_V
Process Pipe	0-2"	0	0	0	0	0	0	0	0
	3"-6"	0	0	0	15	15	0	0	0
	7"-12"	0	0	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0	0
Process Pipe (Inter-unit)	0-2"	210	0	0	0	0	0	0	0
	3"-6"	0	103	0	0	0	0	81	0
	7"-12"	0	0	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0	0
Flange	0-2"	4	9	0	3	0	0	1	0
Thungo	3"-6"	0	4	0	12	16	0	14	0
	7"-12"	0	0	0	0	0	0	0	0
	13"-12	0	0	0	0	0	0	0	0
		0	0	0	0	0	0	0	0
	19"-24"		0		0	0	0		
Manual Mahaa	25"-36" 0-2"	0		0	4	2	0	0	0
Manual Valves			10					4	
	3"-6"	0	2	0	2	3	0	3	0
	7"-12"	0	0	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0	0
Actuated Valves	0-2"	1	3	0	1	1	0	3	0
	3"-6"	0	0	0	2	1	0	3	0
	7"-12"	0	0	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0	0
Small Bore Fittings	2"	1	6	0	2	3	0	1	0
Process Vessel/ Storage Tank	<= 6"	0	0	1	0	1	0	0	0.5
<u></u>	> 6 "	0	0	0	0	0	0	0	0
Centrifugal Pump	<= 6"	0	0	0	1	0	0	0	0
	> 6 "	0	0	0	0	0	0	0	0
Reciprocating Pump	<= 6"	0	0	0	0	0	0	0	0
····	> 6 "	0	0	0	0	0	0	0	0
Centrifugal Compressor	<= 6"	0	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0	0
Reciprocating Compressor	<= 6"	0	0	0	0	0	0	0	0
Compression and Compression	> 6 "	0	0	0	0	0	0	0	0
Shell Side Heat Exchanger	<= 6"	0	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0	0
Tubo Sido Hoot Evolopgor	<= 6"	0	0	0	0	0	0	0	0
Tube Side Heat Exchanger	<= 0 > 6 "	0	0	0	0	0	0	0	0
Diate Heat Evenesses				0	0		0	0	0
Plate Heat Exchanger	<= 6"	0	0			0			
	> 6 "	0	0	0	0	0	0	0	0
Air Cooled Heat Exchanger	<= 6"	0	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0	0
Filters	<= 6"	0	0	0	1	0	0	0	0
	> 6 "	0	0	0	0	0	0	0	0
Pig Trap	<= 6"	0	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0	0
Loading Hose	-	0	0	0	0	0	1	0	0
Loading Arm	-	0	0	0	0	0	0	0	0

Equipment	Size	KGT39_PC3_08_L	KGT40_PC3_09_V	KGT40_PC3_10_L	KGT41_PC4_04_L	KGT43_PC4_06_V	KGT43_PC4_07_L	KGT44_PC4_08_V	KGT44_PC4_09_L
Process Pipe	0-2"	0	0	0	0	0	0	0	0
	3"-6"	0	0	0	0	0	0	0	0
	7"-12"	0	0	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0	0
Process Pipe (Inter-unit)	0-2"	0	0	0	0	0	0	0	0
	3"-6"	0	0	0	87	0	0	0	0
	7"-12"	0	0	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0	0
Flange	0-2"	0	0	0	4	0	0	0	0
	3"-6"	0	0	0	11	0	0	0	0
	7"-12"	0	0	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0	0
Manual Valves	0-2"	0	0	0	8	0	0	0	0
	3"-6"	0	0	0	3	0	0	0	0
	7"-12"	0	0	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0	0
Actuated Valves	0-2"	0	0	0	5	0	0	0	0
	3"-6"	0	0	0	2	0	0	0	0
	7"-12"	0	0	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0	0
Small Bore Fittings	2"	0	0	0	1	0	0	0	0
Process Vessel/ Storage Tank	<= 6"	0.5	0.5	0.5	0	0.5	0.5	0.5	0.5
	> 6 "	0	0	0	0	0	0	0	0
Centrifugal Pump	<= 6"	0	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0	0
Reciprocating Pump	<= 6"	0	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0	0
Centrifugal Compressor	<= 6"	0	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0	0
Reciprocating Compressor	<= 6"	0	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0	0
Shell Side Heat Exchanger	<= 6"	0	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0	0
Tube Side Heat Exchanger	<= 6"	0	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0	0
Plate Heat Exchanger	<= 6"	0	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0	0
Air Cooled Heat Exchanger	<= 6"	0	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0	0
Filters	<= 6"	0	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0	0
Pig Trap	<= 6"	0	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0	0
Loading Hose	-	0	0	0	0	0	0	0	0
Loading Arm	-	0	0	0	0	0	0	0	0

Equipment	Size	KGT45_PC3_12_L	KGT46_PC4_11_L	KGT47_LPG_01_L	KGT47_LPG_02_L	KGT47_LPG_05_L
Process Pipe	0-2"	0	0	0	0	0
	3"-6"	0	0	15	0	0
	7"-12"	15	15	0	0	0
	13"-18"	0	0	0	0	0
	19"-24"	0	0	0	0	0
	25"-36"	0	0	0	0	0
Process Pipe (Inter-unit)	0-2"	0	0	0	0	0
	3"-6"	0	0	0	0	0
	7"-12"	0	0	0	0	0
	13"-18"	0	0	0	0	0
	19"-24"	0	0	0	0	0
-	25"-36"	0	0	0	0	0
Flange	0-2"	6	2	0	0	0
	3"-6"	18	12	11	0	0
	7"-12"	8	6	0	0	0
	13"-18"	0	0	0	0	0
	19"-24"	0	0	0	0	0
	25"-36"	0	0	0	0	0
Manual Valves	0-2"	13	6	4	0	0
	3"-6"	3	2	3	0	0
	7"-12"	2	2	0	0	0
	13"-18"	0	0	0	0	0
	19"-24"	0	0	0	0	0
	25"-36"	0	0	0	0	0
Actuated Valves	0-2"	5	4	2	0	0
	3"-6"	5	3	0	0	0
	7"-12"	0	0	0	0	0
	13"-18"	0	0	0	0	0
	19"-24"	0	0	0	0	0
	25"-36"	0	0	0	0	0
Small Bore Fittings	2"	4	3	3	0	0
Process Vessel/ Storage Tank	<= 6"	0	0	0	0	0
	> 6 "	0	0	0	0	0
Centrifugal Pump	<= 6"	1	1	0	0	0
	> 6 "	0	0	0	0	0
Reciprocating Pump	<= 6"	0	0	0	0	0
	> 6 "	0	0	0	0	0
Centrifugal Compressor	<= 6"	0	0	0	Ō	0
	> 6 "	0	0	0	0	0
Reciprocating Compressor	<= 6"	0	0	0	0	0
	> 6 "	0	0	0	0	0
Shell Side Heat Exchanger	<= 6"	0	0	0	0	0
	> 6 "	0	0	0	0	0
Tube Side Heat Exchanger	<= 6"	0	0	0	0	0
	> 6 "	0	0	0	0	0
Plate Heat Exchanger	<= 6"	0	0	0	0	0
	> 6 "	0	0	0	0	0
Air Cooled Heat Exchanger	<= 6"	0	0	0	0	0
	> 6 "	0	0	0	0	0
Filters	<= 6"	0	0	0	0	0
	<= 6" > 6 "	1	1	0	0	0
Dia Tran				-	-	
Pig Trap	<= 6"	0	0	0	0	0
La adhara Lla a	> 6 "	0	0	0	0	0
Loading Hose	-	0	0	0	0	1
Loading Arm	-	0	0	0	1	0

## Propane Refrigeration

Equipment	Size	KGT70_REF_01_V	KGT70_REF_02_L	KGT70_REF_03_V	KGT70_REF_04_L	KGT70_REF_05_L	KGT70_REF_07_L	KGT70_REF_11_V
Process Pipe	0-2"	0	0	0	0	0	0	0
	3"-6"	15	15	22	0	15	15	0
	7"-12"	0	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0
Process Pipe (Inter-unit)	0-2"	0	0	0	0	0	0	0
	3"-6"	0	0	0	0	0	0	0
	7"-12"	0	0	0	174	0	0	154
	13"-18"	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0
Flange	0-2"	3	6	3	21	5	3	7
	3"-6"	1	8	23	1	3	2	13
	7"-12"	0	0	0	3	0	0	24
	13"-18"	0	0	0	0	0	0	0
	_			-				
	19"-24"	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0
Manual Valves	0-2"	2	2	2	15	1	1	12
	3"-6"	0	3	7	0	0	1	5
	7"-12"	0	0	0	0	0	0	6
	13"-18"	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0
Actuated Valves	0-2"	1	1	1	6	0	0	3
	3"-6"	1	0	1	0	0	0	1
	7"-12"	0	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0
Small Bore Fittings	2"	3	3	4	5	5	2	7
Process Vessel	<= 6"	0.5	0.5	0.5	0	0	0	0
	> 6 "	0	0	0	0.5	0	0	0.5
Centrifugal Pump	<= 6"	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0
Posiproacting Dump	<= 6"	0	0	0	0	0	0	0
Reciprocating Pump	> 6 "	0	0	0	0	0	0	0
Contrifunal Compressor	<= 6"	0	0	0	0	0	0	0
Centrifugal Compressor	<= 6 "			0				0
		0	0		0	0	0	
Reciprocating Compressor	<= 6"	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0
Shell Side Heat Exchanger	<= 6"	0	0	0	0	1	1	0
	> 6 "	0	0	0	0	0	0	0
Tube Side Heat Exchanger	<= 6"	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0
Plate Heat Exchanger	<= 6"	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0
Air Cooled Heat Exchanger	<= 6"	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0
Filters	<= 6"	0	0	2	0	0	0	0
	> 6 "	0	0	0	0	0	0	2
Pig Trap	<= 6"	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0

Equipment	Size	KGT70_REF_14_V	KGT70_REF_15_L	KGT70_REF_06_L
Process Pipe	0-2"	0	0	0
	3"-6"	0	0	64
	7"-12"	65	28	0
	13"-18"	0	0	0
	19"-24"	0	0	0
	25"-36"	0	0	0
Process Pipe (Inter-unit)	0-2"	0	0	0
	3"-6"	0	0	0
	7"-12"	0	0	0
	13"-18"	0	0	0
	19"-24"	0	0	0
	25"-36"	0	0	0
Flange	0-2"	13	1	5
Ī	3"-6"	22	4	8
	7"-12"	1	1	0
	13"-18"	0	0	0
	19"-24"	0	0	0
	25"-36"	0	0	0
Manual Valves	0-2"	7	5	1
	3"-6"	4	1	3
	7"-12"	0	0	0
	13"-18"	0	0	0
	19"-24"	0	0	0
	25"-36"	0	0	0
Actuated Valves	0-2"	2	0	0
	3"-6"	1	0	0
	7"-12"	0	0	0
	13"-18"	0	0	0
	19"-24"	0	0	0
	25"-36"	0	0	0
Small Bore Fittings	2"	20	8	4
Process Vessel	<= 6"	2	0	0
	> 6 "	0	0	0
Centrifugal Pump	<= 6"	0	0	0
	> 6 "	0	0	0
Reciprocating Pump	<= 6"	0	0	0
· · · ·	> 6 "	0	0	0
Centrifugal Compressor	<= 6"	0	0	0
	> 6 "	0	0	0
Reciprocating Compressor	<= 6"	0	0	0
	> 6 "	2	0	0
Shell Side Heat Exchanger	<= 6"	0	0	1
	> 6 "	0	0	0
Tube Side Heat Exchanger	<= 6"	0	0	0
	> 6 "	0	0	0
Plate Heat Exchanger	<= 6"	0	0	0
	> 6 "	0	0	0
Air Cooled Heat Exchanger	<= 6"	0	2	0
	> 6 "	0	1	0
Filters	<= 6"	0	0	0
	> 6 "	0	0	0
Pig Trap	<= 6"	0	0	0
	> 6 "	0	0	0

#### Mercaptans and Methanol Injection System

Equipment	Size	KGT50_EMC_01_L	KGT50_EMC_02_L	KGT51_BMC_05_L	KGT52_BMC_01_L	KGT52_BMC_02_L	KGT52_BMC_03_L	KGT55_MOH_01_L	KGT55_MOH_02_L	KGT55_MOH_03_L
Process Pipe	0-2"	15	0	0	0	15	0	0	0	0
	3"-6"	0	0	0	0	0	0	0	0	0
	7"-12"	0	0	0	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0	0	0
Process Pipe (Inter-unit)	0-2"	0	0	0	0	0	0	0	343	0
	3"-6"	0	0	0	0	0	0	0	0	0
	7"-12"	0	0	0	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0	0	0
Flange	0-2"	0	0	0	0	3	0	0	17	0
- Kango	3"-6"	0	0	0	0	0	0	0	0	0
	7"-12"	0	0	0	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0	0	0
Manual Valves	0-2"	19	0	0	0	17	0	0	55	0
	3"-6"	0	0		0	0	0	0	0	0
	7"-12"	-		0	-		-	-		0
		0	0	0	0	0	0	0	0	-
	13"-18"	0	0	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0	0	0
Actuated Valves	0-2"	3	0	0	0	0	0	0	2	0
	3"-6"	0	0	0	0	0	0	0	0	0
	7"-12"	0	0	0	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0	0	0
Small Bore Fittings	2"	3	0	0	0	6	0	0	9	0
Storage Tank /Portable Drum	<= 6"	0	1	1	1	0	0	4	0	0
	> 6 "	0	0	0	0	0	0	0	0	0
Centrifugal Pump	<= 6"	1	0	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0	0	0
Reciprocating Pump	<= 6"	0	0	0	0	1	0	0	2	0
	> 6 "	0	0	0	0	0	0	0	0	0
Centrifugal Compressor	<= 6"	0	0	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0	0	0
Reciprocating Compressor	<= 6"	0	0	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0	0	0
Shell Side Heat Exchanger	<= 6"	0	0	0	0	0	0	0	0	0
j j	> 6 "	0	0	0	0	0	0	0	0	0
Tube Side Heat Exchanger	<= 6"	0	0	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0	0	0
Plate Heat Exchanger	<= 6"	0	0	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0	0	0
Air Cooled Heat Exchanger	<= 6"	0	0	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0	0	0
Filters	<= 6"	1	0	0	0	2	0	0	4	0
	> 6 "	0	0	0	0	0	0	0	0	0
Din Tren	<= 6"	1					0			0
Pig Trap	-		0	0	0	0		0	0	
Leadier Lleas	> 6 "	0	0	0	0	0	0	0	0	0
Loading Hose	-	0	0	0	0	0	1	0	0	1
Loading Arm	-	0	0	0	0	0	0	0	0	0

## CO2 Recovery - Ammonia

Equipment	Size	KGT80_AMM_01_V	KGT80_AMM_11_V	KGT80_AMM_02_V	KGT80_AMM_03_L	KGT80_AMM_04_L	KGT80_AMM_07_L	KGT80_AMM_08_V	KGT80_AMM_09_V
Process Pipe	0-2"	0	0	15	0	0	38	0	0
	3"-6"	15	15	0	15	21	0	0	48
	7"-12"	0	0	0	0	0	0	15	0
	13"-18"	0	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0	0
Process Pipe (Inter-unit)	0-2"	0	0	0	0	0	0	0	0
	3"-6"	0	0	0	0	0	0	0	0
	7"-12"	0	0	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0	0
Flange	0-2"	6	2	2	6	21	8	6	37
	3"-6"	9	7	0	2	0	0	10	1
	7"-12"	0	0	0	0	0	0	4	0
	13"-18"	0	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0	0
Manual Valves	0-2"	12	8	7	9	21	14	12	21
	3"-6"	4	3	0	0	0	0	4	0
	7"-12"	0	0	0	0	0	0	1	0
	13"-18"	0	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0	0
A studted ) (sluce	0-2"	1	2	2	0	9	2	1	7
Actuated Valves	3"-6"	0	0	0	0	0	0	0	0
	7"-12"	0	0	0	0		0	0	0
						0			
	13"-18" 19"-24"	0	0	0	0	0	0	0	0
		0			0				0
	25"-36"	0	0	0	0	0	0	0	0
Small Bore Fittings	2"	6	7	4	2	6	4	4	7
Process Vessel	<= 6"	0.5	0.5	1	1	0	0	0	0
	> 6 "	0	0	0	0	0	0	0	0
Centrifugal Pump	<= 6"	0	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0	0
Reciprocating Pump	<= 6"	0	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0	0
Centrifugal Compressor	<= 6"	0	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0	0
Reciprocating Compressor	<= 6"	0	0	0	0	0	0	0	0
	> 6 "	1	1	0	0	0	0	0	0
Shell Side Heat Exchanger	<= 6"	0	0	0	0	1	1	1	0
	> 6 "	0	0	0	0	0	0	0	0
Tube Side Heat Exchanger	<= 6"	0	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0	0
Plate Heat Exchanger	<= 6"	0	0	0	2	2	0	0	2
	> 6 "	0	0	0	0	0	0	0	0
Air Cooled Heat Exchanger	<= 6"	0	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0	0
Filters	<= 6"	0	0	0	0	3	0	1	2
	> 6 "	0	0	0	0	0	0	0	0
Pig Trap	<= 6"	0	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0	0

#### CO2 Recovery - CO2

Equipment	Size	KGT90_CO2_01_V	KGT90_CO2_02_V	KGT90_CO2_03_V	KGT90_CO2_07_V	KGT90_CO2_08_L	KGT90_CO2_16_V	KGT90_CO2_18_V	KGT90_CO2_19_V	KGT90_CO2_23_V
Process Pipe	0-2"	0	0	0	0	0	0	0	0	0
	3"-6"	15	15	31	89	71	0	0	15	0
	7"-12"	0	0	0	0	0	0	0	0	15
	13"-18"	0	0	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0	0	0
Process Pipe (Inter-unit)	0-2"	0	0	0	0	0	0	321	0	0
	3"-6"	0	0	0	0	0	0	0	0	0
	7"-12"	0	0	0	0	0	180	0	0	0
	13"-18"	0	0	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0	0	0
Flange	0-2"	2	4	5	33	35	11	30	44	0
	3"-6"	9	6	15	26	11	11	0	5	2
	7"-12"	0	0	0	0	0	60	0	0	3
	13"-18"	0	0	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0	0	0
Manual Valves	0-2"	3	5	3	18	23	18	33	22	1
	3"-6"	2	2	1	15	7	2	0	1	0
	7"-12"	0	0	0	0	0	18	0	0	0
		0			0			0		0
	13"-18"		0	0		0	0		0	
	19"-24"	0	0	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0	0	0
Actuated Valves	0-2"	2	2	1	1	12	0	2	5	0
	3"-6"	0	0	1	0	0	2	0	0	1
	7"-12"	0	0	0	0	0	2	0	0	1
	13"-18"	0	0	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0	0	0
Small Bore Fittings	2"	9	9	6	9	9	25	2	19	1
Process Vessel/ Storage Tank	<= 6"	2	2	2	2	1	0	0	2	0
	> 6 "	0	0	0	0	0	5.5	0	0	1
Centrifugal Pump	<= 6"	0	0	0	0	1	0	0	0	0
	> 6 "	0	0	0	0	0	0	0	0	0
Reciprocating Pump	<= 6"	0	0	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0	0	0
Centrifugal Compressor	<= 6"	0	0	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	2	0	0	0
Reciprocating Compressor	<= 6"	0	0	0	0	0	0	0	0	0
	> 6 "	1	1	0	0	0	0	0	0	0
Shell Side Heat Exchanger	<= 6"	0	0	1	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0	0	0
Tube Side Heat Exchanger	<= 6"	1	1	1	0	1	0	0	0	0
	> 6 "	0	0	0	0	0	0	0	0	0
Plate Heat Exchanger	<= 6"	0	0	0	0	0	2	0	0	0
Ŭ Ŭ	> 6 "	0	0	0	0	0	0	0	0	0
Air Cooled Heat Exchanger	<= 6"	0	0	0	0	0	0	0	2	0
	> 6 "	0	0	0	0	0	0	0	0	0
Filters	<= 6"	0	0	0	1	1	0	0	0	0
	> 6 "	0	0	0	0	0	0	0	0	0
Pig Trap	<= 6"	0	0	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0	0	0
Loading Hose	>0	0	0	0	0	0	0	0	0	0
	-	0			0			0		0
Loading Arm	-	0	0	0	U	0	0	0	0	0

Equipment	Size	KGT90_CO2_09_L	KGT90_CO2_10_L	KGT90_CO2_11_L	KGT90_CO2_12_L	KGT90_CO2_24_L	KGT90_CO2_25_L	KGT90_CO2_26_V
Process Pipe	0-2"	0	0	0	0	0	15	23
	3"-6"	0	0	0	0	71	0	0
	7"-12"	0	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0
Process Pipe (Inter-unit)	0-2"	0	0	0	0	0	0	0
	3"-6"	0	0	0	0	0	0	0
	7"-12"	0	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0
Flange	0-2"	0	0	0	0	4	11	7
	3"-6"	0	0	0	0	17	0	0
	7"-12"	0	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0
Manual Valves	0-2"	0	0	0	0	5	3	11
	3"-6"	0	0	0	0	13	0	0
	7"-12"	0	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0
Actuated Valves	0-2"	0	0	0	0	10	2	1
	3"-6"	0	0	0	0	0	0	0
	7"-12"	0	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0	0
Small Bore Fittings	2"	0	0	0	0	1	2	1
Process Vessel/ Storage Tank	<= 6"	1	1	1	1	0	0	0
	> 6 "	0	0	0	0	0	0	0
Centrifugal Pump	<= 6"	0	0	0	0	1	0	0
	> 6 "	0	0	0	0	0	0	0
Reciprocating Pump	<= 6"	0	0	0	0	0	1	0
	> 6 "	0	0	0	0	0	0	0
Centrifugal Compressor	<= 6"	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0
Reciprocating Compressor	<= 6"	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0
Shell Side Heat Exchanger	<= 6"	0	0	0	0	0	0	0
5	> 6 "	0	0	0	0	0	0	0
Tube Side Heat Exchanger	<= 6"	0	0	0	0	0	0	0
3	> 6 "	0	0	0	0	0	0	0
Plate Heat Exchanger	<= 6"	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0
Air Cooled Heat Exchanger	<= 6"	0	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0	0
Filters	<= 6"	0	0	0	0	1	1	0
	> 6 "	0	0	0	0	0	0	0
Pig Trap	<= 6"	0	0	0	0	0	0	0
- ig indp	> 6 "	0	0	0	0	0	0	0
Loading Hose		0	0	0	0	0	0	0
Loading 11030	1 -	U	, v	, v	0	0	, v	v

Equipment	Size	KGT90_CO2_27_V	KGT90_CO2_28_L	KGT90_CO2_29_V	KGT90_CO2_30_L	KGT90_CO2_31_V	KGT90_CO2_32_L
Process Pipe	0-2"	15	0	0	0	0	0
	3"-6"	0	0	0	0	0	0
	7"-12"	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0
Process Pipe (Inter-unit)	0-2"	0	0	0	0	0	0
	3"-6"	0	0	0	0	0	0
	7"-12"	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0
Flange	0-2"	5	0	0	0	0	0
1101190	3"-6"	0	0	0	0	0	0
	7"-12"	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0
-	25"-36"	0	0	0	0	0	0
Manual Valves	0-2"	6	0	0	0	0	0
	3"-6"	0	0	0	0	0	0
	7"-12"	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0
Actuated Valves	0-2"	3	0	0	0	0	0
	3"-6"	0	0	0	0	0	0
	7"-12"	0	0	0	0	0	0
	13"-18"	0	0	0	0	0	0
	19"-24"	0	0	0	0	0	0
	25"-36"	0	0	0	0	0	0
Small Bore Fittings	2"	1	0	0	0	0	0
Process Vessel/ Storage Tank	<= 6"	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0
Centrifugal Pump	<= 6"	0	0	0	0	0	0
	> 6 "	Ō	0	0	0	0	0
Reciprocating Pump	<= 6"	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0
Centrifugal Compressor	<= 6"	0	0	0	0	0	0
<b>V</b>	> 6 "	0	0	0	0	0	0
Reciprocating Compressor	<= 6"	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0
Shell Side Heat Exchanger	<= 6"	0	0	0	0	0	0
onen olde meat Exchanger	> 6 "	0	0	0	0	0	0
Tube Side Heat Exchanger	<= 6"	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0
Plate Heat Exchanger	> 6 " <= 6"	0	0	0	0	0	0
Plate Heat Exchanger			-				
Air Cooled Heat Frederic	> 6 "	0	0	0	0	0	0
Air Cooled Heat Exchanger	<= 6"	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0
Filters	<= 6"	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0
Pig Trap	<= 6"	0	0	0	0	0	0
	> 6 "	0	0	0	0	0	0
Loading Hose	-	0	1	1	1	1	1
Loading Arm	-	0	0	0	0	0	0





Appendix 3. Estimated Piping Lengths





# Table A3- 1: Estimated Piping Lengths

From	То	Estimated length (m) Note1	After applied 25% Safety Factor (m)		
Raw Gas from (M-507)	Absorber Towers (D-101-1/2) inlet Valves (PV-101-1/2) and bypass to Separator (D-201-4) top line	207	259		
Inlet Separator (M-507)	LPG Surge Vaporiser (F-201)	174	218		
300 line & 309 line (XSV-594)	AUP/ Ballance & Lactose Plant -306 line (up to XSV-9622)	88.7	111		
High Temperature Separator (M-307)	KPS and Whareroa (up to KPS/KGTP Site Boundary)	183	229		
Product Gas header near LTS pipe bridge	Gas Storage Compressors in LTS unit (via LTS pipe bridge)	219	274		
Product Gas compressors (C-903-2/3/5)	Stores/ Workshop/ Admin. Building (end of pipe rack)	201	251		
Product Gas compressors (C-903-2/3/5)	100/200 Pipelines in Transmission metering area (via LTS pipe bridge)	222	278		
Fuel Gas Superheater (E-603)	HRSG A/B Burners (B-604-A-1/2/3, B-604-B1/2/3)	111	138		
Product Gas header from Gas Treatment Plant	Ammonia/ CO <sub>2</sub> Compressor Engines (CE-821/822) in CO <sub>2</sub> Recovery Unit	123	154		
Product Gas header from Gas Treatment Plant	Gas Flare System Burners (D1-4100B)	219	274		
High Temperature Separator (M-307)	De-ethaniser (D-420-2)	155	194		
De-Ethaniser(D-420-2)	OVHD Compressor (C-421-1/2)	88	110		
De-Ethaniser OVHD Compressor (C-421-1)	Absorber Towers (D-101-1/2) and Decanted Water Strippers (D-201-3/4)	115	143		
Wash Water Coalescer (M-302)	Stabiliser (D-420-1)	115	144		
De-Butaniser (D-440-2)	Surge Vaporiser (F-201)	134	168		
60/40 Condensing Tank (M-430)	XSV-434 on KPS export line (up to KPS/KGTP Site Boundary)	186	232		
Gasoline Cooler (E-460)	KPS (up to KPS/KGTP Site Boundary)	168	210		
Gasoline Cooler (E-460)	NGL Storage Tank (F-4033)	83 (aboveground) 475 (underground) <sup>Note2</sup>	578 Note2		
Propane Product Coolers (E-4001-1/2)	Propane Storage Vessels (F-4003, F-4004)	81 (aboveground) 475 (underground) <sup>Note2</sup>	556 Note2		
De-Butaniser Reflux Pumps (G-440-3/4)	Butane Storage Vessels (F-4001, F-4002)	70 (aboveground) 475 (underground) <sup>Note2</sup>	562 Note2		
Propane Refrigerant Economiser (D-315-2)	Gas Chiller (E-313-3), De-Ethaniser Overhead Condenser (E-420-2)	140	174		
Gas Chiller (E-313-3), De-Ethaniser Overhead Condenser (E-420-2)	Compressors (C-330-1/ 2)	123	154		
Methanol Storage Tanks (F-502-1/2/4/6)	De-ethaniser (D-420-2), HT Separator Condensate Pumps (G-30101/2), Gas/gas Heat Exchanger (E-313-1/2)	274	343		
Raw Gas Boosters (C-885 / C-823)	CO <sub>2</sub> Compressors (C-802/822)	144	180		
CO <sub>2</sub> storages (F-801-1/2/3)	Utility CO <sub>2</sub> users: Product Gas Compressor Shelter and LPG Storage tanks	257 (aboveground) 475 (underground) <sup>Note2</sup>	796 Note2		

Note:

- 1. The piping lengths are measured from KGTP Layout drawings using scale. A safety factor of 1.25 has been applied to all lengths measured from the map to account for bends and elevations which could not be determined from the 2D map.
- 2. Underground length (475m) is indicated on P&ID (1000000-0104-0033-01). 25% safety factor is only applied to above ground section, assuming no bend and elevation change for underground piping section.





Appendix 4. Leak Frequencies



# Table A4- 1: Leak Frequencies

No	Node Section		Ba	ase Case/ Sensitiv	vity Case 1 Releas	e Frequencies (p	er year)	Sensitivity 2 (Future Production) Release Frequencies (per year)							
		1 - 3 mm (2 mm)	3 - 10 mm (6 mm)	10 - 50 mm (22 mm)	50 - 150 mm (85 mm)	> 150 mm (Rupture)	Total	% Contribution	1 - 3 mm (2 mm)	3 - 10 mm (6 mm)	10 - 50 mm (22 mm)	50 - 150 mm (85 mm)	> 150 mm (Rupture)	Total	% Contribution
			1	•			Raw Gas and	l Maui Gas Lines	1	•	L			•	
1	KGT01_RGS_01_V	6.06E-03	2.72E-03	1.52E-03	2.82E-04	5.65E-05	1.06E-02	1.19%	6.06E-03	2.72E-03	1.52E-03	2.82E-04	5.65E-05	1.06E-02	1.00%
2	KGT01_RCS_01_L	1.31E-03	6.00E-04	3.07E-04	1.04E-04	2.44E-06	2.32E-03	0.26%	1.31E-03	6.00E-04	3.07E-04	1.04E-04	2.44E-06	2.32E-03	0.22%
3	KGT01_MAU_01_V	4.12E-03	1.83E-03	1.02E-03	1.39E-04	3.51E-05	7.14E-03	0.80%	4.12E-03	1.83E-03	1.02E-03	1.39E-04	3.51E-05	7.14E-03	0.67%
4	KGT01_MAU_02_V	3.54E-03	1.43E-03	6.57E-04	8.28E-05	9.16E-06	5.72E-03	0.64%	3.54E-03	1.43E-03	6.57E-04	8.28E-05	9.16E-06	5.72E-03	0.54%
				•	·		CO <sub>2</sub> I	Removal	•						
5	KGT02_TGS_01_V	3.09E-03	1.42E-03	7.86E-04	1.97E-04	1.46E-05	5.51E-03	0.61%	3.09E-03	1.42E-03	7.86E-04	1.97E-04	1.46E-05	5.51E-03	0.52%
6	KGT03_TGS_04_V	3.03E-03	1.40E-03	7.73E-04	1.87E-04	2.11E-05	5.41E-03	0.60%	3.03E-03	1.40E-03	7.73E-04	1.87E-04	2.11E-05	5.41E-03	0.51%
7	KGT05_RGS_07_V	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00%	2.50E-03	1.13E-03	6.03E-04	9.17E-05	3.21E-05	4.36E-03	0.41%
8	KGT05_TGS_16_V	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00%	4.14E-03	1.86E-03	1.04E-03	1.35E-04	4.91E-05	7.23E-03	0.68%
							Dehydration and	d Dewpoint Control							
9	KGT01_TGS_07_V	4.84E-03	2.14E-03	1.17E-03	1.55E-04	3.03E-05	8.34E-03	0.93%	4.84E-03	2.14E-03	1.17E-03	1.55E-04	3.03E-05	8.34E-03	0.79%
10	KGT01_TGS_10_V	3.37E-03	1.65E-03	9.73E-04	1.88E-04	1.03E-04	6.28E-03	0.70%	3.37E-03	1.65E-03	9.73E-04	1.88E-04	1.03E-04	6.28E-03	0.59%
11	KGT01_TGS_12_V	2.19E-03	1.03E-03	5.89E-04	9.96E-05	4.51E-05	3.95E-03	0.44%	2.19E-03	1.03E-03	5.89E-04	9.96E-05	4.51E-05	3.95E-03	0.37%
12	KGT01_PGS_02_V	3.63E-03	1.68E-03	8.67E-04	1.66E-04	5.65E-05	6.40E-03	0.71%	3.63E-03	1.68E-03	8.67E-04	1.66E-04	5.65E-05	6.40E-03	0.60%
13	KGT04_PGS_07_V	1.25E-03	5.44E-04	2.82E-04	4.54E-05	3.86E-06	2.12E-03	0.24%	1.25E-03	5.44E-04	2.82E-04	4.54E-05	3.86E-06	2.12E-03	0.20%
14	KGT01_MPG_01_L	1.32E-03	5.88E-04	3.08E-04	6.92E-05	1.44E-06	2.29E-03	0.25%	1.32E-03	5.88E-04	3.08E-04	6.92E-05	1.44E-06	2.29E-03	0.22%
15	KGT04_MPG_03_L	1.68E-03	7.74E-04	3.88E-04	1.33E-04	4.74E-06	2.98E-03	0.33%	1.68E-03	7.74E-04	3.88E-04	1.33E-04	4.74E-06	2.98E-03	0.28%
16	KGT04_MPG_04_L	1.87E-03	7.41E-04	3.10E-04	7.55E-05	2.13E-06	3.00E-03	0.33%	1.87E-03	7.41E-04	3.10E-04	7.55E-05	2.13E-06	3.00E-03	0.28%
17	KGT04_MPG_05_L	3.13E-03	8.28E-04	2.39E-04	3.09E-05	2.48E-06	4.23E-03	0.47%	3.13E-03	8.28E-04	2.39E-04	3.09E-05	2.48E-06	4.23E-03	0.40%
18	KGT04_MPG_06_L	2.33E-03	1.02E-03	5.32E-04	1.01E-04	3.86E-06	3.99E-03	0.45%	2.33E-03	1.02E-03	5.32E-04	1.01E-04	3.86E-06	3.99E-03	0.38%
19	KGT01_TGS_11_V	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00%	2.52E-03	1.28E-03	7.71E-04	3.57E-04	1.02E-05	4.94E-03	0.47%
20	KGT01_PGS_03_V	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00%	3.89E-03	1.75E-03	8.83E-04	2.48E-04	3.17E-06	6.78E-03	0.64%
21	KGT01_MPG_02_L	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00%	1.01E-03	4.44E-04	2.28E-04	4.47E-05	1.44E-06	1.73E-03	0.16%
			1	1	1 1		Product Gas Line	es and Compressors	1			1		I	
22	KGT01_PGS_01_V	5.87E-03	2.59E-03	1.44E-03	1.84E-04	3.56E-05	1.01E-02	1.13%	5.87E-03	2.59E-03	1.44E-03	1.84E-04	3.56E-05	1.01E-02	0.96%
23	KGT01_PGS_13_V	1.83E-03	7.99E-04	3.99E-04	8.55E-05	1.44E-06	3.12E-03	0.35%	1.83E-03	7.99E-04	3.99E-04	8.55E-05	1.44E-06	3.12E-03	0.29%
24	KGT01_PGS_14_V	7.70E-04	3.48E-04	1.90E-04	2.66E-05	1.02E-05	1.34E-03	0.15%	7.70E-04	3.48E-04	1.90E-04	2.66E-05	1.02E-05	1.34E-03	0.13%
25	KGT13_PGS_15_V	3.71E-03	1.68E-03	8.83E-04	2.47E-04	5.23E-05	6.57E-03	0.73%	3.71E-03	1.68E-03	8.83E-04	2.47E-04	5.23E-05	6.57E-03	0.62%
26	KGT13_PGS_16_V	7.35E-03	3.16E-03	1.49E-03	4.24E-04	8.35E-06	1.24E-02	1.39%	7.35E-03	3.16E-03	1.49E-03	4.24E-04	8.35E-06	1.24E-02	1.17%
27	KGT13_PGS_17_V	3.88E-03	1.80E-03	1.01E-03	1.76E-04	6.43E-05	6.93E-03	0.77%	3.88E-03	1.80E-03	1.01E-03	1.76E-04	6.43E-05	6.93E-03	0.65%





No	Node Section		Ba	ase Case/ Sensitiv	vity Case 1 Releas	e Frequencies (p	er year)	Sensitivity 2 (Future Production) Release Frequencies (per year)							
		1 - 3 mm (2 mm)	3 - 10 mm (6 mm)	10 - 50 mm (22 mm)	50 - 150 mm (85 mm)	> 150 mm (Rupture)	Total	% Contribution	1 - 3 mm (2 mm)	3 - 10 mm (6 mm)	10 - 50 mm (22 mm)	50 - 150 mm (85 mm)	> 150 mm (Rupture)	Total	% Contribution
28	KGT01_MGS_01_V	1.38E-02	5.91E-03	2.89E-03	5.52E-04	1.22E-04	2.33E-02	2.60%	1.38E-02	5.91E-03	2.89E-03	5.52E-04	1.22E-04	2.33E-02	2.20%
29	KGT01_MGS_03_V	7.12E-03	3.08E-03	1.47E-03	3.68E-04	2.68E-05	1.21E-02	1.34%	7.12E-03	3.08E-03	1.47E-03	3.68E-04	2.68E-05	1.21E-02	1.14%
30	KGT01_MGS_07_V	5.42E-03	2.31E-03	1.05E-03	3.11E-04	1.11E-05	9.10E-03	1.01%	5.42E-03	2.31E-03	1.05E-03	3.11E-04	1.11E-05	9.10E-03	0.86%
31	KGT11_MGS_05_V	2.16E-03	1.07E-03	6.38E-04	1.48E-04	7.01E-05	4.09E-03	0.46%	2.16E-03	1.07E-03	6.38E-04	1.48E-04	7.01E-05	4.09E-03	0.39%
32	KGT11_MGS_08_V	2.76E-03	1.20E-03	5.70E-04	1.56E-04	0.00E+00	4.68E-03	0.52%	2.76E-03	1.20E-03	5.70E-04	1.56E-04	0.00E+00	4.68E-03	0.44%
33	KGT11_MGS_09_V	8.16E-03	3.57E-03	1.87E-03	2.89E-04	5.86E-05	1.39E-02	1.56%	8.16E-03	3.57E-03	1.87E-03	2.89E-04	5.86E-05	1.39E-02	1.32%
				_			Pi	gging							
34	KGT01_PIG_01_V	9.52E-07	4.86E-07	2.70E-07	6.52E-08	2.91E-08	1.80E-06	0.00%	9.52E-07	4.86E-07	2.70E-07	6.52E-08	2.91E-08	1.80E-06	0.00%
35	KGT13_PIG_02_V	8.80E-07	4.56E-07	2.53E-07	6.52E-08	2.91E-08	1.68E-06	0.00%	8.80E-07	4.56E-07	2.53E-07	6.52E-08	2.91E-08	1.68E-06	0.00%
36	KGT11_PIG_03_V	8.76E-07	4.53E-07	2.52E-07	6.23E-08	2.91E-08	1.67E-06	0.00%	8.76E-07	4.53E-07	2.52E-07	6.23E-08	2.91E-08	1.67E-06	0.00%
37	KGT11_PIG_04_V	8.76E-07	4.53E-07	2.52E-07	6.23E-08	2.91E-08	1.67E-06	0.00%	8.76E-07	4.53E-07	2.52E-07	6.23E-08	2.91E-08	1.67E-06	0.00%
		Utilities and Cogen Unit													
38	KGT01_MPG_21_V	5.40E-03	2.28E-03	1.08E-03	2.10E-04	1.72E-05	8.98E-03	1.00%	5.40E-03	2.28E-03	1.08E-03	2.10E-04	1.72E-05	8.98E-03	0.85%
39	KGT01_MPG_22_L	1.66E-03	6.53E-04	2.58E-04	8.39E-05	0.00E+00	2.65E-03	0.30%	1.66E-03	6.53E-04	2.58E-04	8.39E-05	0.00E+00	2.65E-03	0.25%
40	KGT01_MPG_23_L	1.22E-03	5.37E-04	2.53E-04	8.31E-05	0.00E+00	2.10E-03	0.23%	1.22E-03	5.37E-04	2.53E-04	8.31E-05	0.00E+00	2.10E-03	0.20%
41	KGT01_FGA_01_V	5.24E-03	2.41E-03	1.34E-03	3.48E-04	1.44E-05	9.35E-03	1.04%	5.24E-03	2.41E-03	1.34E-03	3.48E-04	1.44E-05	9.35E-03	0.88%
42	KGT01_FGA_02_V	1.51E-02	6.35E-03	3.12E-03	4.50E-04	3.52E-05	2.50E-02	2.79%	1.51E-02	6.35E-03	3.12E-03	4.50E-04	3.52E-05	2.50E-02	2.36%
43	KGT01_PGS_19_V	7.50E-03	2.91E-03	1.15E-03	2.79E-04	3.46E-07	1.18E-02	1.32%	7.50E-03	2.91E-03	1.15E-03	2.79E-04	3.46E-07	1.18E-02	1.12%
44	KGT01_PGS_21_V	1.21E-02	4.59E-03	1.73E-03	4.04E-04	2.98E-06	1.88E-02	2.10%	1.21E-02	4.59E-03	1.73E-03	4.04E-04	2.98E-06	1.88E-02	1.77%
45	KGT01_PGS_22_V	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00%	4.86E-03	2.11E-03	1.05E-03	1.77E-04	2.45E-05	8.23E-03	0.78%
						LP	G Production Fac	ility - Stabiliser, De-C	2						
46	KGT01_MPG_07_L	1.83E-03	8.53E-04	4.70E-04	1.57E-04	4.63E-06	3.32E-03	0.37%	1.83E-03	8.53E-04	4.70E-04	1.57E-04	4.63E-06	3.32E-03	0.31%
47	KGT01_DET_01_V	2.51E-03	1.16E-03	6.33E-04	2.10E-04	4.55E-06	4.52E-03	0.50%	2.51E-03	1.16E-03	6.33E-04	2.10E-04	4.55E-06	4.52E-03	0.43%
48	KGT01_PGS_04_V	1.94E-03	8.86E-04	4.73E-04	1.27E-04	1.75E-06	3.43E-03	0.38%	1.94E-03	8.86E-04	4.73E-04	1.27E-04	1.75E-06	3.43E-03	0.32%
49	KGT01_PGS_05_V	1.04E-02	4.62E-03	2.15E-03	7.04E-04	8.73E-06	1.79E-02	2.00%	1.04E-02	4.62E-03	2.15E-03	7.04E-04	8.73E-06	1.79E-02	1.69%
50	KGT01_DEX_01_L	5.37E-03	1.75E-03	6.47E-04	1.45E-04	1.44E-06	7.91E-03	0.88%	5.37E-03	1.75E-03	6.47E-04	1.45E-04	1.44E-06	7.91E-03	0.75%
51	KGT01_DEB_01_L	2.93E-03	1.32E-03	6.85E-04	1.63E-04	3.51E-06	5.10E-03	0.57%	2.93E-03	1.32E-03	6.85E-04	1.63E-04	3.51E-06	5.10E-03	0.48%
52	KGT01_MPG_09_L	2.56E-03	1.13E-03	6.19E-04	8.89E-05	9.72E-06	4.41E-03	0.49%	2.56E-03	1.13E-03	6.19E-04	8.89E-05	9.72E-06	4.41E-03	0.42%
53	KGT01_MPG_10_V	1.34E-03	5.95E-04	3.06E-04	7.36E-05	1.44E-06	2.31E-03	0.26%	1.34E-03	5.95E-04	3.06E-04	7.36E-05	1.44E-06	2.31E-03	0.22%
54	KGT01_MPG_13_L	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00%	8.47E-04	3.63E-04	1.80E-04	3.18E-05	2.07E-06	1.42E-03	0.13%
55	KGT01_STT_01_V	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00%	3.49E-03	1.51E-03	8.04E-04	1.07E-04	3.86E-06	5.91E-03	0.56%
56	KGT01_PGS_10_V	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00%	3.46E-03	1.52E-03	7.82E-04	1.57E-04	1.11E-05	5.94E-03	0.56%





No	Node Section		Ba	ase Case/ Sensiti	vity Case 1 Releas	e Frequencies (p	er year)			Sen	sitivity 2 (Future	Production) Rele	ase Frequencies	(per year)	
		1 - 3 mm (2 mm)	3 - 10 mm (6 mm)	10 - 50 mm (22 mm)	50 - 150 mm (85 mm)	> 150 mm (Rupture)	Total	% Contribution	1 - 3 mm (2 mm)	3 - 10 mm (6 mm)	10 - 50 mm (22 mm)	50 - 150 mm (85 mm)	> 150 mm (Rupture)	Total	% Contribution
57	KGT01_PGS_11_V	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00%	9.26E-03	4.12E-03	1.89E-03	6.85E-04	4.20E-06	1.60E-02	1.51%
58	KGT01_STB_01_L	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00%	3.99E-03	1.75E-03	9.17E-04	1.58E-04	1.44E-06	6.82E-03	0.64%
							LPG Production	on Facility - De-C3							
59	KGT01_DPT_11_V	3.06E-03	1.27E-03	6.12E-04	1.26E-04	6.62E-06	5.08E-03	0.57%	3.06E-03	1.27E-03	6.12E-04	1.26E-04	6.62E-06	5.08E-03	0.48%
60	KGT01_DPX_11_L	4.59E-03	1.47E-03	5.91E-04	8.80E-05	3.86E-06	6.75E-03	0.75%	4.59E-03	1.47E-03	5.91E-04	8.80E-05	3.86E-06	6.75E-03	0.64%
61	KGT01_PC3_02_L	2.98E-03	1.34E-03	6.74E-04	1.84E-04	1.73E-06	5.17E-03	0.58%	2.98E-03	1.34E-03	6.74E-04	1.84E-04	1.73E-06	5.17E-03	0.49%
62	KGT01_DPB_11_L	4.09E-03	1.84E-03	9.47E-04	2.36E-04	6.76E-06	7.12E-03	0.79%	4.09E-03	1.84E-03	9.47E-04	2.36E-04	6.76E-06	7.12E-03	0.67%
63	KGT01_DPT_01_V	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00%	5.26E-03	2.19E-03	1.11E-03	1.31E-04	6.62E-06	8.70E-03	0.82%
64	KGT01_DPX_01_L	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00%	4.76E-03	1.54E-03	6.22E-04	8.62E-05	3.17E-06	7.01E-03	0.66%
65	KGT01_PC3_01_L	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00%	2.42E-03	1.09E-03	5.45E-04	1.69E-04	0.00E+00	4.22E-03	0.40%
66	KGT01_DPB_01_L	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00%	4.18E-03	1.86E-03	9.57E-04	2.07E-04	4.22E-06	7.21E-03	0.68%
							LPG Production	on Facility - De-C4							
67	KGT01_DBT_11_V	3.56E-03	1.52E-03	7.58E-04	1.83E-04	7.83E-06	6.03E-03	0.67%	3.56E-03	1.52E-03	7.58E-04	1.83E-04	7.83E-06	6.03E-03	0.57%
68	KGT01_DBX_11_L	7.28E-03	2.56E-03	1.07E-03	1.93E-04	2.13E-06	1.11E-02	1.24%	7.28E-03	2.56E-03	1.07E-03	1.93E-04	2.13E-06	1.11E-02	1.05%
69	KGT01_NGL_01_L	4.11E-03	1.82E-03	9.36E-04	1.98E-04	4.03E-06	7.06E-03	0.79%	4.11E-03	1.82E-03	9.36E-04	1.98E-04	4.03E-06	7.06E-03	0.67%
70	KGT01_NGL_02_L	5.96E-03	2.45E-03	1.11E-03	2.48E-04	2.21E-06	9.77E-03	1.09%	5.96E-03	2.45E-03	1.11E-03	2.48E-04	2.21E-06	9.77E-03	0.92%
71	KGT01_DBT_01_V	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00%	3.88E-03	1.62E-03	8.01E-04	1.32E-04	4.90E-06	6.44E-03	0.61%
72	KGT01_DBX_01_L	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00%	5.21E-03	1.74E-03	7.23E-04	1.12E-04	2.13E-06	7.78E-03	0.73%
73	KGT01_DBB_01_L	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00%	2.61E-03	1.17E-03	6.03E-04	1.53E-04	1.44E-06	4.54E-03	0.43%
74	KGT01_PC4_12_L	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00%	2.48E-03	1.12E-03	5.66E-04	2.02E-04	3.94E-06	4.37E-03	0.41%
75	KGT01_PC3_13_L	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00%	1.47E-03	6.34E-04	2.96E-04	7.85E-05	0.00E+00	2.48E-03	0.23%
76	KGT01_LPG_04_L	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00%	3.01E-03	1.30E-03	6.52E-04	1.29E-04	0.00E+00	5.10E-03	0.48%
			•			LPG Pro	duction Facility -	Product Export and Lo	oadout	•					•
77	KGT32_NGL_05_L	6.83E-04	2.98E-04	1.42E-04	4.45E-05	0.00E+00	1.17E-03	0.13%	6.83E-04	2.98E-04	1.42E-04	4.45E-05	0.00E+00	1.17E-03	0.11%
78	KGT33_NGL_06_L	1.49E-03	6.41E-04	3.22E-04	5.40E-05	1.68E-06	2.51E-03	0.28%	1.49E-03	6.41E-04	3.22E-04	5.40E-05	1.68E-06	2.51E-03	0.24%
79	KGT34_NGL_07_L	0.00E+00	1.00E-04	5.00E-06	0.00E+00	5.00E-06	1.10E-04	0.01%	0.00E+00	1.00E-04	5.00E-06	0.00E+00	5.00E-06	1.10E-04	0.01%
80	KGT35_NGL_09_L	4.77E-03	1.46E-03	4.84E-04	9.03E-05	5.59E-06	6.81E-03	0.76%	4.77E-03	1.46E-03	4.84E-04	9.03E-05	5.59E-06	6.81E-03	0.64%
81	KGT36_NGL_10_L	1.24E-03	5.63E-04	2.96E-04	7.35E-05	4.20E-06	2.18E-03	0.24%	1.24E-03	5.63E-04	2.96E-04	7.35E-05	4.20E-06	2.18E-03	0.21%
82	KGT36_NGL_11_L	0.00E+00	5.72E-02	0.00E+00	0.00E+00	5.72E-03	6.29E-02	7.02%	0.00E+00	8.00E-02	0.00E+00	0.00E+00	8.00E-03	8.80E-02	8.30%
82A	KGT36_NGL_12_L	0.00E+00	0.00E+00	0.00E+00	8.16E-08	8.16E-08	1.63E-07	0.00%	0.00E+00	0.00E+00	0.00E+00	1.14E-07	1.14E-07	2.28E-07	0.00%
83	KGT37_PC3_05_L	1.07E-03	4.68E-04	2.26E-04	5.09E-05	7.00E-06	1.82E-03	0.20%	1.07E-03	4.68E-04	2.26E-04	5.09E-05	7.00E-06	1.82E-03	0.17%
84	KGT39_PC3_07_V	0.00E+00	5.00E-06	2.50E-07	0.00E+00	2.50E-07	5.50E-06	0.00%	0.00E+00	5.00E-06	2.50E-07	0.00E+00	2.50E-07	5.50E-06	0.00%



W	or	ev
energy	chemicals   res	sources

No	Node Section		Ва	ase Case/ Sensiti	vity Case 1 Releas	e Frequencies (p	er year)			Sen	sitivity 2 (Future	Production) Rele	ase Frequencies	(per year)	
		1 - 3 mm (2 mm)	3 - 10 mm (6 mm)	10 - 50 mm (22 mm)	50 - 150 mm (85 mm)	> 150 mm (Rupture)	Total	% Contribution	1 - 3 mm (2 mm)	3 - 10 mm (6 mm)	10 - 50 mm (22 mm)	50 - 150 mm (85 mm)	> 150 mm (Rupture)	Total	% Contribution
85	KGT39_PC3_08_L	0.00E+00	5.00E-06	2.50E-07	0.00E+00	2.50E-07	5.50E-06	0.00%	0.00E+00	5.00E-06	2.50E-07	0.00E+00	2.50E-07	5.50E-06	0.00%
86	KGT40_PC3_09_V	0.00E+00	5.00E-06	2.50E-07	0.00E+00	2.50E-07	5.50E-06	0.00%	0.00E+00	5.00E-06	2.50E-07	0.00E+00	2.50E-07	5.50E-06	0.00%
87	KGT40_PC3_10_L	0.00E+00	5.00E-06	2.50E-07	0.00E+00	2.50E-07	5.50E-06	0.00%	0.00E+00	5.00E-06	2.50E-07	0.00E+00	2.50E-07	5.50E-06	0.00%
88	KGT41_PC4_04_L	1.33E-03	5.78E-04	2.70E-04	7.22E-05	5.33E-06	2.25E-03	0.25%	1.33E-03	5.78E-04	2.70E-04	7.22E-05	5.33E-06	2.25E-03	0.21%
89	KGT43_PC4_06_V	0.00E+00	5.00E-06	2.50E-07	0.00E+00	2.50E-07	5.50E-06	0.00%	0.00E+00	5.00E-06	2.50E-07	0.00E+00	2.50E-07	5.50E-06	0.00%
90	KGT43_PC4_07_L	0.00E+00	5.00E-06	2.50E-07	0.00E+00	2.50E-07	5.50E-06	0.00%	0.00E+00	5.00E-06	2.50E-07	0.00E+00	2.50E-07	5.50E-06	0.00%
91	KGT44_PC4_08_V	0.00E+00	5.00E-06	2.50E-07	0.00E+00	2.50E-07	5.50E-06	0.00%	0.00E+00	5.00E-06	2.50E-07	0.00E+00	2.50E-07	5.50E-06	0.00%
92	KGT44_PC4_09_L	0.00E+00	5.00E-06	2.50E-07	0.00E+00	2.50E-07	5.50E-06	0.00%	0.00E+00	5.00E-06	2.50E-07	0.00E+00	2.50E-07	5.50E-06	0.00%
93	KGT45_PC3_12_L	6.16E-03	2.08E-03	7.99E-04	1.52E-04	2.13E-05	9.22E-03	1.03%	6.16E-03	2.08E-03	7.99E-04	1.52E-04	2.13E-05	9.22E-03	0.87%
94	KGT46_PC4_11_L	5.54E-03	1.80E-03	6.51E-04	1.16E-04	1.75E-05	8.13E-03	0.91%	5.54E-03	1.80E-03	6.51E-04	1.16E-04	1.75E-05	8.13E-03	0.77%
95	KGT47_LPG_01_L	9.71E-04	4.15E-04	2.06E-04	3.29E-05	2.48E-06	1.63E-03	0.18%	9.71E-04	4.15E-04	2.06E-04	3.29E-05	2.48E-06	1.63E-03	0.15%
96	KGT47_LPG_02_L	0.00E+00	8.71E-04	0.00E+00	0.00E+00	8.71E-05	9.58E-04	0.11%	0.00E+00	1.79E-03	0.00E+00	0.00E+00	1.79E-04	1.97E-03	0.19%
96A	KGT47_LPG_03_L	0.00E+00	0.00E+00	0.00E+00	1.66E-07	1.66E-07	3.32E-07	0.00%	0.00E+00	0.00E+00	0.00E+00	3.41E-07	3.41E-07	6.82E-07	0.00%
97	KGT47_LPG_05_L	0.00E+00	6.24E-04	0.00E+00	0.00E+00	6.24E-05	6.86E-04	0.08%	0.00E+00	1.20E-03	0.00E+00	0.00E+00	1.20E-04	1.32E-03	0.12%
97A	KGT47_LPG_06_L	0.00E+00	0.00E+00	0.00E+00	8.90E-10	8.90E-10	1.78E-09	0.00%	0.00E+00	0.00E+00	0.00E+00	1.71E-09	1.71E-09	3.42E-09	0.00%
	·	·					Propane Refr	igeration System							
98	KGT70_REF_01_V	9.37E-04	4.14E-04	2.08E-04	4.63E-05	3.17E-06	1.61E-03	0.18%	9.37E-04	4.14E-04	2.08E-04	4.63E-05	3.17E-06	1.61E-03	0.15%
99	KGT70_REF_02_L	9.71E-04	4.28E-04	2.21E-04	4.47E-05	2.48E-06	1.67E-03	0.19%	9.71E-04	4.28E-04	2.21E-04	4.47E-05	2.48E-06	1.67E-03	0.16%
100	KGT70_REF_03_V	3.80E-03	1.50E-03	6.23E-04	1.33E-04	6.26E-06	6.05E-03	0.68%	3.80E-03	1.50E-03	6.23E-04	1.33E-04	6.26E-06	6.05E-03	0.57%
101	KGT70_REF_04_L	2.12E-03	9.36E-04	4.65E-04	1.06E-04	9.60E-06	3.63E-03	0.41%	2.12E-03	9.36E-04	4.65E-04	1.06E-04	9.60E-06	3.63E-03	0.34%
102	KGT70_REF_05_L	1.70E-03	7.66E-04	3.87E-04	1.05E-04	1.44E-06	2.96E-03	0.33%	1.70E-03	7.66E-04	3.87E-04	1.05E-04	1.44E-06	2.96E-03	0.28%
103	KGT70_REF_07_L	1.34E-03	6.17E-04	3.05E-04	1.05E-04	1.79E-06	2.37E-03	0.26%	1.34E-03	6.17E-04	3.05E-04	1.05E-04	1.79E-06	2.37E-03	0.22%
104	KGT70_REF_11_V	4.91E-03	1.99E-03	9.02E-04	1.49E-04	3.14E-05	7.98E-03	0.89%	4.91E-03	1.99E-03	9.02E-04	1.49E-04	3.14E-05	7.98E-03	0.75%
105	KGT70_REF_14_V	1.80E-02	8.15E-03	3.84E-03	8.13E-04	2.48E-04	3.10E-02	3.46%	1.80E-02	8.15E-03	3.84E-03	8.13E-04	2.48E-04	3.10E-02	2.93%
106	KGT70_REF_15_L	4.01E-03	1.52E-03	6.46E-04	1.03E-04	1.10E-05	6.28E-03	0.70%	4.01E-03	1.52E-03	6.46E-04	1.03E-04	1.10E-05	6.28E-03	0.59%
107	KGT70_REF_06_L	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00%	2.13E-03	9.46E-04	4.61E-04	1.23E-04	7.18E-06	3.67E-03	0.35%
							Mercaptan	s and Methanol							
108	KGT50_EMC_01_L	5.77E-03	1.95E-03	7.39E-04	2.37E-04	0.00E+00	8.70E-03	0.97%	5.77E-03	1.95E-03	7.39E-04	2.37E-04	0.00E+00	8.70E-03	0.82%
109	KGT50_EMC_02_L	1.20E-04	2.88E-05	0.00E+00	0.00E+00	4.00E-06	1.53E-04	0.02%	1.20E-04	2.88E-05	0.00E+00	0.00E+00	4.00E-06	1.53E-04	0.01%
110	KGT51_BMC_05_L	1.00E-06	2.40E-07	0.00E+00	0.00E+00	2.00E-06	3.24E-06	0.00%	1.00E-06	2.40E-07	0.00E+00	0.00E+00	2.00E-06	3.24E-06	0.00%
111	KGT52_BMC_01_L	0.00E+00	1.00E-05	5.00E-07	0.00E+00	5.00E-07	1.10E-05	0.00%	0.00E+00	1.00E-05	5.00E-07	0.00E+00	5.00E-07	1.10E-05	0.00%
112	KGT52_BMC_02_L	4.42E-03	1.97E-03	1.01E-03	5.79E-04	0.00E+00	7.98E-03	0.89%	4.42E-03	1.97E-03	1.01E-03	5.79E-04	0.00E+00	7.98E-03	0.75%





No	Node Section		Ва	ase Case/ Sensiti	vity Case 1 Releas	e Frequencies (p	er year)			Sen	sitivity 2 (Future	Production) Rele	ase Frequencies	(per year)	
		1 - 3 mm (2 mm)	3 - 10 mm (6 mm)	10 - 50 mm (22 mm)	50 - 150 mm (85 mm)	> 150 mm (Rupture)	Total	% Contribution	1 - 3 mm (2 mm)	3 - 10 mm (6 mm)	10 - 50 mm (22 mm)	50 - 150 mm (85 mm)	> 150 mm (Rupture)	Total	% Contribution
113	KGT52_BMC_03_L	0.00E+00	2.66E-05	0.00E+00	0.00E+00	2.66E-06	2.93E-05	0.00%	0.00E+00	2.66E-05	0.00E+00	0.00E+00	2.66E-06	2.93E-05	0.00%
113A	KGT52_BMC_04_L	0.00E+00	0.00E+00	0.00E+00	3.80E-11	7.60E-10	7.98E-10	0.00%	0.00E+00	0.00E+00	0.00E+00	3.80E-11	7.60E-10	7.98E-10	0.00%
114	KGT55_MOH_01_L	0.00E+00	4.00E-05	2.00E-06	0.00E+00	2.00E-06	4.40E-05	0.00%	0.00E+00	4.00E-05	2.00E-06	0.00E+00	2.00E-06	4.40E-05	0.00%
115	KGT55_MOH_02_L	9.19E-03	4.12E-03	2.10E-03	1.23E-03	0.00E+00	1.66E-02	1.86%	9.19E-03	4.12E-03	2.10E-03	1.23E-03	0.00E+00	1.66E-02	1.57%
116	KGT55_MOH_03_L	0.00E+00	8.40E-03	0.00E+00	0.00E+00	8.40E-04	9.24E-03	1.03%	0.00E+00	1.20E-02	0.00E+00	0.00E+00	1.20E-03	1.32E-02	1.25%
116A	KGT55_MOH_04_L	0.00E+00	0.00E+00	0.00E+00	1.20E-08	2.40E-07	2.52E-07	0.00%	0.00E+00	0.00E+00	0.00E+00	1.71E-08	3.42E-07	3.59E-07	0.00%
		·	•	•			CO2 Recov	ery - Ammonia	•		•	· · · · ·		•	
117	KGT80_AMM_01_V	8.30E-03	3.77E-03	1.75E-03	3.93E-04	1.18E-04	1.43E-02	1.60%	8.30E-03	3.77E-03	1.75E-03	3.93E-04	1.18E-04	1.43E-02	1.35%
118	KGT80_AMM_11_V	8.46E-03	3.82E-03	1.77E-03	3.88E-04	1.18E-04	1.46E-02	1.62%	8.46E-03	3.82E-03	1.77E-03	3.88E-04	1.18E-04	1.46E-02	1.37%
119	KGT80_AMM_02_V	1.43E-03	6.42E-04	3.24E-04	9.75E-05	0.00E+00	2.49E-03	0.28%	1.43E-03	6.42E-04	3.24E-04	9.75E-05	0.00E+00	2.49E-03	0.24%
120	KGT80_AMM_03_L	1.21E-02	4.42E-03	1.58E-03	4.18E-04	1.44E-06	1.85E-02	2.06%	1.21E-02	4.42E-03	1.58E-03	4.18E-04	1.44E-06	1.85E-02	1.75%
121	KGT80_AMM_04_L	1.83E-02	6.86E-03	2.55E-03	6.83E-04	2.02E-06	2.84E-02	3.17%	1.83E-02	6.86E-03	2.55E-03	6.83E-04	2.02E-06	2.84E-02	2.68%
122	KGT80_AMM_07_L	2.48E-03	1.12E-03	5.45E-04	1.87E-04	0.00E+00	4.32E-03	0.48%	2.48E-03	1.12E-03	5.45E-04	1.87E-04	0.00E+00	4.32E-03	0.41%
123	KGT80_AMM_08_V	3.27E-03	1.40E-03	6.46E-04	1.89E-04	5.75E-06	5.51E-03	0.61%	3.27E-03	1.40E-03	6.46E-04	1.89E-04	5.75E-06	5.51E-03	0.52%
124	KGT80_AMM_09_V	1.64E-02	6.07E-03	2.23E-03	5.41E-04	4.61E-06	2.52E-02	2.81%	1.64E-02	6.07E-03	2.23E-03	5.41E-04	4.61E-06	2.52E-02	2.38%
				•			CO2 Rec	overy - CO2							•
125	KGT90_CO2_01_V	9.50E-03	4.37E-03	2.09E-03	5.57E-04	1.17E-04	1.66E-02	1.86%	9.50E-03	4.37E-03	2.09E-03	5.57E-04	1.17E-04	1.66E-02	1.57%
126	KGT90_CO2_02_V	9.52E-03	4.38E-03	2.10E-03	5.63E-04	1.17E-04	1.67E-02	1.86%	9.52E-03	4.38E-03	2.10E-03	5.63E-04	1.17E-04	1.67E-02	1.57%
127	KGT90_CO2_03_V	3.37E-03	1.60E-03	8.57E-04	3.36E-04	5.05E-06	6.17E-03	0.69%	3.37E-03	1.60E-03	8.57E-04	3.36E-04	5.05E-06	6.17E-03	0.58%
128	KGT90_CO2_07_V	4.78E-03	2.05E-03	9.86E-04	2.35E-04	1.37E-05	8.06E-03	0.90%	4.78E-03	2.05E-03	9.86E-04	2.35E-04	1.37E-05	8.06E-03	0.76%
129	KGT90_CO2_08_L	8.75E-03	3.25E-03	1.37E-03	3.95E-04	9.24E-06	1.38E-02	1.54%	8.75E-03	3.25E-03	1.37E-03	3.95E-04	9.24E-06	1.38E-02	1.30%
130	KGT90_CO2_16_V	2.50E-02	1.02E-02	4.48E-03	8.92E-04	1.99E-04	4.08E-02	4.55%	2.50E-02	1.02E-02	4.48E-03	8.92E-04	1.99E-04	4.08E-02	3.85%
131	KGT90_CO2_18_V	1.63E-03	7.45E-04	3.80E-04	1.36E-04	0.00E+00	2.89E-03	0.32%	1.63E-03	7.45E-04	3.80E-04	1.36E-04	0.00E+00	2.89E-03	0.27%
132	KGT90_CO2_19_V	6.14E-03	2.55E-03	1.23E-03	2.56E-04	1.79E-06	1.02E-02	1.13%	6.14E-03	2.55E-03	1.23E-03	2.56E-04	1.79E-06	1.02E-02	0.96%
133	KGT90_CO2_23_V	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00%	8.01E-04	3.82E-04	2.04E-04	4.31E-05	1.78E-05	1.45E-03	0.14%
134	KGT90_CO2_09_L	0.00E+00	1.00E-05	5.00E-07	0.00E+00	5.00E-07	1.10E-05	0.00%	0.00E+00	1.00E-05	5.00E-07	0.00E+00	5.00E-07	1.10E-05	0.00%
135	KGT90_CO2_10_L	0.00E+00	1.00E-05	5.00E-07	0.00E+00	5.00E-07	1.10E-05	0.00%	0.00E+00	1.00E-05	5.00E-07	0.00E+00	5.00E-07	1.10E-05	0.00%
136	KGT90_CO2_11_L	0.00E+00	1.00E-05	5.00E-07	0.00E+00	5.00E-07	1.10E-05	0.00%	0.00E+00	1.00E-05	5.00E-07	0.00E+00	5.00E-07	1.10E-05	0.00%
137	KGT90_CO2_12_L	0.00E+00	1.00E-05	5.00E-07	0.00E+00	5.00E-07	1.10E-05	0.00%	0.00E+00	1.00E-05	5.00E-07	0.00E+00	5.00E-07	1.10E-05	0.00%
138	KGT90_CO2_24_L	6.53E-03	2.19E-03	7.77E-04	1.78E-04	1.13E-05	9.69E-03	1.08%	6.53E-03	2.19E-03	7.77E-04	1.78E-04	1.13E-05	9.69E-03	0.91%
139	KGT90_CO2_25_L	2.85E-03	1.35E-03	7.40E-04	5.17E-04	0.00E+00	5.45E-03	0.61%	2.85E-03	1.35E-03	7.40E-04	5.17E-04	0.00E+00	5.45E-03	0.51%
140	KGT90_CO2_26_V	8.01E-04	3.57E-04	1.74E-04	6.00E-05	0.00E+00	1.39E-03	0.16%	8.01E-04	3.57E-04	1.74E-04	6.00E-05	0.00E+00	1.39E-03	0.13%





No	Node Section		Ва	se Case/ Sensitiv	vity Case 1 Releas	e Frequencies (p	er year)			Sen	sitivity 2 (Future	Production) Rele	ase Frequencies	(per year)	
		1 - 3 mm (2 mm)	3 - 10 mm (6 mm)	10 - 50 mm (22 mm)	50 - 150 mm (85 mm)	> 150 mm (Rupture)	Total	% Contribution	1 - 3 mm (2 mm)	3 - 10 mm (6 mm)	10 - 50 mm (22 mm)	50 - 150 mm (85 mm)	> 150 mm (Rupture)	Total	% Contribution
141	KGT90_CO2_27_V	8.77E-04	3.78E-04	1.72E-04	5.31E-05	0.00E+00	1.48E-03	0.17%	8.77E-04	3.78E-04	1.72E-04	5.31E-05	0.00E+00	1.48E-03	0.14%
142	KGT90_CO2_28_L	0.00E+00	6.00E-03	0.00E+00	0.00E+00	6.00E-04	6.60E-03	0.74%	0.00E+00	6.00E-03	0.00E+00	0.00E+00	6.00E-04	6.60E-03	0.62%
143	KGT90_CO2_29_V	0.00E+00	2.40E-02	0.00E+00	0.00E+00	2.40E-03	2.64E-02	2.94%	0.00E+00	2.40E-02	0.00E+00	0.00E+00	2.40E-03	2.64E-02	2.49%
144	KGT90_CO2_30_L	0.00E+00	2.40E-02	0.00E+00	0.00E+00	2.40E-03	2.64E-02	2.94%	0.00E+00	2.40E-02	0.00E+00	0.00E+00	2.40E-03	2.64E-02	2.49%
145	KGT90_CO2_31_V	0.00E+00	4.60E-03	0.00E+00	0.00E+00	4.60E-04	5.06E-03	0.56%	0.00E+00	4.60E-03	0.00E+00	0.00E+00	4.60E-04	5.06E-03	0.48%
146	KGT90_CO2_32_L	0.00E+00	4.60E-03	0.00E+00	0.00E+00	4.60E-04	5.06E-03	0.56%	0.00E+00	4.60E-03	0.00E+00	0.00E+00	4.60E-04	5.06E-03	0.48%
147	KGT90_CO2_33_L	0.00E+00	0.00E+00	0.00E+00	8.56E-09	8.56E-09	1.71E-08	0.00%	0.00E+00	0.00E+00	0.00E+00	8.56E-09	8.56E-09	1.71E-08	0.00%
148	KGT90_CO2_34_L	0.00E+00	0.00E+00	0.00E+00	3.42E-08	3.42E-08	6.84E-08	0.00%	0.00E+00	0.00E+00	0.00E+00	3.42E-08	3.42E-08	6.84E-08	0.00%
149	KGT90_CO2_35_L	0.00E+00	0.00E+00	0.00E+00	6.56E-09	6.56E-09	1.31E-08	0.00%	0.00E+00	0.00E+00	0.00E+00	6.56E-09	6.56E-09	1.31E-08	0.00%
	Total	4.53E-01	3.19E-01	8.79E-02	2.14E-02	1.51E-02	8.97E-01	100%	5.31E-01	3.80E-01	1.05E-01	2.52E-02	1.81E-02	1.06E+00	100%
	% Contribution	50.5%	35.6%	9.8%	2.4%	1.7%	100%		50.2%	35.9%	9.9%	2.4%	1.7%	100%	







Appendix 5. Ignited Event and Toxic Event Frequencies





# Table A5- 1: Ignited and Toxic Event Frequencies

				Bas	se Case/ Sensitivity C	ase 1	Ser	nsitivity 2 (Future Oper	ation)
Line No.	Release Scenario	Release Rate (kg/s)	Explosion Probability	Immediate Ignition Event Frequency	Delayed Ignition Event Frequency	Unignited Event Frequency <sup>Note 1</sup>	Immediate Ignition Event Frequency	Delayed Ignition Event Frequency	Unignited Event Frequency <sup>Note 1</sup>
1	KGT01_RGS_01_V_2mm	0.03	0.04	1.82E-06	4.24E-06	6.05E-03	1.82E-06	4.24E-06	6.05E-03
2	KGT01_RGS_01_V_6mm	0.2	0.04	1.21E-06	2.83E-06	2.72E-03	1.21E-06	2.83E-06	2.72E-03
3	KGT01_RGS_01_V_22mm	3.1	0.12	3.56E-06	8.32E-06	1.51E-03	3.56E-06	8.32E-06	1.51E-03
4	KGT01_RGS_01_V_85mm	47	0.12	9.88E-06	2.30E-05	2.49E-04	9.88E-06	2.30E-05	2.49E-04
5	KGT01_RGS_01_V_274mm	485	0.3	1.10E-05	2.57E-05	1.98E-05	1.10E-05	2.57E-05	1.98E-05
6	KGT01_RCS_01_L_2mm	0.1	0.04	4.70E-07	1.10E-06	1.31E-03	4.70E-07	1.10E-06	1.31E-03
7	KGT01_RCS_01_L_6mm	1.1	0.12	5.04E-07	1.18E-06	5.99E-04	5.04E-07	1.18E-06	5.99E-04
8	KGT01_RCS_01_L_22mm	15	0.12	2.29E-06	5.34E-06	2.99E-04	2.29E-06	5.34E-06	2.99E-04
9	KGT01_RCS_01_L_71mm	160	0.3	4.14E-06	9.66E-06	9.23E-05	4.14E-06	9.66E-06	9.23E-05
10	KGT01_MAU_01_V_2mm	0.02	0.04	1.24E-06	2.88E-06	4.11E-03	1.24E-06	2.88E-06	4.11E-03
11	KGT01_MAU_01_V_6mm	0.2	0.04	7.98E-07	1.86E-06	1.83E-03	7.98E-07	1.86E-06	1.83E-03
12	KGT01_MAU_01_V_22mm	2.9	0.12	2.25E-06	5.24E-06	1.01E-03	2.25E-06	5.24E-06	1.01E-03
13	KGT01_MAU_01_V_85mm	44	0.12	4.57E-06	1.07E-05	1.23E-04	4.57E-06	1.07E-05	1.23E-04
14	KGT01_MAU_01_V_274mm	456	0.3	6.85E-06	1.60E-05	1.23E-05	6.85E-06	1.60E-05	1.23E-05
15	KGT01_MAU_02_V_2mm	0.02	0.04	1.06E-06	2.48E-06	3.54E-03	1.06E-06	2.48E-06	3.54E-03
16	KGT01_MAU_02_V_6mm	0.2	0.04	6.24E-07	1.46E-06	1.43E-03	6.24E-07	1.46E-06	1.43E-03
17	KGT01_MAU_02_V_22mm	2.9	0.12	1.45E-06	3.38E-06	6.52E-04	1.45E-06	3.38E-06	6.52E-04
18	KGT01_MAU_02_V_71mm	31	0.12	2.11E-06	4.93E-06	8.49E-05	2.11E-06	4.93E-06	8.49E-05
19	KGT02_TGS_01_V_2mm	0.02	0.04	9.28E-07	2.17E-06	3.09E-03	9.28E-07	2.17E-06	3.09E-03
20	KGT02_TGS_01_V_6mm	0.2	0.04	6.00E-07	1.40E-06	1.42E-03	6.00E-07	1.40E-06	1.42E-03
21	KGT02_TGS_01_V_22mm	2.7	0.12	1.58E-06	3.68E-06	7.80E-04	1.58E-06	3.68E-06	7.80E-04
22	KGT02_TGS_01_V_85mm	40	0.12	5.90E-06	1.38E-05	1.77E-04	5.90E-06	1.38E-05	1.77E-04
23	KGT02_TGS_01_V_212mm	249	0.3	2.73E-06	6.36E-06	5.52E-06	2.73E-06	6.36E-06	5.52E-06
24	KGT03_TGS_04_V_2mm	0.02	0.04	9.09E-07	2.12E-06	3.03E-03	9.09E-07	2.12E-06	3.03E-03
25	KGT03_TGS_04_V_6mm	0.2	0.04	5.90E-07	1.38E-06	1.40E-03	5.90E-07	1.38E-06	1.40E-03
26	KGT03_TGS_04_V_22mm	2.7	0.12	1.55E-06	3.63E-06	7.68E-04	1.55E-06	3.63E-06	7.68E-04
27	KGT03_TGS_04_V_85mm	40	0.12	5.60E-06	1.31E-05	1.68E-04	5.60E-06	1.31E-05	1.68E-04
28	KGT03_TGS_04_V_194mm	208	0.3	3.29E-06	7.68E-06	1.01E-05	3.29E-06	7.68E-06	1.01E-05
29	KGT05_RGS_07_V_2mm	0.03	0.04	0.00E+00	0.00E+00	0.00E+00	7.51E-07	1.75E-06	2.50E-03
30	KGT05_RGS_07_V_6mm	0.2	0.04	0.00E+00	0.00E+00	0.00E+00	5.04E-07	1.18E-06	1.13E-03
31	KGT05_RGS_07_V_22mm	3.1	0.12	0.00E+00	0.00E+00	0.00E+00	1.41E-06	3.30E-06	5.98E-04
32	KGT05_RGS_07_V_85mm	47	0.12	0.00E+00	0.00E+00	0.00E+00	3.21E-06	7.49E-06	8.10E-05
33	KGT05_RGS_07_V_212mm	290	0.3	0.00E+00	0.00E+00	0.00E+00	6.26E-06	1.46E-05	1.12E-05
34	KGT05_TGS_16_V_2mm	0.02	0.04	0.00E+00	0.00E+00	0.00E+00	1.24E-06	2.90E-06	4.14E-03
35	KGT05_TGS_16_V_6mm	0.2	0.04	0.00E+00	0.00E+00	0.00E+00	7.87E-07	1.84E-06	1.86E-03
36	KGT05_TGS_16_V_22mm	2.7	0.12	0.00E+00	0.00E+00	0.00E+00	2.09E-06	4.87E-06	1.03E-03
37	KGT05_TGS_16_V_85mm	40	0.12	0.00E+00	0.00E+00	0.00E+00	4.04E-06	9.43E-06	1.21E-04
38	KGT05_TGS_16_V_212mm	249	0.3	0.00E+00	0.00E+00	0.00E+00	9.16E-06	2.14E-05	1.85E-05
39	KGT01_TGS_07_V_2mm	0.02	0.04	1.45E-06	3.39E-06	4.83E-03	1.45E-06	3.39E-06	4.83E-03
40	KGT01_TGS_07_V_6mm	0.2	0.04	9.03E-07	2.11E-06	2.14E-03	9.03E-07	2.11E-06	2.14E-03
41	KGT01_TGS_07_V_22mm	2.7	0.12	2.36E-06	5.51E-06	1.17E-03	2.36E-06	5.51E-06	1.17E-03
42	KGT01_TGS_07_V_85mm	40	0.12	4.64E-06	1.08E-05	1.39E-04	4.64E-06	1.08E-05	1.39E-04
43	KGT01_TGS_07_V_212mm	249	0.3	5.66E-06	1.32E-05	1.15E-05	5.66E-06	1.32E-05	1.15E-05
44	KGT01_TGS_10_V_2mm	0.02	0.04	1.01E-06	2.36E-06	3.37E-03	1.01E-06	2.36E-06	3.37E-03
45	KGT01_TGS_10_V_6mm	0.2	0.04	6.95E-07	1.62E-06	1.65E-03	6.95E-07	1.62E-06	1.65E-03
46	KGT01_TGS_10_V_22mm	2.7	0.12	1.95E-06	4.56E-06	9.66E-04	1.95E-06	4.56E-06	9.66E-04
47	KGT01_TGS_10_V_85mm	40	0.12	5.63E-06	1.31E-05	1.69E-04	5.63E-06	1.31E-05	1.69E-04
48	KGT01_TGS_10_V_212mm	249	0.3	1.93E-05	4.50E-05	3.91E-05	1.93E-05	4.50E-05	3.91E-05
49	KGT01 TGS 12 V 2mm	0.02	0.04	6.57E-07	1.53E-06	2.19E-03	6.57E-07	1.53E-06	2.19E-03

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		Release		Ва	se Case/ Sensitivity C	ase 1	Sensitivity 2 (Future Ope		ation)
Line No.	Release Scenario	Rate (kg/s)	Explosion Probability	Immediate Ignition Event Frequency	Delayed Ignition Event Frequency	Unignited Event Frequency <sup>Note 1</sup>	Immediate Ignition Event Frequency	Delayed Ignition Event Frequency	Unignited Event Frequency <sup>Note 1</sup>
50	KGT01_TGS_12_V_6mm	0.2	0.04	4.35E-07	1.02E-06	1.03E-03	4.35E-07	1.02E-06	1.03E-03
51	KGT01_TGS_12_V_22mm	2.7	0.12	1.18E-06	2.76E-06	5.85E-04	1.18E-06	2.76E-06	5.85E-04
52	KGT01_TGS_12_V_85mm	40	0.12	2.99E-06	6.97E-06	8.96E-05	2.99E-06	6.97E-06	8.96E-05
53	KGT01_TGS_12_V_173mm	166	0.3	5.60E-06	1.31E-05	2.64E-05	5.60E-06	1.31E-05	2.64E-05
54	KGT01_PGS_02_V_2mm	0.02	0.04	1.09E-06	2.54E-06	3.63E-03	1.09E-06	2.54E-06	3.63E-03
55	KGT01_PGS_02_V_6mm	0.2	0.04	7.03E-07	1.64E-06	1.68E-03	7.03E-07	1.64E-06	1.68E-03
56	KGT01_PGS_02_V_22mm	2.6	0.12	1.71E-06	3.98E-06	8.62E-04	1.71E-06	3.98E-06	8.62E-04
57	KGT01_PGS_02_V_85mm	39	0.12	4.88E-06	1.14E-05	1.50E-04	4.88E-06	1.14E-05	1.50E-04
58	KGT01_PGS_02_V_173mm	162	0.3	6.87E-06	1.60E-05	3.36E-05	6.87E-06	1.60E-05	3.36E-05
59	KGT04_PGS_07_V_2mm	0.02	0.04	3.74E-07	8.73E-07	1.25E-03	3.74E-07	8.73E-07	1.25E-03
60	KGT04_PGS_07_V_6mm	0.2	0.04	2.28E-07	5.32E-07	5.44E-04	2.28E-07	5.32E-07	5.44E-04
61	KGT04_PGS_07_V_22mm	2.6	0.12	5.54E-07	1.29E-06	2.80E-04	5.54E-07	1.29E-06	2.80E-04
62	KGT04_PGS_07_V_63mm	22	0.12	7.95E-07	1.85E-06	4.66E-05	7.95E-07	1.85E-06	4.66E-05
63	KGT01_MPG_01_L_2mm	0.1	0.04	4.25E-07	9.92E-07	1.32E-03	4.25E-07	9.92E-07	1.32E-03
64	KGT01_MPG_01_L_6mm	0.8	0.04	4.15E-07	9.68E-07	5.87E-04	4.15E-07	9.68E-07	5.87E-04
65	KGT01_MPG_01_L_22mm	11	0.12	1.78E-06	4.15E-06	3.02E-04	1.78E-06	4.15E-06	3.02E-04
66	KGT01_MPG_01_L_63mm	93	0.3	2.39E-06	5.58E-06	6.27E-05	2.39E-06	5.58E-06	6.27E-05
67	KGT04_MPG_03_L_2mm	0.1	0.04	5.41E-07	1.26E-06	1.68E-03	5.41E-07	1.26E-06	1.68E-03
68	KGT04_MPG_03_L_6mm	0.8	0.04	5.46E-07	1.27E-06	7.72E-04	5.46E-07	1.27E-06	7.72E-04
69	KGT04_MPG_03_L_22mm	11	0.12	2.24E-06	5.23E-06	3.80E-04	2.24E-06	5.23E-06	3.80E-04
70	KGT04_MPG_03_L_71mm	118	0.3	5.39E-06	1.26E-05	1.20E-04	5.39E-06	1.26E-05	1.20E-04
71	KGT04_MPG_04_L_2mm	0.1	0.04	6.03E-07	1.41E-06	1.87E-03	6.03E-07	1.41E-06	1.87E-03
72	KGT04_MPG_04_L_6mm	0.8	0.04	5.23E-07	1.22E-06	7.39E-04	5.23E-07	1.22E-06	7.39E-04
73	KGT04_MPG_04_L_22mm	11	0.12	1.79E-06	4.18E-06	3.04E-04	1.79E-06	4.18E-06	3.04E-04
74	KGT04_MPG_04_L_85mm	169	0.3	2.95E-06	6.87E-06	6.57E-05	2.95E-06	6.87E-06	6.57E-05
75	KGT04_MPG_04_L_150mm	527	0.3	8.31E-08	1.94E-07	1.85E-06	8.31E-08	1.94E-07	1.85E-06
76	KGT04_MPG_05_L_2mm	0.1	0.04	1.01E-06	2.36E-06	3.13E-03	1.01E-06	2.36E-06	3.13E-03
77	KGT04_MPG_05_L_6mm	0.8	0.04	5.84E-07	1.36E-06	8.26E-04	5.84E-07	1.36E-06	8.26E-04
78	KGT04_MPG_05_L_22mm	4.3	0.12	6.11E-07	1.43E-06	2.37E-04	6.11E-07	1.43E-06	2.37E-04
79	KGT04_MPG_05_L_71mm	4.3	0.12	8.54E-08	1.99E-07	3.31E-05	8.54E-08	1.99E-07	3.31E-05
80	KGT04_MPG_06_L_2mm	0.1	0.04	7.52E-07	1.75E-06	2.33E-03	7.52E-07	1.75E-06	2.33E-03
81	KGT04_MPG_06_L_6mm	0.8	0.04	7.23E-07	1.69E-06	1.02E-03	7.23E-07	1.69E-06	1.02E-03
82	KGT04_MPG_06_L_22mm	11	0.12	3.07E-06	7.16E-06	5.22E-04	3.07E-06	7.16E-06	5.22E-04
83	KGT04_MPG_06_L_71mm	118	0.3	4.08E-06	9.52E-06	9.10E-05	4.08E-06	9.52E-06	9.10E-05
84	KGT01_TGS_11_V_2mm	0.02	0.04	0.00E+00	0.00E+00	0.00E+00	7.56E-07	1.76E-06	2.52E-03
85	KGT01_TGS_11_V_6mm	0.2	0.04	0.00E+00	0.00E+00	0.00E+00	5.42E-07	1.27E-06	1.28E-03
86	KGT01_TGS_11_V_22mm	2.7	0.12	0.00E+00	0.00E+00	0.00E+00	1.55E-06	3.62E-06	7.66E-04
87	KGT01_TGS_11_V_85mm	40	0.12	0.00E+00	0.00E+00	0.00E+00	1.07E-05	2.50E-05	3.21E-04
88	KGT01_TGS_11_V_173mm	166	0.3	0.00E+00	0.00E+00	0.00E+00	1.27E-06	2.95E-06	5.97E-06
89	KGT01_PGS_03_V_2mm	0.02	0.04	0.00E+00	0.00E+00	0.00E+00	1.17E-06	2.72E-06	3.88E-03
90	KGT01_PGS_03_V_6mm	0.2	0.04	0.00E+00	0.00E+00	0.00E+00	7.35E-07	1.71E-06	1.75E-03
91	KGT01_PGS_03_V_22mm	2.6	0.12	0.00E+00	0.00E+00	0.00E+00	1.74E-06	4.05E-06	8.77E-04
92	KGT01_PGS_03_V_85mm	39	0.12	0.00E+00	0.00E+00	0.00E+00	7.27E-06	1.70E-05	2.23E-04
93	KGT01_PGS_03_V_150mm	122	0.3	0.00E+00	0.00E+00	0.00E+00	2.90E-07	6.76E-07	2.20E-06
94	KGT01_MPG_02_L_2mm	0.1	0.04	0.00E+00	0.00E+00	0.00E+00	3.27E-07	7.62E-07	1.01E-03
95	KGT01_MPG_02_L_6mm	0.8	0.04	0.00E+00	0.00E+00	0.00E+00	3.13E-07	7.31E-07	4.43E-04
96	KGT01_MPG_02_L_22mm	11	0.12	0.00E+00	0.00E+00	0.00E+00	1.31E-06	3.07E-06	2.23E-04
97	KGT01_MPG_02_L_71mm	118	0.3	0.00E+00	0.00E+00	0.00E+00	1.80E-06	4.20E-06	4.01E-05
98	KGT01_PGS_01_V_2mm	0.02	0.04	1.76E-06	4.11E-06	5.87E-03	1.76E-06	4.11E-06	5.87E-03
	KGT01_PGS_01_V_6mm	0.2	0.04	1.08E-06	2.52E-06	2.58E-03	1.08E-06	2.52E-06	2.58E-03

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		Release		Ва	se Case/ Sensitivity C	ase 1	Ser	nsitivity 2 (Future Oper	ation)
Line No.	Release Scenario	Rate (kg/s)	Explosion Probability	Immediate Ignition Event Frequency	Delayed Ignition Event Frequency	Unignited Event Frequency <sup>Note 1</sup>	Immediate Ignition Event Frequency	Delayed Ignition Event Frequency	Unignited Event Frequency <sup>Note 1</sup>
100	KGT01_PGS_01_V_22mm	2.6	0.12	2.81E-06	6.56E-06	1.43E-03	2.81E-06	6.56E-06	1.43E-03
101	KGT01_PGS_01_V_85mm	39	0.12	5.36E-06	1.25E-05	1.66E-04	5.36E-06	1.25E-05	1.66E-04
102	KGT01_PGS_01_V_245mm	323	0.3	6.95E-06	1.62E-05	1.25E-05	6.95E-06	1.62E-05	1.25E-05
103	KGT01_PGS_13_V_2mm	0.02	0.04	5.50E-07	1.28E-06	1.83E-03	5.50E-07	1.28E-06	1.83E-03
104	KGT01_PGS_13_V_6mm	0.2	0.04	3.33E-07	7.78E-07	7.97E-04	3.33E-07	7.78E-07	7.97E-04
105	KGT01_PGS_13_V_22mm	2.6	0.12	7.78E-07	1.81E-06	3.96E-04	7.78E-07	1.81E-06	3.96E-04
106	KGT01_PGS_13_V_71mm	27	0.12	1.77E-06	4.12E-06	8.11E-05	1.77E-06	4.12E-06	8.11E-05
107	KGT01_PGS_14_V_2mm	0.02	0.04	2.31E-07	5.39E-07	7.69E-04	2.31E-07	5.39E-07	7.69E-04
108	KGT01_PGS_14_V_6mm	0.2	0.04	1.45E-07	3.39E-07	3.48E-04	1.45E-07	3.39E-07	3.48E-04
109	KGT01_PGS_14_V_22mm	2.6	0.12	3.70E-07	8.64E-07	1.88E-04	3.70E-07	8.64E-07	1.88E-04
110	KGT01_PGS_14_V_85mm	39	0.12	7.74E-07	1.80E-06	2.40E-05	7.74E-07	1.80E-06	2.40E-05
111	KGT01_PGS_14_V_173mm	161	0.3	1.23E-06	2.88E-06	6.12E-06	1.23E-06	2.88E-06	6.12E-06
112	KGT13_PGS_15_V_2mm	0.02	0.04	1.11E-06	2.59E-06	3.70E-03	1.11E-06	2.59E-06	3.70E-03
113	KGT13_PGS_15_V_6mm	0.2	0.04	7.03E-07	1.64E-06	1.68E-03	7.03E-07	1.64E-06	1.68E-03
114	KGT13_PGS_15_V_22mm	2.6	0.12	1.72E-06	4.02E-06	8.77E-04	1.72E-06	4.02E-06	8.77E-04
115	KGT13_PGS_15_V_85mm	39	0.12	7.18E-06	1.68E-05	2.23E-04	7.18E-06	1.68E-05	2.23E-04
116	KGT13_PGS_15_V_274mm	404	0.3	1.02E-05	2.38E-05	1.83E-05	1.02E-05	2.38E-05	1.83E-05
117	KGT13_PGS_16_V_2mm	0.02	0.04	2.20E-06	5.14E-06	7.34E-03	2.20E-06	5.14E-06	7.34E-03
117	KGT13_PGS_16_V_6mm	0.02	0.04	1.32E-06	3.08E-06	3.16E-03	1.32E-06	3.08E-06	3.16E-03
119	KGT13_PGS_16_V_22mm	2.6	0.04	2.90E-06	6.77E-06	1.48E-03	2.90E-06	6.77E-06	1.48E-03
		39	0.12						
120	KGT13_PGS_16_V_85mm			1.23E-05	2.88E-05	3.83E-04	1.23E-05	2.88E-05	3.83E-04
121	KGT13_PGS_16_V_150mm	121	0.3	7.58E-07	1.77E-06	5.83E-06	7.58E-07	1.77E-06	5.83E-06
122	KGT13_PGS_17_V_2mm	0.02	0.04	1.16E-06	2.72E-06	3.88E-03	1.16E-06	2.72E-06	3.88E-03
123	KGT13_PGS_17_V_6mm	0.2	0.04	7.51E-07	1.75E-06	1.79E-03	7.51E-07	1.75E-06	1.79E-03
124	KGT13_PGS_17_V_22mm	2.6	0.12	1.97E-06	4.60E-06	1.00E-03	1.97E-06	4.60E-06	1.00E-03
125	KGT13_PGS_17_V_85mm	39	0.12	5.12E-06	1.19E-05	1.59E-04	5.12E-06	1.19E-05	1.59E-04
126	KGT13_PGS_17_V_274mm	404	0.3	1.25E-05	2.93E-05	2.25E-05	1.25E-05	2.93E-05	2.25E-05
127	KGT01_MGS_01_V_2mm	0.02	0.04	4.14E-06	9.66E-06	1.38E-02	4.14E-06	9.66E-06	1.38E-02
128	KGT01_MGS_01_V_6mm	0.2	0.04	2.47E-06	5.76E-06	5.90E-03	2.47E-06	5.76E-06	5.90E-03
129	KGT01_MGS_01_V_22mm	2.6	0.12	5.63E-06	1.31E-05	2.87E-03	5.63E-06	1.31E-05	2.87E-03
130	KGT01_MGS_01_V_85mm	39	0.12	1.61E-05	3.75E-05	4.98E-04	1.61E-05	3.75E-05	4.98E-04
131	KGT01_MGS_01_V_245mm	323	0.3	2.38E-05	5.56E-05	4.28E-05	2.38E-05	5.56E-05	4.28E-05
132	KGT01_MGS_03_V_2mm	0.04	0.04	2.13E-06	4.98E-06	7.11E-03	2.13E-06	4.98E-06	7.11E-03
133	KGT01_MGS_03_V_6mm	0.3	0.04	1.55E-06	3.62E-06	3.07E-03	1.55E-06	3.62E-06	3.07E-03
134	KGT01_MGS_03_V_22mm	4.4	0.12	4.84E-06	1.13E-05	1.45E-03	4.84E-06	1.13E-05	1.45E-03
135	KGT01_MGS_03_V_85mm	66	0.3	1.81E-05	4.23E-05	3.08E-04	1.81E-05	4.23E-05	3.08E-04
136	KGT01_MGS_03_V_173mm	272	0.3	5.22E-06	1.22E-05	9.37E-06	5.22E-06	1.22E-05	9.37E-06
137	KGT01_MGS_07_V_2mm	0.04	0.04	1.63E-06	3.79E-06	5.41E-03	1.63E-06	3.79E-06	5.41E-03
138	KGT01_MGS_07_V_6mm	0.3	0.04	1.16E-06	2.71E-06	2.31E-03	1.16E-06	2.71E-06	2.31E-03
139	KGT01_MGS_07_V_22mm	4.4	0.12	3.46E-06	8.07E-06	1.04E-03	3.46E-06	8.07E-06	1.04E-03
140	KGT01_MGS_07_V_85mm	66	0.3	1.53E-05	3.56E-05	2.60E-04	1.53E-05	3.56E-05	2.60E-04
141	KGT01_MGS_07_V_173mm	272	0.3	2.17E-06	5.07E-06	3.90E-06	2.17E-06	5.07E-06	3.90E-06
142	KGT11_MGS_05_V_2mm	0.04	0.04	6.49E-07	1.52E-06	2.16E-03	6.49E-07	1.52E-06	2.16E-03
143	KGT11_MGS_05_V_6mm	0.3	0.04	5.41E-07	1.26E-06	1.07E-03	5.41E-07	1.26E-06	1.07E-03
144	KGT11_MGS_05_V_22mm	4.4	0.12	2.10E-06	4.90E-06	6.31E-04	2.10E-06	4.90E-06	6.31E-04
145	KGT11_MGS_05_V_85mm	66	0.3	7.26E-06	1.69E-05	1.23E-04	7.26E-06	1.69E-05	1.23E-04
146	KGT11_MGS_05_V_229mm	476	0.3	1.37E-05	3.19E-05	2.45E-05	1.37E-05	3.19E-05	2.45E-05
147	KGT11_MGS_08_V_2mm	0.04	0.04	8.28E-07	1.93E-06	2.76E-03	8.28E-07	1.93E-06	2.76E-03
148	KGT11_MGS_08_V_6mm	0.3	0.04	6.03E-07	1.41E-06	1.20E-03	6.03E-07	1.41E-06	1.20E-03
149	KGT11_MGS_08_V_22mm	4.4	0.12	1.88E-06	4.39E-06	5.64E-04	1.88E-06	4.39E-06	5.64E-04

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				Ba	se Case/ Sensitivity C	ase 1	Sensitivity 2 (Future Ope		ation)
Line No.	Release Scenario	Release Rate (kg/s)	Explosion Probability	Immediate Ignition Event Frequency	Delayed Ignition Event Frequency	Unignited Event Frequency <sup>Note 1</sup>	Immediate Ignition Event Frequency	Delayed Ignition Event Frequency	Unignited Event Frequency <sup>Note 1</sup>
150	KGT11_MGS_08_V_50mm	23	0.12	2.65E-06	6.18E-06	1.47E-04	2.65E-06	6.18E-06	1.47E-04
151	KGT11_MGS_09_V_2mm	0.04	0.04	2.45E-06	5.71E-06	8.15E-03	2.45E-06	5.71E-06	8.15E-03
152	KGT11_MGS_09_V_6mm	0.3	0.04	1.80E-06	4.19E-06	3.57E-03	1.80E-06	4.19E-06	3.57E-03
153	KGT11_MGS_09_V_22mm	4.4	0.12	6.17E-06	1.44E-05	1.85E-03	6.17E-06	1.44E-05	1.85E-03
154	KGT11_MGS_09_V_85mm	66	0.3	1.42E-05	3.32E-05	2.41E-04	1.42E-05	3.32E-05	2.41E-04
155	KGT11_MGS_09_V_229mm	476	0.3	1.14E-05	2.67E-05	2.05E-05	1.14E-05	2.67E-05	2.05E-05
156	KGT01_PIG_01_V_2mm	0.02	0.04	2.86E-10	6.67E-10	9.51E-07	2.86E-10	6.67E-10	9.51E-07
157	KGT01_PIG_01_V_6mm	0.2	0.04	2.12E-10	4.95E-10	4.85E-07	2.12E-10	4.95E-10	4.85E-07
158	KGT01_PIG_01_V_22mm	2.9	0.12	5.95E-10	1.39E-09	2.68E-07	5.95E-10	1.39E-09	2.68E-07
159	KGT01_PIG_01_V_85mm	44	0.12	2.15E-09	5.01E-09	5.80E-08	2.15E-09	5.01E-09	5.80E-08
160	KGT01_PIG_01_V_274mm	456	0.3	5.68E-09	1.32E-08	1.02E-08	5.68E-09	1.32E-08	1.02E-08
161	KGT13_PIG_02_V_2mm	0.02	0.04	2.64E-10	6.16E-10	8.79E-07	2.64E-10	6.16E-10	8.79E-07
162	KGT13_PIG_02_V_6mm	0.2	0.04	1.90E-10	4.44E-10	4.55E-07	1.90E-10	4.44E-10	4.55E-07
163	KGT13_PIG_02_V_22mm	2.6	0.12	4.94E-10	1.15E-09	2.51E-07	4.94E-10	1.15E-09	2.51E-07
164	KGT13_PIG_02_V_85mm	39	0.12	1.90E-09	4.43E-09	5.89E-08	1.90E-09	4.43E-09	5.89E-08
165	KGT13_PIG_02_V_274mm	404	0.3	5.68E-09	1.32E-08	1.02E-08	5.68E-09	1.32E-08	1.02E-08
166	KGT11_PIG_03_V_2mm	0.04	0.04	2.63E-10	6.13E-10	8.75E-07	2.63E-10	6.13E-10	8.75E-07
167	KGT11_PIG_03_V_6mm	0.3	0.04	2.28E-10	5.32E-10	4.52E-07	2.28E-10	5.32E-10	4.52E-07
168	KGT11_PIG_03_V_22mm	4.4	0.12	8.30E-10	1.94E-09	2.49E-07	8.30E-10	1.94E-09	2.49E-07
169	KGT11_PIG_03_V_85mm	66	0.3	3.06E-09	7.15E-09	5.20E-08	3.06E-09	7.15E-09	5.20E-08
109		272	0.3	5.68E-09	1.32E-08	1.02E-08	5.68E-09	1.32E-08	1.02E-08
	KGT11_PIG_03_V_173mm								
171	KGT11_PIG_04_V_2mm	0.04	0.04	2.63E-10	6.13E-10	8.75E-07	2.63E-10	6.13E-10	8.75E-07
172	KGT11_PIG_04_V_6mm	0.3	0.04	2.28E-10	5.32E-10	4.52E-07	2.28E-10	5.32E-10	4.52E-07
173	KGT11_PIG_04_V_22mm	4.4	0.12	8.30E-10	1.94E-09	2.49E-07	8.30E-10	1.94E-09	2.49E-07
174	KGT11_PIG_04_V_85mm	66	0.3	3.06E-09	7.15E-09	5.20E-08	3.06E-09	7.15E-09	5.20E-08
175	KGT11_PIG_04_V_173mm	272	0.3	5.68E-09	1.32E-08	1.02E-08	5.68E-09	1.32E-08	1.02E-08
176	KGT01_MPG_21_V_2mm	0.003	0.04	1.62E-06	3.78E-06	5.39E-03	1.62E-06	3.78E-06	5.39E-03
177	KGT01_MPG_21_V_6mm	0.03	0.04	6.83E-07	1.59E-06	2.27E-03	6.83E-07	1.59E-06	2.27E-03
178	KGT01_MPG_21_V_22mm	0.4	0.04	5.96E-07	1.39E-06	1.08E-03	5.96E-07	1.39E-06	1.08E-03
179	KGT01_MPG_21_V_71mm	4.4	0.12	7.45E-07	1.74E-06	2.25E-04	7.45E-07	1.74E-06	2.25E-04
180	KGT01_MPG_22_L_2mm	0.04	0.04	4.97E-07	1.16E-06	1.65E-03	4.97E-07	1.16E-06	1.65E-03
181	KGT01_MPG_22_L_6mm	0.4	0.04	3.46E-07	8.08E-07	6.52E-04	3.46E-07	8.08E-07	6.52E-04
182	KGT01_MPG_22_L_22mm	5.1	0.12	7.59E-07	1.77E-06	2.55E-04	7.59E-07	1.77E-06	2.55E-04
183	KGT01_MPG_22_L_50mm	26	0.12	9.81E-07	2.29E-06	8.06E-05	9.81E-07	2.29E-06	8.06E-05
184	KGT01_MPG_23_L_2mm	0.1	0.04	4.40E-07	1.03E-06	1.22E-03	4.40E-07	1.03E-06	1.22E-03
185	KGT01_MPG_23_L_6mm	1.1	0.12	4.51E-07	1.05E-06	5.35E-04	4.51E-07	1.05E-06	5.35E-04
186	KGT01_MPG_23_L_22mm	15	0.12	1.89E-06	4.40E-06	2.47E-04	1.89E-06	4.40E-06	2.47E-04
187	KGT01_MPG_23_L_50mm	79	0.3	2.46E-06	5.75E-06	7.48E-05	2.46E-06	5.75E-06	7.48E-05
188	KGT01_FGA_01_V_2mm	0.02	0.04	1.57E-06	3.67E-06	5.24E-03	1.57E-06	3.67E-06	5.24E-03
189	KGT01_FGA_01_V_6mm	0.2	0.04	1.00E-06	2.34E-06	2.40E-03	1.00E-06	2.34E-06	2.40E-03
190	KGT01_FGA_01_V_22mm	2.6	0.12	2.61E-06	6.10E-06	1.33E-03	2.61E-06	6.10E-06	1.33E-03
191	KGT01_FGA_01_V_85mm	39	0.12	1.01E-05	2.36E-05	3.14E-04	1.01E-05	2.36E-05	3.14E-04
192	KGT01_FGA_01_V_150mm	121	0.3	1.30E-06	3.04E-06	1.00E-05	1.30E-06	3.04E-06	1.00E-05
193	KGT01_FGA_02_V_2mm	0.02	0.04	4.53E-06	1.06E-05	1.51E-02	4.53E-06	1.06E-05	1.51E-02
194	KGT01_FGA_02_V_6mm	0.2	0.04	2.65E-06	6.19E-06	6.35E-03	2.65E-06	6.19E-06	6.35E-03
195	KGT01_FGA_02_V_22mm	2.6	0.12	6.09E-06	1.42E-05	3.10E-03	6.09E-06	1.42E-05	3.10E-03
196	KGT01_FGA_02_V_85mm	39	0.12	1.31E-05	3.06E-05	4.06E-04	1.31E-05	3.06E-05	4.06E-04
197	KGT01_FGA_02_V_150mm	121	0.3	3.19E-06	7.45E-06	2.46E-05	3.19E-06	7.45E-06	2.46E-05
198	KGT01_PGS_19_V_2mm	0.02	0.04	2.25E-06	5.25E-06	7.49E-03	2.25E-06	5.25E-06	7.49E-03
⊢	KGT01_PGS_19_V_6mm	0.2	0.04	1.22E-06	2.84E-06	2.91E-03	1.22E-06	2.84E-06	2.91E-03

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Line No. 200 201	Release Scenario	Release Rate	Evalacian	Base Case/ Sensitivity Case 1				Sensitivity 2 (Future Operation)			
		(kg/s)	Explosion Probability	Immediate Ignition Event Frequency	Delayed Ignition Event Frequency	Unignited Event Frequency <sup>Note 1</sup>	Immediate Ignition Event Frequency	Delayed Ignition Event Frequency	Unignited Event Frequency <sup>Note 1</sup>		
201	KGT01_PGS_19_V_22mm	2.6	0.12	2.24E-06	5.23E-06	1.14E-03	2.24E-06	5.23E-06	1.14E-03		
	KGT01_PGS_19_V_50mm	13	0.12	2.81E-06	6.56E-06	2.69E-04	2.81E-06	6.56E-06	2.69E-04		
202	KGT01_PGS_21_V_2mm	0.02	0.04	3.62E-06	8.45E-06	1.21E-02	3.62E-06	8.45E-06	1.21E-02		
203	KGT01_PGS_21_V_6mm	0.2	0.04	1.91E-06	4.47E-06	4.58E-03	1.91E-06	4.47E-06	4.58E-03		
204	KGT01_PGS_21_V_22mm	2.6	0.12	3.38E-06	7.89E-06	1.72E-03	3.38E-06	7.89E-06	1.72E-03		
205	KGT01_PGS_21_V_71mm	27	0.12	8.27E-06	1.93E-05	3.79E-04	8.27E-06	1.93E-05	3.79E-04		
206	KGT01_PGS_22_V_2mm	0.02	0.04	0.00E+00	0.00E+00	0.00E+00	1.46E-06	3.41E-06	4.86E-03		
207	KGT01_PGS_22_V_6mm	0.2	0.04	0.00E+00	0.00E+00	0.00E+00	8.81E-07	2.06E-06	2.11E-03		
208	KGT01_PGS_22_V_22mm	2.6	0.12	0.00E+00	0.00E+00	0.00E+00	2.05E-06	4.79E-06	1.04E-03		
209	KGT01_PGS_22_V_85mm	39	0.12	0.00E+00	0.00E+00	0.00E+00	5.15E-06	1.20E-05	1.60E-04		
210	KGT01_PGS_22_V_150mm	121	0.3	0.00E+00	0.00E+00	0.00E+00	2.22E-06	5.19E-06	1.71E-05		
211	KGT01_MPG_07_L_2mm	0.1	0.04	5.60E-07	1.31E-06	1.83E-03	5.60E-07	1.31E-06	1.83E-03		
212	KGT01_MPG_07_L_6mm	0.7	0.04	5.71E-07	1.33E-06	8.52E-04	5.71E-07	1.33E-06	8.52E-04		
213	KGT01_MPG_07_L_22mm	10	0.12	2.39E-06	5.57E-06	4.62E-04	2.39E-06	5.57E-06	4.62E-04		
214	KGT01_MPG_07_L_71mm	101	0.3	5.89E-06	1.37E-05	1.42E-04	5.89E-06	1.37E-05	1.42E-04		
215	KGT01_DET_01_V_2mm	0.02	0.04	7.52E-07	1.75E-06	2.50E-03	7.52E-07	1.75E-06	2.50E-03		
216	KGT01_DET_01_V_6mm	0.1	0.04	4.36E-07	1.02E-06	1.16E-03	4.36E-07	1.02E-06	1.16E-03		
217	KGT01_DET_01_V_22mm	1.9	0.12	9.09E-07	2.12E-06	6.30E-04	9.09E-07	2.12E-06	6.30E-04		
218	KGT01_DET_01_V_71mm	20	0.12	3.20E-06	7.48E-06	2.04E-04	3.20E-06	7.48E-06	2.04E-04		
219	KGT01_PGS_04_V_2mm	0.02	0.04	5.82E-07	1.36E-06	1.94E-03	5.82E-07	1.36E-06	1.94E-03		
220	KGT01_PGS_04_V_6mm	0.1	0.04	3.32E-07	7.74E-07	8.85E-04	3.32E-07	7.74E-07	8.85E-04		
221	KGT01_PGS_04_V_22mm	1.9	0.12	6.78E-07	1.58E-06	4.70E-04	6.78E-07	1.58E-06	4.70E-04		
222	KGT01_PGS_04_V_63mm	16	0.12	1.51E-06	3.53E-06	1.24E-04	1.51E-06	3.53E-06	1.24E-04		
223	KGT01_PGS_05_V_2mm	0.02	0.04	3.12E-06	7.29E-06	1.04E-02	3.12E-06	7.29E-06	1.04E-02		
224	KGT01_PGS_05_V_6mm	0.1	0.04	1.73E-06	4.03E-06	4.61E-03	1.73E-06	4.03E-06	4.61E-03		
225	KGT01_PGS_05_V_22mm	1.9	0.12	3.09E-06	7.21E-06	2.14E-03	3.09E-06	7.21E-06	2.14E-03		
226	KGT01_PGS_05_V_85mm	29	0.12	1.51E-05	3.52E-05	6.54E-04	1.51E-05	3.52E-05	6.54E-04		
227	KGT01_PGS_05_V_173mm	118	0.3	7.74E-07	1.81E-06	6.14E-06	7.74E-07	1.81E-06	6.14E-06		
228	KGT01_DEX_01_L_2mm	0.1	0.04	1.74E-06	4.07E-06	5.37E-03	1.74E-06	4.07E-06	5.37E-03		
229	KGT01_DEX_01_L_6mm	0.9	0.04	1.24E-06	2.90E-06	1.74E-03	1.24E-06	2.90E-06	1.74E-03		
230	KGT01_DEX_01_L_22mm	0.9	0.04	4.62E-07	1.08E-06	6.45E-04	4.62E-07	1.08E-06	6.45E-04		
231	KGT01_DEX_01_L_63mm	0.9	0.04	1.05E-07	2.44E-07	1.46E-04	1.05E-07	2.44E-07	1.46E-04		
232	KGT01_DEB_01_L_2mm	0.1	0.04	9.52E-07	2.22E-06	2.93E-03	9.52E-07	2.22E-06	2.93E-03		
233	KGT01_DEB_01_L_6mm	0.9	0.04	9.36E-07	2.18E-06	1.31E-03	9.36E-07	2.18E-06	1.31E-03		
234	KGT01_DEB_01_L_22mm	12	0.12	4.02E-06	9.38E-06	6.72E-04	4.02E-06	9.38E-06	6.72E-04		
235	KGT01_DEB_01_L_85mm	172	0.3	6.37E-06	1.49E-05	1.42E-04	6.37E-06	1.49E-05	1.42E-04		
236	KGT01_DEB_01_L_150mm	537	0.3	1.37E-07	3.20E-07	3.06E-06	1.37E-07	3.20E-07	3.06E-06		
237	KGT01_MPG_09_L_2mm	0.1	0.04	8.30E-07	1.94E-06	2.55E-03	8.30E-07	1.94E-06	2.55E-03		
238	KGT01_MPG_09_L_6mm	0.9	0.04	8.05E-07	1.88E-06	1.13E-03	8.05E-07	1.88E-06	1.13E-03		
239	KGT01_MPG_09_L_22mm	12	0.12	3.63E-06	8.47E-06	6.07E-04	3.63E-06	8.47E-06	6.07E-04		
240	KGT01_MPG_09_L_85mm	172	0.3	3.47E-06	8.09E-06	7.73E-05	3.47E-06	8.09E-06	7.73E-05		
241	KGT01_MPG_09_L_150mm	537	0.3	3.79E-07	8.84E-07	8.45E-06	3.79E-07	8.84E-07	8.45E-06		
242	KGT01_MPG_10_V_2mm	0.03	0.04	4.01E-07	9.35E-07	1.33E-03	4.01E-07	9.35E-07	1.33E-03		
243	KGT01_MPG_10_V_6mm	0.2	0.04	2.71E-07	6.32E-07	5.94E-04	2.71E-07	6.32E-07	5.94E-04		
244	KGT01_MPG_10_V_22mm	3.3	0.12	7.60E-07	1.77E-06	3.03E-04	7.60E-07	1.77E-06	3.03E-04		
245	KGT01_MPG_10_V_71mm	35	0.12	1.94E-06	4.53E-06	6.86E-05	1.94E-06	4.53E-06	6.86E-05		
246	KGT01_MPG_13_L_2mm	0.1	0.04	0.00E+00	0.00E+00	0.00E+00	2.59E-07	6.04E-07	8.46E-04		
247	KGT01_MPG_13_L_6mm	0.7	0.04	0.00E+00	0.00E+00	0.00E+00	2.43E-07	5.67E-07	3.62E-04		
248	KGT01_MPG_13_L_22mm	10	0.12	0.00E+00	0.00E+00	0.00E+00	9.13E-07	2.13E-06	1.77E-04		
249	KGT01_MPG_13_L_85mm	145	0.3	0.00E+00	0.00E+00	0.00E+00	1.24E-06	2.90E-06	2.77E-05		

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		Poloaco	Base Case/ Sensitivity Case 1				Sensitivity 2 (Future Operation)			
Line No.	Release Scenario	Release Rate (kg/s)	Explosion Probability	Immediate Ignition Event Frequency	Delayed Ignition Event Frequency	Unignited Event Frequency <sup>Note 1</sup>	Immediate Ignition Event Frequency	Delayed Ignition Event Frequency	Unignited Event Frequency <sup>Note 1</sup>	
250	KGT01_MPG_13_L_150mm	453	0.3	0.00E+00	0.00E+00	0.00E+00	8.09E-08	1.89E-07	1.80E-06	
251	KGT01_STT_01_V_2mm	0.02	0.04	0.00E+00	0.00E+00	0.00E+00	1.05E-06	2.44E-06	3.48E-03	
252	KGT01_STT_01_V_6mm	0.1	0.04	0.00E+00	0.00E+00	0.00E+00	5.67E-07	1.32E-06	1.51E-03	
253	KGT01_STT_01_V_22mm	1.9	0.12	0.00E+00	0.00E+00	0.00E+00	1.15E-06	2.69E-06	8.00E-04	
254	KGT01_STT_01_V_63mm	16	0.12	0.00E+00	0.00E+00	0.00E+00	1.31E-06	3.05E-06	1.07E-04	
255	KGT01_PGS_10_V_2mm	0.02	0.04	0.00E+00	0.00E+00	0.00E+00	1.04E-06	2.42E-06	3.46E-03	
256	KGT01_PGS_10_V_6mm	0.1	0.04	0.00E+00	0.00E+00	0.00E+00	5.70E-07	1.33E-06	1.52E-03	
257	KGT01_PGS_10_V_22mm	1.9	0.12	0.00E+00	0.00E+00	0.00E+00	1.12E-06	2.62E-06	7.78E-04	
258	KGT01_PGS_10_V_71mm	20	0.12	0.00E+00	0.00E+00	0.00E+00	2.51E-06	5.85E-06	1.59E-04	
259	KGT01_PGS_11_V_2mm	0.02	0.04	0.00E+00	0.00E+00	0.00E+00	2.78E-06	6.48E-06	9.25E-03	
260	KGT01_PGS_11_V_6mm	0.1	0.04	0.00E+00	0.00E+00	0.00E+00	1.54E-06	3.60E-06	4.12E-03	
261	KGT01_PGS_11_V_22mm	1.9	0.12	0.00E+00	0.00E+00	0.00E+00	2.71E-06	6.32E-06	1.88E-03	
262	KGT01_PGS_11_V_71mm	20	0.12	0.00E+00	0.00E+00	0.00E+00	1.03E-05	2.40E-05	6.55E-04	
263	KGT01_STB_01_L_2mm	0.1	0.04	0.00E+00	0.00E+00	0.00E+00	1.30E-06	3.02E-06	3.99E-03	
264	KGT01_STB_01_L_6mm	0.9	0.04	0.00E+00	0.00E+00	0.00E+00	1.24E-06	2.90E-06	1.75E-03	
265	KGT01_STB_01_L_22mm	12	0.12	0.00E+00	0.00E+00	0.00E+00	5.38E-06	1.26E-05	8.99E-04	
265	KGT01_STB_01_L_85mm	172	0.12	0.00E+00	0.00E+00	0.00E+00	6.16E-06	1.44E-05	1.37E-04	
267	KGT01_STB_01_L_150mm	537	0.3	0.00E+00	0.00E+00	0.00E+00	5.62E-08	1.31E-07	1.25E-06	
268	KGT01_DPT_11_V_2mm	0.01	0.04	9.19E-07	2.14E-06	3.06E-03	9.19E-07	2.14E-06	3.06E-03	
269	KGT01_DPT_11_V_6mm	0.1	0.04	4.29E-07	1.00E-06	1.27E-03	4.29E-07	1.00E-06	1.27E-03	
270	KGT01_DPT_11_V_22mm	1.4	0.12	6.55E-07	1.53E-06	6.10E-04	6.55E-07	1.53E-06	6.10E-04	
271	KGT01_DPT_11_V_85mm	21	0.12	2.00E-06	4.68E-06	1.19E-04	2.00E-06	4.68E-06	1.19E-04	
272	KGT01_DPT_11_V_150mm	66	0.3	3.29E-07	7.69E-07	5.53E-06	3.29E-07	7.69E-07	5.53E-06	
273	KGT01_DPX_11_L_2mm	0.1	0.04	1.38E-06	3.22E-06	4.59E-03	1.38E-06	3.22E-06	4.59E-03	
274	KGT01_DPX_11_L_6mm	0.7	0.04	9.55E-07	2.23E-06	1.47E-03	9.55E-07	2.23E-06	1.47E-03	
275	KGT01_DPX_11_L_22mm	3.8	0.12	1.37E-06	3.19E-06	5.86E-04	1.37E-06	3.19E-06	5.86E-04	
276	KGT01_DPX_11_L_71mm	3.8	0.12	2.13E-07	4.96E-07	9.11E-05	2.13E-07	4.96E-07	9.11E-05	
277	KGT01_PC3_02_L_2mm	0.1	0.04	8.93E-07	2.08E-06	2.98E-03	8.93E-07	2.08E-06	2.98E-03	
278	KGT01_PC3_02_L_6mm	0.7	0.04	8.65E-07	2.02E-06	1.33E-03	8.65E-07	2.02E-06	1.33E-03	
279	KGT01_PC3_02_L_22mm	3.8	0.12	1.56E-06	3.64E-06	6.69E-04	1.56E-06	3.64E-06	6.69E-04	
280	KGT01_PC3_02_L_50mm	3.8	0.12	4.31E-07	1.00E-06	1.84E-04	4.31E-07	1.00E-06	1.84E-04	
281	KGT01_DPB_11_L_2mm	0.1	0.04	1.23E-06	2.86E-06	4.09E-03	1.23E-06	2.86E-06	4.09E-03	
282	KGT01_DPB_11_L_6mm	0.7	0.04	1.19E-06	2.79E-06	1.83E-03	1.19E-06	2.79E-06	1.83E-03	
283	KGT01_DPB_11_L_22mm	9.0	0.12	4.51E-06	1.05E-05	9.32E-04	4.51E-06	1.05E-05	9.32E-04	
284	KGT01_DPB_11_L_85mm	135	0.3	9.20E-06	2.15E-05	2.05E-04	9.20E-06	2.15E-05	2.05E-04	
285	KGT01_DPB_11_L_150mm	420	0.3	2.64E-07	6.15E-07	5.88E-06	2.64E-07	6.15E-07	5.88E-06	
286	KGT01_DPT_01_V_2mm	0.01	0.04	0.00E+00	0.00E+00	0.00E+00	1.58E-06	3.68E-06	5.26E-03	
287	KGT01_DPT_01_V_6mm	0.1	0.04	0.00E+00	0.00E+00	0.00E+00	7.39E-07	1.73E-06	2.19E-03	
288	KGT01_DPT_01_V_22mm	1.4	0.12	0.00E+00	0.00E+00	0.00E+00	1.19E-06	2.77E-06	1.11E-03	
289	KGT01_DPT_01_V_85mm	21	0.12	0.00E+00	0.00E+00	0.00E+00	2.09E-06	4.88E-06	1.24E-04	
289	KGT01_DPT_01_V_150mm	66	0.12	0.00E+00	0.00E+00	0.00E+00	3.29E-07	7.69E-07	5.53E-06	
290	KGT01_DP1_01_V_150mm KGT01_DPX_01_L_2mm	0.1	0.3	0.00E+00	0.00E+00	0.00E+00	1.43E-06	3.33E-06	4.75E-03	
292	KGT01_DPX_01_L_6mm	0.7	0.04	0.00E+00	0.00E+00	0.00E+00	9.97E-07	2.33E-06	1.54E-03	
293	KGT01_DPX_01_L_22mm	4.5	0.12	0.00E+00	0.00E+00	0.00E+00	1.66E-06	3.88E-06	6.17E-04	
294	KGT01_DPX_01_L_71mm	4.5	0.12	0.00E+00	0.00E+00	0.00E+00	2.39E-07	5.58E-07	8.85E-05	
295	KGT01_PC3_01_L_2mm	0.1	0.04	0.00E+00	0.00E+00	0.00E+00	7.25E-07	1.69E-06	2.41E-03	
296	KGT01_PC3_01_L_6mm	0.7	0.04	0.00E+00	0.00E+00	0.00E+00	7.06E-07	1.65E-06	1.09E-03	
297	KGT01_PC3_01_L_22mm	4.5	0.12	0.00E+00	0.00E+00	0.00E+00	1.46E-06	3.40E-06	5.40E-04	
298	KGT01_PC3_01_L_50mm	4.5	0.12	0.00E+00	0.00E+00	0.00E+00	4.51E-07	1.05E-06	1.67E-04	
299	KGT01_DPB_01_L_2mm	0.1	0.04	0.00E+00	0.00E+00	0.00E+00	1.26E-06	2.93E-06	4.18E-03	

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		Release		Base Case/ Sensitivity Case 1			Ser	Sensitivity 2 (Future Operation)		
Line No.	Release Scenario	Rate (kg/s)	Explosion Probability	Immediate Ignition Event Frequency	Delayed Ignition Event Frequency	Unignited Event Frequency <sup>Note 1</sup>	Immediate Ignition Event Frequency	Delayed Ignition Event Frequency	Unignited Event Frequency <sup>Note 1</sup>	
300	KGT01_DPB_01_L_6mm	0.7	0.04	0.00E+00	0.00E+00	0.00E+00	1.21E-06	2.82E-06	1.85E-03	
301	KGT01_DPB_01_L_22mm	9.0	0.12	0.00E+00	0.00E+00	0.00E+00	4.56E-06	1.06E-05	9.42E-04	
302	KGT01_DPB_01_L_85mm	135	0.3	0.00E+00	0.00E+00	0.00E+00	8.07E-06	1.88E-05	1.80E-04	
303	KGT01_DPB_01_L_150mm	420	0.3	0.00E+00	0.00E+00	0.00E+00	1.65E-07	3.84E-07	3.67E-06	
304	KGT01_DBT_11_V_2mm	0.01	0.04	1.07E-06	2.49E-06	3.56E-03	1.07E-06	2.49E-06	3.56E-03	
305	KGT01_DBT_11_V_6mm	0.1	0.04	4.57E-07	1.07E-06	1.52E-03	4.57E-07	1.07E-06	1.52E-03	
306	KGT01_DBT_11_V_22mm	0.8	0.04	5.24E-07	1.22E-06	7.56E-04	5.24E-07	1.22E-06	7.56E-04	
307	KGT01_DBT_11_V_85mm	12	0.12	1.63E-06	3.79E-06	1.77E-04	1.63E-06	3.79E-06	1.77E-04	
308	KGT01_DBT_11_V_150mm	37	0.12	2.17E-07	5.06E-07	7.11E-06	2.17E-07	5.06E-07	7.11E-06	
309	KGT01_DBX_11_L_2mm	0.1	0.04	2.18E-06	5.10E-06	7.27E-03	2.18E-06	5.10E-06	7.27E-03	
310	KGT01_DBX_11_L_6mm	0.5	0.04	1.50E-06	3.51E-06	2.56E-03	1.50E-06	3.51E-06	2.56E-03	
311	KGT01_DBX_11_L_22mm	3.1	0.12	2.11E-06	4.91E-06	1.06E-03	2.11E-06	4.91E-06	1.06E-03	
312	KGT01_DBX_11_L_63mm	3.1	0.12	3.83E-07	8.95E-07	1.94E-04	3.83E-07	8.95E-07	1.94E-04	
313	KGT01_NGL_01_L_2mm	0.1	0.04	1.23E-06	2.88E-06	4.10E-03	1.23E-06	2.88E-06	4.10E-03	
314	KGT01_NGL_01_L_6mm	0.5	0.04	1.06E-06	2.48E-06	1.81E-03	1.06E-06	2.48E-06	1.81E-03	
315	KGT01_NGL_01_L_22mm	6.7	0.12	3.47E-06	8.09E-06	9.25E-04	3.47E-06	8.09E-06	9.25E-04	
316	KGT01_NGL_01_L_85mm	100	0.3	7.12E-06	1.66E-05	1.74E-04	7.12E-06	1.66E-05	1.74E-04	
317	KGT01_NGL_01_L_150mm	311	0.3	1.57E-07	3.67E-07	3.51E-06	1.57E-07	3.67E-07	3.51E-06	
318	KGT01_NGL_02_L_2mm	0.1	0.04	1.79E-06	4.17E-06	5.96E-03	1.79E-06	4.17E-06	5.96E-03	
319	KGT01_NGL_02_L_6mm	0.5	0.04	1.47E-06	3.43E-06	2.44E-03	1.47E-06	3.43E-06	2.44E-03	
320	KGT01_NGL_02_L_22mm	7.2	0.12	4.39E-06	1.02E-05	1.10E-03	4.39E-06	1.02E-05	1.10E-03	
321	KGT01_NGL_02_L_85mm	108	0.3	9.51E-06	2.22E-05	2.17E-04	9.51E-06	2.22E-05	2.17E-04	
322	KGT01_NGL_02_L_150mm	335	0.3	8.61E-08	2.01E-07	1.92E-06	8.61E-08	2.01E-07	1.92E-06	
323	KGT01_DBT_01_V_2mm	0.01	0.04	0.00E+00	0.00E+00	0.00E+00	1.17E-06	2.72E-06	3.88E-03	
324	KGT01_DBT_01_V_6mm	0.1	0.04	0.00E+00	0.00E+00	0.00E+00	4.86E-07	1.13E-06	1.62E-03	
325	KGT01_DBT_01_V_22mm	0.8	0.04	0.00E+00	0.00E+00	0.00E+00	5.53E-07	1.29E-06	7.99E-04	
326	KGT01_DBT_01_V_71mm	8.3	0.12	0.00E+00	0.00E+00	0.00E+00	8.49E-07	1.98E-06	1.34E-04	
327	KGT01 DBX 01 L 2mm	0.1	0.04	0.00E+00	0.00E+00	0.00E+00	1.56E-06	3.64E-06	5.20E-03	
328	KGT01_DBX_01_L_6mm	0.5	0.04	0.00E+00	0.00E+00	0.00E+00	1.02E-06	2.38E-06	1.73E-03	
329	KGT01_DBX_01_L_22mm	3.1	0.12	0.00E+00	0.00E+00	0.00E+00	1.42E-06	3.32E-06	7.19E-04	
330	KGT01_DBX_01_L_63mm	3.1	0.12	0.00E+00	0.00E+00	0.00E+00	2.25E-07	5.25E-07	1.14E-04	
331	KGT01_DBB_01_L_2mm	0.1	0.04	0.00E+00	0.00E+00	0.00E+00	7.84E-07	1.83E-06	2.61E-03	
332	KGT01_DBB_01_L_6mm	0.5	0.04	0.00E+00	0.00E+00	0.00E+00	6.86E-07	1.60E-06	1.17E-03	
333	KGT01_DBB_01_L_22mm	6.7	0.12	0.00E+00	0.00E+00	0.00E+00	2.23E-06	5.21E-06	5.96E-04	
334	KGT01_DBB_01_L_85mm	100	0.3	0.00E+00	0.00E+00	0.00E+00	5.48E-06	1.28E-05	1.34E-04	
335	KGT01_DBB_01_L_150mm	311	0.3	0.00E+00	0.00E+00	0.00E+00	5.62E-08	1.31E-07	1.25E-06	
336	KGT01_PC4_12_L_2mm	0.1	0.04	0.00E+00	0.00E+00	0.00E+00	7.43E-07	1.73E-06	2.47E-03	
337	KGT01_PC4_12_L_6mm	0.5	0.04	0.00E+00	0.00E+00	0.00E+00	6.57E-07	1.53E-06	1.12E-03	
338	KGT01_PC4_12_L_22mm	6.7	0.12	0.00E+00	0.00E+00	0.00E+00	2.11E-06	4.93E-06	5.59E-04	
339	KGT01_PC4_12_L_63mm	55	0.12	0.00E+00	0.00E+00	0.00E+00	4.50E-06	1.05E-05	1.91E-04	
340	KGT01_PC3_13_L_2mm	0.1	0.04	0.00E+00	0.00E+00	0.00E+00	4.30E-00 4.42E-07	1.03E-05	1.47E-03	
340	KGT01_PC3_13_L_2mm	0.1	0.04	0.00E+00	0.00E+00	0.00E+00	4.42E-07 4.10E-07	9.58E-07	6.33E-04	
341		8.9	0.04	0.00E+00	0.00E+00	0.00E+00	4.10E-07 1.39E-06	3.25E-07	2.91E-04	
	KGT01_PC3_13_L_22mm	46				0.00E+00	1.39E-06		7.36E-05	
343	KGT01_PC3_13_L_50mm	0.1	0.12	0.00E+00	0.00E+00 0.00E+00		9.03E-07	3.43E-06	7.36E-05 3.01E-03	
344	KGT01_LPG_04_L_2mm			0.00E+00		0.00E+00		2.11E-06		
345	KGT01_LPG_04_L_6mm	0.6	0.04	0.00E+00	0.00E+00	0.00E+00	8.09E-07	1.89E-06	1.30E-03	
346	KGT01_LPG_04_L_22mm	7.9	0.12	0.00E+00	0.00E+00	0.00E+00	2.78E-06	6.50E-06	6.43E-04	
347	KGT01_LPG_04_L_50mm	41	0.12	0.00E+00	0.00E+00	0.00E+00	2.19E-06	5.11E-06	1.22E-04	
348	KGT32_NGL_05_L_2mm	0.1	0.04	2.05E-07	4.78E-07	6.82E-04	2.05E-07	4.78E-07	6.82E-04	
349	KGT32_NGL_05_L_6mm	0.5	0.04	1.79E-07	4.18E-07	2.98E-04	1.79E-07	4.18E-07	2.98E-04	

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		Delegas		Base Case/ Sensitivity Case 1				Sensitivity 2 (Future Operation)			
Line No.	Release Scenario	Release Rate (kg/s)	Explosion Probability	Immediate Ignition Event Frequency	Delayed Ignition Event Frequency	Unignited Event Frequency <sup>Note 1</sup>	Immediate Ignition Event Frequency	Delayed Ignition Event Frequency	Unignited Event Frequency <sup>Note 1</sup>		
350	KGT32_NGL_05_L_22mm	7.2	0.12	5.59E-07	1.30E-06	1.40E-04	5.59E-07	1.30E-06	1.40E-04		
351	KGT32_NGL_05_L_50mm	37	0.12	6.98E-07	1.63E-06	4.22E-05	6.98E-07	1.63E-06	4.22E-05		
352	KGT33_NGL_06_L_2mm	0.1	0.04	4.47E-07	1.04E-06	1.49E-03	4.47E-07	1.04E-06	1.49E-03		
353	KGT33_NGL_06_L_6mm	0.5	0.04	3.85E-07	8.99E-07	6.39E-04	3.85E-07	8.99E-07	6.39E-04		
354	KGT33_NGL_06_L_22mm	7.2	0.12	1.27E-06	2.97E-06	3.18E-04	1.27E-06	2.97E-06	3.18E-04		
355	KGT33_NGL_06_L_71mm	75	0.3	1.58E-06	3.69E-06	5.04E-05	1.58E-06	3.69E-06	5.04E-05		
356	KGT34_NGL_07_L_10mm	0.01	0.04	3.00E-08	7.00E-08	9.99E-05	3.00E-08	7.00E-08	9.99E-05		
357	KGT34_NGL_07_L_50mm	0.1	0.04	1.60E-09	3.74E-09	4.99E-06	1.60E-09	3.74E-09	4.99E-06		
358	KGT34_NGL_07_L_FBR	1000	0.3	2.25E-08	5.25E-08	4.93E-06	2.25E-08	5.25E-08	4.93E-06		
359	KGT35_NGL_09_L_2mm	0.04	0.04	1.43E-06	3.34E-06	4.77E-03	1.43E-06	3.34E-06	4.77E-03		
360	KGT35_NGL_09_L_6mm	0.3	0.04	7.54E-07	1.76E-06	1.46E-03	7.54E-07	1.76E-06	1.46E-03		
361	KGT35_NGL_09_L_22mm	4.7	0.12	1.33E-06	3.11E-06	4.80E-04	1.33E-06	3.11E-06	4.80E-04		
362	KGT35_NGL_09_L_71mm	11	0.12	5.33E-07	1.24E-06	9.41E-05	5.33E-07	1.24E-06	9.41E-05		
363	KGT36_NGL_10_L_2mm	0.04	0.04	3.73E-07	8.71E-07	1.24E-03	3.73E-07	8.71E-07	1.24E-03		
364	KGT36_NGL_10_L_6mm	0.3	0.04	2.90E-07	6.77E-07	5.62E-04	2.90E-07	6.77E-07	5.62E-04		
365	KGT36_NGL_10_L_22mm	4.7	0.12	8.16E-07	1.90E-06	2.94E-04	8.16E-07	1.90E-06	2.94E-04		
366	KGT36_NGL_10_L_71mm	49	0.12	1.53E-06	3.58E-06	7.26E-05	1.53E-06	3.58E-06	7.26E-05		
367	KGT36_NGL_11_L_10mm	1.0	0.04	4.24E-05	9.90E-05	5.71E-02	5.94E-05	1.39E-04	7.98E-02		
368	KGT36_NGL_11_L_100mm	97	0.3	2.01E-04	4.69E-04	5.05E-03	2.81E-04	6.56E-04	7.06E-03		
369	KGT37_PC3_05_L_2mm	0.1	0.04	3.20E-07	7.47E-07	1.07E-03	3.20E-07	7.47E-07	1.07E-03		
370	KGT37_PC3_05_L_6mm	0.7	0.04	3.04E-07	7.08E-07	4.67E-04	3.04E-07	7.08E-07	4.67E-04		
371	KGT37_PC3_05_L_22mm	8.9	0.12	1.07E-06	2.50E-06	2.23E-04	1.07E-06	2.50E-06	2.23E-04		
372	KGT37_PC3_05_L_63mm	73	0.3	1.61E-06	3.75E-06	5.26E-05	1.61E-06	3.75E-06	5.26E-05		
373	KGT39_PC3_07_V_10mm	0.2	0.04	1.94E-09	4.52E-09	4.99E-06	1.94E-09	4.52E-09	4.99E-06		
374	KGT39_PC3_07_V_50mm	3.9	0.12	7.36E-10	1.72E-09	2.48E-07	7.36E-10	1.72E-09	2.48E-07		
375	KGT39_PC3_07_V_FBR	1000	0.3	4.88E-08	1.14E-07	8.75E-08	4.88E-08	1.14E-07	8.75E-08		
376	KGT39_PC3_08_L_10mm	1.3	0.12	4.70E-09	1.10E-08	4.98E-06	4.70E-09	1.10E-08	4.98E-06		
377	KGT39_PC3_08_L_50mm	33	0.12	3.52E-09	8.20E-09	2.38E-07	3.52E-09	8.20E-09	2.38E-07		
378	KGT39_PC3_08_L_FBR	1000	0.3	9.75E-09	2.28E-08	2.18E-07	9.75E-09	2.28E-08	2.38E-07 2.18E-07		
379	KGT40_PC3_09_V_10mm	0.2	0.04	1.94E-09	4.52E-09	4.99E-06	1.94E-09	4.52E-09	4.99E-06		
379	KGT40_PC3_09_V_50mm	3.9	0.04	7.36E-10	1.72E-09	2.48E-07	7.36E-10	4.32E-09 1.72E-09	2.48E-07		
	KGT40_PC3_09_V_50MM	1000	0.12	4.88E-08	1.14E-07	8.75E-08	4.88E-08	1.14E-07	8.75E-08		
381				4.88E-08 4.70E-09		4.98E-06	4.88E-08 4.70E-09		4.98E-06		
382	KGT40_PC3_10_L_10mm	1.3	0.12		1.10E-08			1.10E-08			
383	KGT40_PC3_10_L_50mm	33	0.12	3.52E-09	8.20E-09	2.38E-07	3.52E-09	8.20E-09	2.38E-07		
384	KGT40_PC3_10_L_FBR	1000	0.3	9.75E-09	2.28E-08	2.18E-07	9.75E-09	2.28E-08	2.18E-07		
385	KGT41_PC4_04_L_2mm	0.1	0.04	3.98E-07	9.28E-07	1.32E-03	3.98E-07	9.28E-07	1.32E-03 5.77E-04		
386	KGT41_PC4_04_L_6mm	0.5		3.39E-07	7.92E-07	5.77E-04	3.39E-07	7.92E-07			
387	KGT41_PC4_04_L_22mm	6.8	0.12	1.01E-06	2.36E-06	2.67E-04	1.01E-06	2.36E-06	2.67E-04		
388	KGT41_PC4_04_L_63mm	56	0.3	1.70E-06	3.97E-06	7.19E-05	1.70E-06	3.97E-06	7.19E-05		
389	KGT43_PC4_06_V_10mm	0.1	0.04	1.50E-09	3.50E-09	5.00E-06	1.50E-09	3.50E-09	5.00E-06		
390	KGT43_PC4_06_V_50mm	1.5	0.12	2.86E-10	6.66E-10	2.49E-07	2.86E-10	6.66E-10	2.49E-07		
391	KGT43_PC4_06_V_FBR	1000	0.3	4.88E-08	1.14E-07	8.75E-08	4.88E-08	1.14E-07	8.75E-08		
392	KGT43_PC4_07_L_10mm	0.7	0.04	3.38E-09	7.89E-09	4.99E-06	3.38E-09	7.89E-09	4.99E-06		
393	KGT43_PC4_07_L_50mm	19	0.12	2.20E-09	5.13E-09	2.43E-07	2.20E-09	5.13E-09	2.43E-07		
394	KGT43_PC4_07_L_FBR	1000	0.3	9.75E-09	2.28E-08	2.18E-07	9.75E-09	2.28E-08	2.18E-07		
395	KGT44_PC4_08_V_10mm	0.1	0.04	1.50E-09	3.50E-09	5.00E-06	1.50E-09	3.50E-09	5.00E-06		
396	KGT44_PC4_08_V_50mm	1.5	0.12	2.86E-10	6.66E-10	2.49E-07	2.86E-10	6.66E-10	2.49E-07		
397	KGT44_PC4_08_V_FBR	1000	0.3	4.88E-08	1.14E-07	8.75E-08	4.88E-08	1.14E-07	8.75E-08		
398	KGT44_PC4_09_L_10mm	0.7	0.04	3.38E-09	7.89E-09	4.99E-06	3.38E-09	7.89E-09	4.99E-06		
399	KGT44_PC4_09_L_50mm	19	0.12	2.20E-09	5.13E-09	2.43E-07	2.20E-09	5.13E-09	2.43E-07		

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		Release		Base Case/ Sensitivity Case 1			Ser	Sensitivity 2 (Future Operation)		
Line No.	Release Scenario	Rate (kg/s)	Explosion Probability	Immediate Ignition Event Frequency	Delayed Ignition Event Frequency	Unignited Event Frequency <sup>Note 1</sup>	Immediate Ignition Event Frequency	Delayed Ignition Event Frequency	Unignited Event Frequency <sup>Note 1</sup>	
400	KGT44_PC4_09_L_FBR	1000	0.3	9.75E-09	2.28E-08	2.18E-07	9.75E-09	2.28E-08	2.18E-07	
401	KGT45_PC3_12_L_2mm	0.1	0.04	1.85E-06	4.32E-06	6.16E-03	1.85E-06	4.32E-06	6.16E-03	
402	KGT45_PC3_12_L_6mm	0.6	0.04	1.27E-06	2.97E-06	2.08E-03	1.27E-06	2.97E-06	2.08E-03	
403	KGT45_PC3_12_L_22mm	7.6	0.12	3.28E-06	7.66E-06	7.88E-04	3.28E-06	7.66E-06	7.88E-04	
404	KGT45_PC3_12_L_85mm	12	0.12	9.20E-07	2.15E-06	1.49E-04	9.20E-07	2.15E-06	1.49E-04	
405	KGT45_PC3_12_L_173mm	12	0.12	1.29E-07	3.01E-07	2.09E-05	1.29E-07	3.01E-07	2.09E-05	
406	KGT46_PC4_11_L_2mm	0.05	0.04	1.66E-06	3.88E-06	5.53E-03	1.66E-06	3.88E-06	5.53E-03	
407	KGT46_PC4_11_L_6mm	0.4	0.04	9.96E-07	2.32E-06	1.80E-03	9.96E-07	2.32E-06	1.80E-03	
408	KGT46_PC4_11_L_22mm	5.7	0.12	2.12E-06	4.94E-06	6.44E-04	2.12E-06	4.94E-06	6.44E-04	
409	KGT46_PC4_11_L_85mm	14	0.12	7.92E-07	1.85E-06	1.14E-04	7.92E-07	1.85E-06	1.14E-04	
410	KGT46_PC4_11_L_173mm	14	0.12	1.19E-07	2.79E-07	1.71E-05	1.19E-07	2.79E-07	1.71E-05	
411	KGT47_LPG_01_L_2mm	0.1	0.04	2.91E-07	6.79E-07	9.70E-04	2.91E-07	6.79E-07	9.70E-04	
412	KGT47_LPG_01_L_6mm	0.5	0.04	2.43E-07	5.67E-07	4.14E-04	2.43E-07	5.67E-07	4.14E-04	
413	KGT47_LPG_01_L_22mm	6.7	0.12	7.67E-07	1.79E-06	2.03E-04	7.67E-07	1.79E-06	2.03E-04	
414	KGT47_LPG_01_L_71mm	70	0.3	9.45E-07	2.21E-06	3.23E-05	9.45E-07	2.21E-06	3.23E-05	
415	KGT47_LPG_02_L_8mm	0.9	0.04	6.27E-07	1.46E-06	8.69E-04	1.29E-06	3.01E-06	1.79E-03	
416	KGT47_LPG_02_L_80mm	89	0.3	2.84E-06	6.63E-06	7.76E-05	5.84E-06	1.36E-05	1.60E-04	
417	KGT47 LPG 05 L 5mm	0.3	0.04	3.21E-07	7.49E-07	6.23E-04	6.17E-07	1.44E-06	1.20E-03	
418	KGT47_LPG_05_L_50mm	35	0.12	9.24E-07	2.16E-06	5.93E-05	1.78E-06	4.15E-06	1.14E-04	
419	KGT70_REF_01_V_2mm	0.001	0.04	2.81E-07	6.56E-07	9.36E-04	2.81E-07	6.56E-07	9.36E-04	
420	KGT70_REF_01_V_6mm	0.01	0.04	1.24E-07	2.90E-07	4.13E-04	1.24E-07	2.90E-07	4.13E-04	
421	KGT70 REF 01 V 22mm	0.2	0.04	8.44E-08	1.97E-07	2.08E-04	8.44E-08	1.97E-07	2.08E-04	
421	KGT70_REF_01_V_71mm	1.9	0.12	6.91E-08	1.61E-07	4.92E-05	6.91E-08	1.61E-07	4.92E-04	
422	KGT70_REF_01_V_7111111	0.04	0.12	2.91E-07	6.80E-07	9.70E-04	2.91E-07	6.80E-07	9.70E-04	
423	KGT70_REF_02_L_2mm	0.04	0.04	2.23E-07		4.28E-04	2.91E-07 2.23E-07	5.21E-07		
					5.21E-07		6.26E-07		4.28E-04	
425	KGT70_REF_02_L_22mm	4.9	0.12	6.26E-07	1.46E-06	2.19E-04		1.46E-06	2.19E-04	
426	KGT70_REF_02_L_71mm	51	0.3	9.58E-07	2.23E-06	4.40E-05	9.58E-07	2.23E-06	4.40E-05	
427	KGT70_REF_03_V_2mm	0.004	0.04	1.14E-06	2.66E-06	3.79E-03	1.14E-06	2.66E-06	3.79E-03	
428	KGT70_REF_03_V_6mm	0.03	0.04	4.49E-07	1.05E-06	1.49E-03	4.49E-07	1.05E-06	1.49E-03	
429	KGT70_REF_03_V_22mm	0.5	0.04	3.55E-07	8.28E-07	6.22E-04	3.55E-07	8.28E-07	6.22E-04	
430	KGT70_REF_03_V_85mm	6.9	0.12	6.87E-07	1.60E-06	1.31E-04	6.87E-07	1.60E-06	1.31E-04	
431	KGT70_REF_03_V_150mm	21	0.12	1.01E-07	2.35E-07	5.92E-06	1.01E-07	2.35E-07	5.92E-06	
432	KGT70_REF_04_L_2mm	0.04	0.04	6.35E-07	1.48E-06	2.12E-03	6.35E-07	1.48E-06	2.12E-03	
433	KGT70_REF_04_L_6mm	0.4	0.04	4.88E-07	1.14E-06	9.35E-04	4.88E-07	1.14E-06	9.35E-04	
434	KGT70_REF_04_L_22mm	4.9	0.12	1.32E-06	3.07E-06	4.61E-04	1.32E-06	3.07E-06	4.61E-04	
435	KGT70_REF_04_L_85mm	72	0.3	2.91E-06	6.78E-06	9.62E-05	2.91E-06	6.78E-06	9.62E-05	
436	KGT70_REF_04_L_173mm	300	0.3	3.74E-07	8.74E-07	8.35E-06	3.74E-07	8.74E-07	8.35E-06	
437	KGT70_REF_05_L_2mm	0.02	0.04	5.10E-07	1.19E-06	1.70E-03	5.10E-07	1.19E-06	1.70E-03	
438	KGT70_REF_05_L_6mm	0.2	0.04	3.16E-07	7.37E-07	7.65E-04	3.16E-07	7.37E-07	7.65E-04	
439	KGT70_REF_05_L_22mm	2.5	0.12	6.30E-07	1.47E-06	3.85E-04	6.30E-07	1.47E-06	3.85E-04	
440	KGT70_REF_05_L_85mm	38	0.12	1.65E-06	3.85E-06	9.90E-05	1.65E-06	3.85E-06	9.90E-05	
441	KGT70_REF_05_L_150mm	117	0.3	5.62E-08	1.31E-07	1.25E-06	5.62E-08	1.31E-07	1.25E-06	
442	KGT70_REF_07_L_2mm	0.02	0.04	4.03E-07	9.39E-07	1.34E-03	4.03E-07	9.39E-07	1.34E-03	
443	KGT70_REF_07_L_6mm	0.2	0.04	2.54E-07	5.94E-07	6.16E-04	2.54E-07	5.94E-07	6.16E-04	
444	KGT70_REF_07_L_22mm	2.5	0.12	4.96E-07	1.16E-06	3.03E-04	4.96E-07	1.16E-06	3.03E-04	
445	KGT70_REF_07_L_85mm	38	0.12	1.66E-06	3.88E-06	9.99E-05	1.66E-06	3.88E-06	9.99E-05	
446	KGT70_REF_07_L_150mm	117	0.3	6.96E-08	1.62E-07	1.55E-06	6.96E-08	1.62E-07	1.55E-06	
447	KGT70_REF_11_V_2mm	0.001	0.04	1.47E-06	3.44E-06	4.90E-03	1.47E-06	3.44E-06	4.90E-03	
448	KGT70_REF_11_V_6mm	0.01	0.04	5.97E-07	1.39E-06	1.99E-03	5.97E-07	1.39E-06	1.99E-03	
449	KGT70_REF_11_V_22mm	0.2	0.04	3.66E-07	8.54E-07	9.00E-04	3.66E-07	8.54E-07	9.00E-04	

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		Release		Base Case/ Sensitivity Case 1			Sensitivity 2 (Future Operation)			
Line No.	Release Scenario	Rate (kg/s)	Explosion Probability	Immediate Ignition Event Frequency	Delayed Ignition Event Frequency	Unignited Event Frequency <sup>Note 1</sup>	Immediate Ignition Event Frequency	Delayed Ignition Event Frequency	Unignited Event Frequency <sup>Note 1</sup>	
450	KGT70_REF_11_V_85mm	2.7	0.12	2.98E-07	6.95E-07	1.48E-04	2.98E-07	6.95E-07	1.48E-04	
451	KGT70_REF_11_V_212mm	17	0.12	3.91E-07	9.13E-07	3.01E-05	3.91E-07	9.13E-07	3.01E-05	
452	KGT70_REF_14_V_2mm	0.004	0.04	5.39E-06	1.26E-05	1.80E-02	5.39E-06	1.26E-05	1.80E-02	
453	KGT70_REF_14_V_6mm	0.03	0.04	2.45E-06	5.71E-06	8.15E-03	2.45E-06	5.71E-06	8.15E-03	
454	KGT70_REF_14_V_22mm	0.5	0.04	2.19E-06	5.11E-06	3.84E-03	2.19E-06	5.11E-06	3.84E-03	
455	KGT70_REF_14_V_85mm	6.9	0.12	4.20E-06	9.81E-06	7.99E-04	4.20E-06	9.81E-06	7.99E-04	
456	KGT70_REF_14_V_194mm	36	0.12	6.68E-06	1.56E-05	2.26E-04	6.68E-06	1.56E-05	2.26E-04	
457	KGT70_REF_15_L_2mm	0.04	0.04	1.20E-06	2.81E-06	4.00E-03	1.20E-06	2.81E-06	4.00E-03	
458	KGT70_REF_15_L_6mm	0.4	0.04	7.90E-07	1.84E-06	1.51E-03	7.90E-07	1.84E-06	1.51E-03	
459	KGT70_REF_15_L_22mm	4.9	0.12	1.83E-06	4.26E-06	6.40E-04	1.83E-06	4.26E-06	6.40E-04	
460	KGT70_REF_15_L_85mm	72	0.3	2.83E-06	6.60E-06	9.35E-05	2.83E-06	6.60E-06	9.35E-05	
461	KGT70_REF_15_L_173mm	300	0.3	4.29E-07	1.00E-06	9.56E-06	4.29E-07	1.00E-06	9.56E-06	
462	KGT70_REF_06_L_2mm	0.02	0.04	0.00E+00	0.00E+00	0.00E+00	6.40E-07	1.49E-06	2.13E-03	
463	KGT70_REF_06_L_6mm	0.2	0.04	0.00E+00	0.00E+00	0.00E+00	3.90E-07	9.11E-07	9.45E-04	
464	KGT70_REF_06_L_22mm	2.5	0.12	0.00E+00	0.00E+00	0.00E+00	7.51E-07	1.75E-06	4.59E-04	
465	KGT70_REF_06_L_85mm	38	0.12	0.00E+00	0.00E+00	0.00E+00	1.94E-06	4.53E-06	1.16E-04	
466	KGT70_REF_06_L_150mm	117	0.3	0.00E+00	0.00E+00	0.00E+00	2.80E-07	6.53E-07	6.25E-06	
467	KGT50_EMC_01_L_2mm	0.02	0.04	1.73E-06	4.04E-06	5.76E-03	1.73E-06	4.04E-06	5.76E-03	
468	KGT50_EMC_01_L_2mm	0.02	0.04	5.86E-07	1.37E-06	1.95E-03	5.86E-07	1.37E-06	1.95E-03	
469	KGT50 EMC 01 L 12mm	0.02	0.04	2.93E-07			2.93E-07	6.84E-07	9.76E-04	
					6.84E-07	9.76E-04				
470	KGT50_EMC_02_L_5mm	0.2	0.04	4.68E-08	1.09E-07	1.20E-04	4.68E-08	1.09E-07	1.20E-04	
471	KGT50_EMC_02_L_10mm	0.6	0.04	1.84E-08	4.30E-08	2.87E-05	1.84E-08	4.30E-08	2.87E-05	
472	KGT50_EMC_02_L_FBR	1000	0.3	1.56E-07	3.64E-07	3.48E-06	1.56E-07	3.64E-07	3.48E-06	
473	KGT51_BMC_05_L_5mm	0.4	0.04	5.53E-10	1.29E-09	9.98E-07	5.53E-10	1.29E-09	9.98E-07	
474	KGT51_BMC_05_L_10mm	1.7	0.12	2.81E-10	6.55E-10	2.39E-07	2.81E-10	6.55E-10	2.39E-07	
475	KGT51_BMC_05_L_FBR	1000	0.3	7.80E-08	1.82E-07	1.74E-06	7.80E-08	1.82E-07	1.74E-06	
476	KGT52_BMC_01_L_10mm	0.6	0.04	6.25E-09	1.46E-08	9.98E-06	6.25E-09	1.46E-08	9.98E-06	
477	KGT52_BMC_01_L_50mm	15	0.12	3.66E-09	8.53E-09	4.88E-07	3.66E-09	8.53E-09	4.88E-07	
478	KGT52_BMC_01_L_FBR	1000	0.3	1.95E-08	4.55E-08	4.35E-07	1.95E-08	4.55E-08	4.35E-07	
479	KGT52_BMC_02_L_2mm	0.001	0.04	1.33E-06	3.10E-06	4.42E-03	1.33E-06	3.10E-06	4.42E-03	
480	KGT52_BMC_02_L_6mm	0.001	0.04	5.90E-07	1.38E-06	1.97E-03	5.90E-07	1.38E-06	1.97E-03	
481	KGT52_BMC_02_L_12mm	0.001	0.04	4.75E-07	1.11E-06	1.58E-03	4.75E-07	1.11E-06	1.58E-03	
482	KGT52_BMC_03_L_5mm	0.2	0.04	1.02E-08	2.37E-08	2.66E-05	1.02E-08	2.37E-08	2.66E-05	
483	KGT52_BMC_03_L_50mm	15	0.12	1.95E-08	4.54E-08	2.60E-06	1.95E-08	4.54E-08	2.60E-06	
484	KGT55_MOH_01_L_10mm	0.01	0.04	1.20E-08	2.80E-08	4.00E-05	1.20E-08	2.80E-08	4.00E-05	
485	KGT55_MOH_01_L_50mm	0.1	0.04	6.49E-10	1.52E-09	2.00E-06	6.49E-10	1.52E-09	2.00E-06	
486	KGT55_MOH_01_L_FBR	1000	0.3	9.00E-09	2.10E-08	1.97E-06	9.00E-09	2.10E-08	1.97E-06	
487	KGT55_MOH_02_L_2mm	0.01	0.04	2.76E-06	6.44E-06	9.19E-03	2.76E-06	6.44E-06	9.19E-03	
488	KGT55_MOH_02_L_6mm	0.01	0.04	1.24E-06	2.88E-06	4.12E-03	1.24E-06	2.88E-06	4.12E-03	
489	KGT55_MOH_02_L_16mm	0.01	0.04	1.00E-06	2.33E-06	3.33E-03	1.00E-06	2.33E-06	3.33E-03	
490	KGT55_MOH_03_L_4mm	0.01	0.04	2.52E-06	5.88E-06	8.39E-03	3.60E-06	8.40E-06	1.20E-02	
491	KGT55_MOH_03_L_40mm	1.1	0.12	6.78E-07	1.58E-06	8.38E-04	9.69E-07	2.26E-06	1.20E-03	
492	KGT80_AMM_01_V_2mm	0.01	-	Тохіс	Toxic	8.30E-03	Toxic	Toxic	8.30E-03	
493	KGT80_AMM_01_V_6mm	0.1	-	Toxic	Toxic	3.77E-03	Toxic	Toxic	3.77E-03	
494	KGT80_AMM_01_V_22mm	0.9	_	Toxic	Toxic	1.75E-03	Toxic	Toxic	1.75E-03	
495	KGT80_AMM_01_V_85mm	14	-	Toxic	Toxic	3.93E-04	Toxic	Toxic	3.93E-04	
496	KGT80_AMM_01_V_150mm	43	-	Toxic	Toxic	1.18E-04	Toxic	Toxic	1.18E-04	
497	KGT80_AMM_11_V_2mm	0.01	-	Тохіс	Toxic	8.46E-03	Toxic	Toxic	8.46E-03	
498	KGT80_AMM_11_V_6mm	0.1	-	Тохіс	Toxic	3.82E-03	Toxic	Toxic	3.82E-03	
		0.9		Тохіс	Toxic	1.77E-03	Toxic	Toxic	1.77E-03	

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		Release		Ва	se Case/ Sensitivity C	Case 1	Ser	nsitivity 2 (Future Open	ation)
Line No.	Release Scenario	Rate (kg/s)	Explosion Probability	Immediate Ignition Event Frequency	Delayed Ignition Event Frequency	Unignited Event Frequency <sup>Note 1</sup>	Immediate Ignition Event Frequency	Delayed Ignition Event Frequency	Unignited Event Frequency <sup>Note 1</sup>
500	KGT80_AMM_11_V_85mm	14	-	Тохіс	Toxic	3.88E-04	Toxic	Toxic	3.88E-04
501	KGT80_AMM_11_V_150mm	43	-	Тохіс	Toxic	1.18E-04	Toxic	Toxic	1.18E-04
502	KGT80_AMM_02_V_2mm	0.01	-	Тохіс	Toxic	1.43E-03	Toxic	Toxic	1.43E-03
503	KGT80_AMM_02_V_6mm	0.1	-	Toxic	Toxic	6.42E-04	Toxic	Toxic	6.42E-04
504	KGT80_AMM_02_V_18mm	0.6	-	Toxic	Toxic	4.21E-04	Toxic	Toxic	4.21E-04
505	KGT80_AMM_03_L_2mm	0.1	-	Toxic	Toxic	1.21E-02	Toxic	Toxic	1.21E-02
506	KGT80_AMM_03_L_6mm	0.8	-	Toxic	Toxic	4.42E-03	Toxic	Toxic	4.42E-03
507	KGT80_AMM_03_L_22mm	11	-	Toxic	Toxic	1.58E-03	Toxic	Toxic	1.58E-03
508	KGT80_AMM_03_L_71mm	115	-	Toxic	Toxic	4.20E-04	Toxic	Toxic	4.20E-04
509	KGT80_AMM_04_L_2mm	0.1	-	Тохіс	Toxic	1.83E-02	Toxic	Toxic	1.83E-02
510	KGT80_AMM_04_L_6mm	0.8	-	Toxic	Toxic	6.86E-03	Toxic	Toxic	6.86E-03
511	KGT80_AMM_04_L_22mm	11	-	Toxic	Toxic	2.55E-03	Toxic	Toxic	2.55E-03
512	KGT80_AMM_04_L_71mm	115	-	Toxic	Toxic	6.85E-04	Toxic	Toxic	6.85E-04
513	KGT80_AMM_07_L_2mm	0.1	-	Toxic	Toxic	2.48E-03	Toxic	Toxic	2.48E-03
514	KGT80_AMM_07_L_6mm	0.8	-	Toxic	Toxic	1.12E-03	Toxic	Toxic	1.12E-03
515	KGT80_AMM_07_L_16mm	5.9	-	Toxic	Toxic	7.33E-04	Toxic	Toxic	7.33E-04
516	KGT80_AMM_08_V_2mm	0.000	-	Toxic	Toxic	3.27E-03	Toxic	Toxic	3.27E-03
517	KGT80_AMM_08_V_6mm	0.001	-	Тохіс	Toxic	1.40E-03	Toxic	Toxic	1.40E-03
518	KGT80_AMM_08_V_22mm	0.01	-	Toxic	Toxic	6.46E-04	Toxic	Toxic	6.46E-04
519	KGT80_AMM_08_V_85mm	0.1	-	Toxic	Toxic	1.89E-04	Toxic	Toxic	1.89E-04
520	KGT80_AMM_08_V_194mm	0.7	-	Toxic	Toxic	5.75E-06	Toxic	Toxic	5.75E-06
521	KGT80_AMM_09_V_2mm	0.000	-	Toxic	Toxic	1.64E-02	Toxic	Toxic	1.64E-02
522	KGT80_AMM_09_V_6mm	0.001	-	Toxic	Toxic	6.07E-03	Toxic	Toxic	6.07E-03
523	KGT80_AMM_09_V_22mm	0.01	-	Тохіс	Toxic	2.23E-03	Toxic	Toxic	2.23E-03
524	KGT80_AMM_09_V_63mm	0.1	_	Тохіс	Toxic	5.46E-04	Toxic	Toxic	5.46E-04
525	KGT90_CO2_01_V_2mm	0.01		Тохіс	Toxic	9.50E-03	Toxic	Toxic	9.50E-03
526	KGT90_CO2_01_V_6mm	0.1	-	Тохіс	Toxic	4.37E-03	Toxic	Toxic	4.37E-03
520	KGT90_CO2_01_V_22mm	1.7	_	Тохіс	Toxic	2.09E-03	Toxic	Toxic	2.09E-03
527	KGT90_CO2_01_V_71mm	18	-	Тохіс	Тохіс	6.75E-04	Toxic	Toxic	6.75E-04
529	KGT90_CO2_02_V_2mm	0.01	-	Тохіс	Тохіс	9.52E-03	Toxic	Toxic	9.52E-04
530	KGT90_CO2_02_V_2mm	0.01	-	Тохіс	Toxic	4.38E-03	Toxic	Toxic	4.38E-03
530	KGT90_CO2_02_V_00000	1.7	-	Тохіс	Toxic	2.10E-03	Toxic	Toxic	2.10E-03
		1.7	-		Toxic	6.80E-04			
532 533	KGT90_CO2_02_V_71mm KGT90_CO2_03_V_2mm	0.01	-	Toxic			Toxic	Toxic	6.80E-04
				Toxic	Toxic	3.37E-03	Toxic	Toxic	3.37E-03
534	KGT90_CO2_03_V_6mm	0.1	-	Toxic	Toxic	1.60E-03	Toxic	Toxic	1.60E-03
535	KGT90_CO2_03_V_22mm	1.7	-	Toxic	Toxic	8.57E-04	Toxic	Toxic	8.57E-04
536	KGT90_CO2_03_V_71mm	18	-	Toxic	Toxic	3.41E-04	Toxic	Toxic	3.41E-04
537	KGT90_CO2_07_V_2mm	0.01	-	Toxic	Toxic	4.78E-03	Toxic	Toxic	4.78E-03
538	KGT90_CO2_07_V_6mm	0.1	-	Toxic	Toxic	2.05E-03	Toxic	Toxic	2.05E-03
539	KGT90_CO2_07_V_22mm	1.7	-	Toxic	Toxic	9.86E-04	Toxic	Toxic	9.86E-04
540	KGT90_CO2_07_V_63mm	14	-	Toxic	Toxic	2.49E-04	Toxic	Toxic	2.49E-04
541	KGT90_CO2_08_L_2mm	0.1	-	Toxic	Toxic	8.75E-03	Toxic	Toxic	8.75E-03
542	KGT90_CO2_08_L_6mm	1.0	-	Toxic	Toxic	3.25E-03	Toxic	Toxic	3.25E-03
543	KGT90_CO2_08_L_22mm	2.1	-	Тохіс	Toxic	1.37E-03	Toxic	Toxic	1.37E-03
544	KGT90_CO2_08_L_71mm	2.1	-	Тохіс	Toxic	4.04E-04	Toxic	Toxic	4.04E-04
545	KGT90_CO2_16_V_2mm	0.001	-	Тохіс	Toxic	2.50E-02	Toxic	Toxic	2.50E-02
546	KGT90_CO2_16_V_6mm	0.01	-	Тохіс	Toxic	1.02E-02	Toxic	Toxic	1.02E-02
547	KGT90_CO2_16_V_22mm	0.2	-	Toxic	Toxic	4.48E-03	Toxic	Toxic	4.48E-03
548	KGT90_CO2_16_V_85mm	2.5	-	Toxic	Toxic	8.92E-04	Toxic	Toxic	8.92E-04
549	KGT90_CO2_16_V_212mm	15	-	Toxic	Toxic	1.99E-04	Toxic	Toxic	1.99E-04

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		Palassa			se Case/ Sensitivity C	ase 1	Sensitivity 2 (Future Operation)			
Line No.	Release Scenario	Release Rate (kg/s)	Explosion Probability	Immediate Ignition Event Frequency	Delayed Ignition Event Frequency	Unignited Event Frequency <sup>Note 1</sup>	Immediate Ignition Event Frequency	Delayed Ignition Event Frequency	Unignited Event Frequency <sup>Note 1</sup>	
550	KGT90_CO2_18_V_2mm	0.000	-	Тохіс	Toxic	1.63E-03	Toxic	Toxic	1.63E-03	
551	KGT90_CO2_18_V_6mm	0.003	-	Тохіс	Toxic	7.45E-04	Toxic	Toxic	7.45E-04	
552	KGT90_CO2_18_V_22mm	0.04	-	Тохіс	Toxic	3.80E-04	Toxic	Toxic	3.80E-04	
553	KGT90_CO2_18_V_50mm	0.2	-	Тохіс	Toxic	1.36E-04	Toxic	Toxic	1.36E-04	
554	KGT90_CO2_19_V_2mm	0.000	-	Тохіс	Toxic	6.14E-03	Toxic	Toxic	6.14E-03	
555	KGT90_CO2_19_V_6mm	0.003	-	Тохіс	Toxic	2.55E-03	Toxic	Toxic	2.55E-03	
556	KGT90_CO2_19_V_22mm	0.05	-	Тохіс	Toxic	1.23E-03	Toxic	Toxic	1.23E-03	
557	KGT90_CO2_19_V_63mm	0.4	-	Тохіс	Toxic	2.57E-04	Toxic	Toxic	2.57E-04	
558	KGT90_CO2_23_V_2mm	0.001	-	0.00E+00	0.00E+00	0.00E+00	Toxic	Toxic	8.01E-04	
559	KGT90_CO2_23_V_6mm	0.01	-	0.00E+00	0.00E+00	0.00E+00	Toxic	Toxic	3.82E-04	
560	KGT90_CO2_23_V_22mm	0.2	-	0.00E+00	0.00E+00	0.00E+00	Toxic	Toxic	2.04E-04	
561	KGT90_CO2_23_V_85mm	2.5	-	0.00E+00	0.00E+00	0.00E+00	Toxic	Toxic	4.31E-05	
562	KGT90_CO2_23_V_212mm	15	-	0.00E+00	0.00E+00	0.00E+00	Toxic	Toxic	1.78E-05	
563	KGT90_CO2_09_L_10mm	2.8	-	Toxic	Toxic	1.00E-05	Toxic	Toxic	1.00E-05	
564	KGT90_CO2_09_L_50mm	70	-	Toxic	Toxic	5.00E-07	Toxic	Toxic	5.00E-07	
565	KGT90_CO2_09_L_FBR	1000	_	Toxic	Toxic	5.00E-07	Toxic	Toxic	5.00E-07	
566	KGT90_CO2_10_L_10mm	2.8	_	Тохіс	Toxic	1.00E-05	Toxic	Toxic	1.00E-05	
567	KGT90_CO2_10_L_50mm	70	-	Toxic	Тохіс	5.00E-07	Toxic	Toxic	5.00E-07	
568		1000	-	Toxic		5.00E-07	Toxic	Toxic	5.00E-07	
	KGT90_CO2_10_L_FBR				Toxic					
569	KGT90_CO2_11_L_10mm	2.8	-	Toxic	Toxic	1.00E-05	Toxic	Toxic	1.00E-05	
570	KGT90_CO2_11_L_50mm	70	-	Toxic	Toxic	5.00E-07	Toxic	Toxic	5.00E-07	
571	KGT90_CO2_11_L_FBR	1000	-	Toxic	Toxic	5.00E-07	Toxic	Toxic	5.00E-07	
572	KGT90_CO2_12_L_10mm	2.8	-	Toxic	Toxic	1.00E-05	Toxic	Toxic	1.00E-05	
573	KGT90_CO2_12_L_50mm	70	-	Toxic	Toxic	5.00E-07	Toxic	Toxic	5.00E-07	
574	KGT90_CO2_12_L_FBR	1000	-	Toxic	Toxic	5.00E-07	Toxic	Toxic	5.00E-07	
575	KGT90_CO2_24_L_2mm	0.1	-	Toxic	Toxic	6.53E-03	Toxic	Toxic	6.53E-03	
576	KGT90_CO2_24_L_6mm	1.0	-	Тохіс	Toxic	2.19E-03	Toxic	Toxic	2.19E-03	
577	KGT90_CO2_24_L_22mm	14	-	Тохіс	Toxic	7.77E-04	Toxic	Toxic	7.77E-04	
578	KGT90_CO2_24_L_71mm	142	-	Тохіс	Toxic	1.89E-04	Toxic	Toxic	1.89E-04	
579	KGT90_CO2_25_L_2mm	0.1	-	Toxic	Toxic	2.85E-03	Toxic	Toxic	2.85E-03	
580	KGT90_CO2_25_L_6mm	1.0	-	Тохіс	Toxic	1.35E-03	Toxic	Toxic	1.35E-03	
581	KGT90_CO2_25_L_22mm	14	-	Тохіс	Toxic	7.40E-04	Toxic	Toxic	7.40E-04	
582	KGT90_CO2_25_L_50mm	70	-	Тохіс	Toxic	5.17E-04	Toxic	Toxic	5.17E-04	
583	KGT90_CO2_26_V_2mm	0.01	-	Тохіс	Toxic	8.01E-04	Toxic	Toxic	8.01E-04	
584	KGT90_CO2_26_V_6mm	0.1	-	Тохіс	Toxic	3.57E-04	Toxic	Toxic	3.57E-04	
585	KGT90_CO2_26_V_22mm	1.7	-	Toxic	Toxic	1.74E-04	Toxic	Toxic	1.74E-04	
586	KGT90_CO2_26_V_50mm	8.8	-	Toxic	Toxic	6.00E-05	Toxic	Toxic	6.00E-05	
587	KGT90_CO2_27_V_2mm	0.01	-	Тохіс	Toxic	8.77E-04	Toxic	Toxic	8.77E-04	
588	KGT90_CO2_27_V_6mm	0.1	-	Toxic	Toxic	3.78E-04	Toxic	Toxic	3.78E-04	
589	KGT90_CO2_27_V_16mm	0.9	-	Toxic	Toxic	2.25E-04	Toxic	Toxic	2.25E-04	
590	KGT90_CO2_28_L_5mm	0.7	-	Toxic	Toxic	6.00E-03	Toxic	Toxic	6.00E-03	
591	KGT90_CO2_28_L_50mm	70	-	Toxic	Toxic	6.00E-04	Toxic	Toxic	6.00E-04	
592	KGT90_CO2_29_V_2.5mm	0.02	-	Toxic	Toxic	2.40E-02	Toxic	Toxic	2.40E-02	
593	KGT90_CO2_29_V_25mm	2.2	-	Toxic	Toxic	2.40E-03	Toxic	Toxic	2.40E-03	
594	KGT90_CO2_30_L_8mm	1.8	-	Тохіс	Toxic	2.40E-02	Toxic	Toxic	2.40E-02	
595	KGT90_CO2_30_L_80mm	180	-	Toxic	Toxic	2.40E-03	Toxic	Toxic	2.40E-03	
596	KGT90_CO2_31_V_2.5mm	0.02	-	Тохіс	Toxic	4.60E-03	Toxic	Toxic	4.60E-03	
597	KGT90 CO2 31 V 25mm	2.2	-	Toxic	Toxic	4.60E-04	Toxic	Toxic	4.60E-04	
598	KGT90 CO2 32 L 5mm	0.7	-	Тохіс	Toxic	4.60E-03	Toxic	Toxic	4.60E-03	
599	KGT90 CO2 32 L 50mm	70	_	Тохіс	Тохіс	4.60E-04	Toxic	Toxic	4.60E-04	





				Ba	se Case/ Sensitivity C	ase 1	Ser	nsitivity 2 (Future Oper	Sensitivity 2 (Future Operation)			
Line No.	Release Scenario	Release Rate (kg/s)	Explosion Probability	Immediate Ignition Event Frequency	Delayed Ignition Event Frequency	Unignited Event Frequency <sup>Note 1</sup>	Immediate Ignition Event Frequency	Delayed Ignition Event Frequency	Unignited Event Frequency Note 1			
600	KGT36_NGL_12_L_100mm	97	0.3	2.87E-09	6.69E-09	8.16E-08	4.01E-09	9.35E-09	1.14E-07			
601	KGT36_NGL_12_L_Cat	1000	0.3	3.18E-09	7.43E-09	8.16E-08	4.45E-09	1.04E-08	1.14E-07			
602	KGT47_LPG_03_L_80mm	89	0.3	5.41E-09	1.26E-08	1.66E-07	1.11E-08	2.59E-08	3.41E-07			
603	KGT47_LPG_03_L_Cat	1000	0.3	6.46E-09	1.51E-08	1.66E-07	1.33E-08	3.10E-08	3.41E-07			
604	KGT47_LPG_06_L_50mm	35	0.12	1.32E-11	3.08E-11	8.90E-10	2.54E-11	5.92E-11	1.71E-09			
605	KGT47_LPG_06_L_Cat	1000	0.3	3.47E-11	8.10E-11	8.90E-10	6.68E-11	1.56E-10	1.71E-09			
606	KGT52_BMC_04_L_50mm	15	0.12	2.78E-13	6.48E-13	3.80E-11	2.78E-13	6.48E-13	3.80E-11			
607	KGT52_BMC_04_L_Cat	1000	0.3	2.97E-11	6.92E-11	7.60E-10	2.97E-11	6.92E-11	7.60E-10			
608	KGT55_MOH_04_L_40mm	1	0.12	9.68E-12	2.26E-11	1.20E-08	1.38E-11	3.23E-11	1.71E-08			
609	KGT55_MOH_04_L_Cat	1000	0.3	9.35E-09	2.18E-08	2.40E-07	1.34E-08	3.12E-08	3.42E-07			
610	KGT90_CO2_33_L_50mm	70	-	Toxic	Toxic	8.56E-09	Toxic	Toxic	8.56E-09			
611	KGT90_CO2_33_L_Cat	1000	-	Toxic	Toxic	8.56E-09	Toxic	Toxic	8.56E-09			
612	KGT90_CO2_34_L_80mm	180	-	Toxic	Toxic	3.42E-08	Toxic	Toxic	3.42E-08			
613	KGT90_CO2_34_L_Cat	1000	-	Toxic	Toxic	3.42E-08	Toxic	Toxic	3.42E-08			
614	KGT90_CO2_35_L_50mm	70	-	Toxic	Toxic	6.56E-09	Toxic	Toxic	6.56E-09			
615	KGT90_CO2_35_L_Cat	1000	-	Toxic	Toxic	6.56E-09	Toxic	Toxic	6.56E-09			

Notes:

1. Unignited frequency is the remaining portion of the leak frequency that is not ignited, i.e. Immediate ignition frequency + delayed ignition frequency + unignited frequency = total leak frequency

For scenarios which consist of toxic materials, the unignited frequency is the toxic event frequency.





**TODD ENERGY LTD** 

# Kapuni Wellsites QRA Assumptions Register

610114-RPT-R0001 July 2022

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A	Issued for Review/Comment	Y Lee	E Gloy	Y Lee	05/2020		
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# 1. ABBREVIATIONS

API	American Petroleum Institute
AWS	Automatic Weather Station
BLEVE	Boiling Liquid Expanding Vapour Explosion
BOP	Blowout Preventer
DNV GL	Det Norske Veritas Germanischer Lloyd
EI	Energy Institute
ESDV	Emergency Shutdown Valve
FBR	Full Bore Rupture
GOR	Gas Oil Ratio
HCRD	Hydrocarbon Release Database
HIPAP4	NSW Hazardous Industry Planning Advisory Paper No. 4
НМВ	Heat and Material Balance
НРКО	High Pressure Knock Out
IOGP	International Association of Oil and Gas Producers
IRPA	Individual Risk Per Annum
KPS	Kapuni Production Station
LFL	Lower Flammable Limit
LPG	Liquefied Petroleum Gas
LSIR	Location Specific Individual Risk
LTS	Low Temperature Separator
PFD	Process Flow Diagram
PFP	Passive Fire Protection
P&ID	Piping & Instrumentation Diagram
PLL	Potential Loss of Life
QRA	Quantitative Risk Assessment
RADD	Risk Assessment Data Directory
STDC	South Taranaki District Council
UK HSE	United Kingdom Health and Safety Executive
VCE	Vapour Cloud Explosion
WSO	Water Shut-off





# 2. INTRODUCTION

This document sets out the assumptions to be used for the Todd Energy (Todd) Kapuni wellsites Quantitative Risk Assessment (QRA).

# 2.1 Objective

The objective of the QRA is to develop risk contours to meet the risk assessment requirements of the South Taranaki District Council (STDC) District Plan, Section 11: Hazardous Substances.

# 2.2 Scope

The scopes include:

- 1) Conduct risk assessment for seven (7) Kapuni wellsites with 17 wells; and
- 2) Update the existing KA-4/14 and KA-13 wellsites QRA [Ref. 1] and hence supersedes the results from the QRA.

The final report will be a combined QRA report for all nine (9) Kapuni wellsites with 20 wells.

Currently, seven (7) wellsites are producing, KA-3 is out of service and KA-9 is designed for water disposal only. The wellsite details are summarised in Table 2-1. Only producing wells will be considered in the QRA.

Wellsite	Number of wells	Producing	Scheduled for Abandon- ment Note 1	Suspended Note 2	Shut in Note 3	Observation / water Note 4	Notes
KA-1, KA-7, KA-19 and KA-20	4	1			1 (KA-7)	2 (KA-1 and KA-20)	
KA-2	1	1					
КА-3	1			1			
KA-4 and KA-14	2	2					KA-14 is only operating once (for 24 hours) every 10 days [Ref. 20].
KA-5 and KA-10	2	1				1 (KA-10)	
KA-6, KA-11 and KA- 17	3	2		1 (KA-11)			
KA-8, KA-12, KA-15 and KA-18	4	2	1 (KA-12)		1 (KA-15)		
КА-9	2					2	A new well, KW03, is drilled in May 2021 for further water injection purposes.

Table 2-1: Kapuni Wellsites





Wellsite	Number of wells	Producing	Scheduled for Abandon- ment Note 1	Suspended Note 2	Shut in Note 3	Observation / water Note 4	Notes
KA-13	1	1					KA-13 is only operating in 1 out of every 3 months.
Total	20	10	1	2	2	5	

Notes:

- 1. Wells that are scheduled for abandonment are plugged with abandonment plans underway.
- 2. Suspended wells are plugged and major intervention is required to bring the well back to service.
- 3. Shut in wells are isolated but could be brought back into service. Note that KA-7 and KA-15 were considered as producing well in the Kapuni Safety Case [Ref. 2], however, the wells are currently shutin and hence will not be included in the risk assessment [Ref. 3 and Ref. 4].
- 4. Water wells are for water injection only and will not be used for hydrocarbon / producing. Observation wells are only for monitoring reservoir conditions and informing development of reserves estimates. They are designed for instrumentation only and cannot inject or produce.

There is no plan to bring the non-producing wells back online in the future. In the unlikely event that this changes, the QRA will be updated to verify any impact on the risk contours. Engagement with STDC will be completed as part of this process and a new resource consent will be required.

# 2.2.1 Exclusions

The following will be excluded from the QRA scope:

- Risk from the gathering pipelines to Kapuni Production Station (KPS). The scope for each wellsite will include up to the pipeline isolation valves (if available) or when the pipelines go underground. Pipelines passing through the wellsites (e.g., at KA-4/14 and KA-5) are not considered in the base case. The pipeline sections will be assessed in the sensitivity case. Note that the pipeline (P/L) to PECPR on the P&ID will be used in some sections to identify the pipeline boundary;
- Risk other than hydrocarbon / process risk (e.g., transportation risk, seismic risk and volcanic risks);
- Decommissioned and/or mothballed equipment;
- Utilities such as produced water and instrument air as they do not contain any hydrocarbon inventory;
- Individual risk calculations, including Individual Risk Per Annum (IRPA) and Potential Loss of Life (PLL) as the wellsites are normally unmanned;
- Societal risk (F-N curve) as the wellsites are located as remote area with low populations;
- Corrosion Inhibitors present at the wellsites as they are not flammable;
- Methanol injecting pumps as they are only used during start-up (except for KA-8/12/15/18 wellsite where methanol dosing is required throughout the year). Note that methanol tanks are always full and connected to the methanol pumps, with the pumps turn off when methanol is not being injected [Ref. 19], hence the methanol tanks and tubing to the methanol pumps will be included.
- Toxic effect of carbon dioxide.





# 2.3 Facility Description

Kapuni is an onshore gas and condensate field located in South Taranaki, approximately 50 km south of New Plymouth. 20 Kapuni wells are located on nine (9) separate wellsites in the area surrounding the Kapuni Production Station (KPS). The production wellsite process is a simple separation of gas and liquids involving the direction of wellstream gas and liquids to a low temperature separator (LTS) unit on the wellsite. The LTS separates the gas and liquids by means of pressure reduction to cause cooling.

An aerial overview of the wellsites location with reference to KPS is shown in Figure 2-1.

The wellsites access are via vehicle gates which are normally adjacent to the main wellsite control huts for the wellsites. Each wellsite hut is a single storey building which contains the wellsite control logic systems, emergency and communications equipment.

The wellsites have an open layout with areas separated from each other to prevent knock-on effects. The open area reduces the potential for overpressure from an explosion and reduces fire damage / escalation potential.





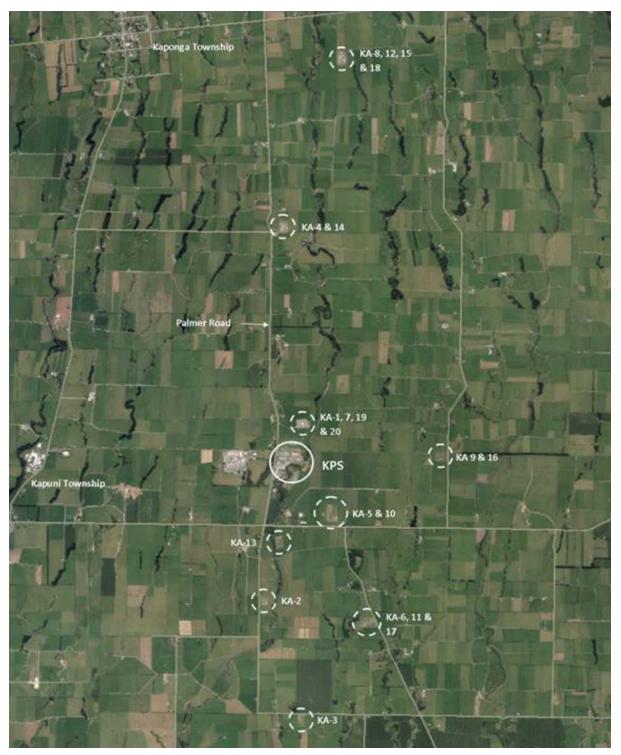


Figure 2-1: Kapuni Wellsites Location with reference to Kapuni Production Station

The details of each of the wellsite is as below.





# 2.3.1 Wellsite KA-1, KA-7, KA-19 and KA-20

Located just off Palmer Road, the site contains 4 wells. A wellstream heater is fitted to the KA-19 well. KA-1 well is suspended, KA-7 is not operational following the recent unsuccessful Water Shut-off (WSO) [Ref. 3] and KA-20 well is an observation well.

This site also acts as a distribution point for gas from the northern wells. It re-routes gas arriving from the gathering lines from wellsite KA-4/14 and KA-8/12/15/18 to KPS.

# 2.3.2 Wellsite KA-2

Located on Palmer Road, the site has an LTS unit and the flowline is equipped with two wellstream coolers.

# 2.3.3 Wellsite KA-3

This wellsite has been suspended and plugged.

# 2.3.4 Wellsite KA-4 and KA-14

Located just off Palmer Road, the site contains two wells, two LTS units, and a wellstream heater.

#### 2.3.5 Wellsite KA-5 and KA-10

Located just off Skeet Road, this site contains one producing well (KA-5) and one observation well (KA-10), with a Desander unit for solids separation, and a PCV used on start-up.

### 2.3.6 Wellsite KA-6, KA-11 and KA-17

Located on Ahipaipa Road, this site contains two in service wells, and one suspended well (KA-11). KA-6 and KA-17 wellstream fluids are co-mingled, routed through a wellstream cooler and then to an LTS Unit.

# 2.3.7 Wellsite KA-8, KA-12, KA-15 and KA-18

Located just off Eltham Road, this site contains two (2) producing wells. KA-12 well is plugged and scheduled for abandonment and KA-15 well is shut-in and isolated [Ref. 4]. Two wellstream process skids and two wellhead compression units are fitted to the wells.

# 2.3.8 Wellsite KA-13

Located just off Skeet Road, this site contains one well, Desander, a flowline choke valve and a High Pressure Knock Out (HPKO) vessel. It connects into the KA-6/5 gathering lines.

# 2.3.9 Wellsite KA-9

Located on Lower Duthie Road, two wells were drilled on the site, KA-9 (referred to as KW-2) and KA-16. KA-16 is suspended and KW-2 is currently in service as a water injection well. There is very little equipment left on the wellsite, only the water injection line, a filter, and two pig receivers.

The wellsites flow schematic is presented in Figure 2-2.





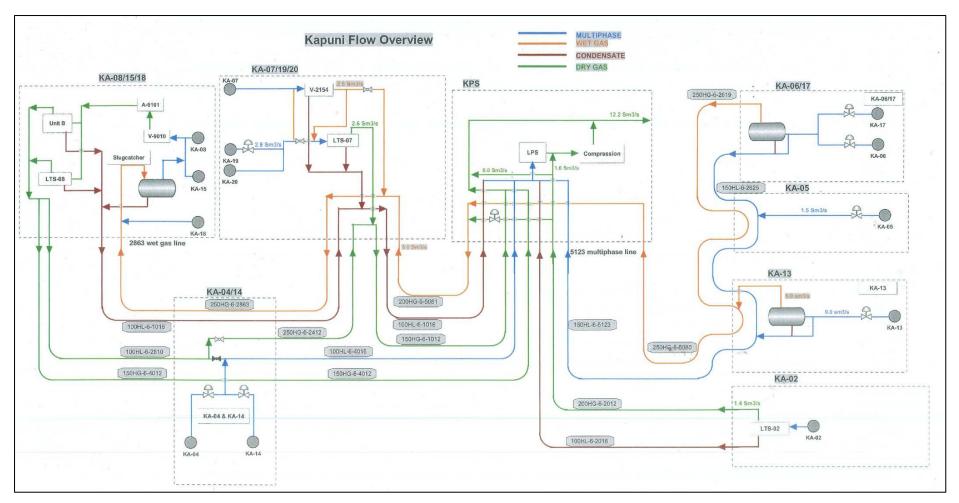


Figure 2-2: Kapuni Wellsites Flow Schematic





# 3. MODELLING INPUTS AND ASSUMPTIONS

This section outlines all modelling inputs and assumptions that will be used in the QRA. The assumptions and methodology will be consistent with those in the Todd Energy's Fire and Gas Analysis and Quantitative Risk Assessment Methodology Guideline [Ref. 5].

# 3.1 Assessment Tool

The risk assessment model will be set up using DNV GL Safeti version 8.22 [Ref. 6].

# 3.2 Definition of Parts Count Sections

# 3.2.1 Isolatable Inventory

Sectionalisation will be performed to segregate the facilities into a number of isolatable sections. Each potential leak source will be associated with a particular isolatable inventory. Primarily, the isolatable inventories will be defined by emergency shutdown valve (ESDV) boundaries. These sections will be split further where required, and the entire contained inventory was considered as available for release. Further segregations are based on:

- Significant change in operating parameters (temperature and pressure);
- Significant change in stream composition;
- Change in stream phase; and
- Equipment location.

The probability of successful detection and isolation is assumed to be 100%. At isolatable boundaries, the valve will be assumed as the last component of the upstream inventory. If a cap or blind flange is shown against a valve, it will be assumed to be closed, even if not indicated as such.

Node sections will be highlighted in the Process Flow Diagrams (PFDs) and will be detailed in a Node Definition table in the QRA report which presents details of all the nodes including unique identification code, definition of boundaries, operating temperature and pressure, maximum pipe diameter, etc.

Following sectionalisation, a parts counts will be conducted to perform the frequency analysis for the QRA.

# 3.2.2 Components

The definition of components within the parts count will be aligned with failure rate data published in the International Association of Oil and Gas Producers (IOGP) Risk Assessment Data Directory (RADD) Process Release Frequency [Ref. 7]. The parts count will consider the following:

- Equipment items;
- Valves;
- Flanges;
- Instrumentation and small-bore fittings; and
- Pipework.

The parts count will be recorded in an MS Excel spreadsheet, with each section broken down based on the piping and instrumentation diagrams (P&IDs). Marked up P&IDs will be attached with the QRA report.





# 3.3 Failure Frequency Data and Hole Size Distributions

# 3.3.1 General Leak Frequency

The leak frequencies for process equipment and piping will be taken from the IOGP Process Release Frequency [Ref. 7]. The release frequencies of the main process equipment items from IOGP are based on the UK HSE (UK Health and Safety Executive) hydrocarbon release database (HCRD) which has been compiled by the UK HSE over a 20-year period. Two sets of data are presented in IOGP Process Release Frequency, which include the 1992 – 2015 data and 2006 – 2015 data.

The recommended values based on experience in the period 2006 – 2015 (inclusive) will be used. The IOGP release notes state that the number of incidents recorded per year in the database has been steadily decreasing, and it is considered appropriate to base the frequency on more recent data on the assumption that this is more representative of what will occur in the future.

Failure frequency data from the HCRD contains detailed historical information on offshore hydrocarbon release incidents occurring in the UK offshore environment and is considered an industry standard for offshore QRA applications. The database categorises failure rates on a detailed basis of equipment type and size and provides a probabilistic hole size distribution associated with the failure.

The HCRD data are also normally used for QRA at onshore facilities, although the use of offshore failure rate may be considered to be conservative for use in most onshore applications, on the basis that:

- Offshore environments tend to be harsher, both external (saliferous environment) and internal (produced sand), increasing the rate of equipment corrosion and erosion;
- Congestion at offshore facilities increases the likelihood of damage through impact; and
- Restricted access to offshore facilities may limit maintenance campaigns, increasing the likelihood of failure.

#### Atmospheric Storage Tank

The IOGP Release Frequency Data does not provide the frequencies for atmospheric storage tanks. Therefore, the following leak frequencies as shown in Table 3-1 from the TNO Purple Book [Ref. 23] will be used for methanol tanks.

Type of Release	Storage Tanks, Atmospheric
Instantaneous release of the complete inventory	5.0E-06 per year
Continuous release of the complete inventory in 10 minutes at a constant rate	5.0E-06 per year
Continuous release from a hole with an effective diameter of 10 mm	1.0E-04 per year

#### Table 3-1: Release Frequencies for Atmospheric Storage Tank





# 3.3.2 Pigging

Pig traps are located at the wellsites to clean, condition and/or monitor the pipelines. The pigging frequency will be used to calculate a modification factor for the leak frequency from the pig receivers.

Tag	Description	т	o	Pigging Frequency (per year)	Average pigging duration (hours)	Modification Factor		
		KA-06/	/17					
A-2613	Hydrocarbon gas to gathering line	A-5001	KPS	4	1.5	0.001		
A-2614	Hydrocarbon liquid to gathering line	A-5003	KPS	4	1.5	0.001		
		КА-0	2					
A-0101B	Hydrocarbon liquid to A-0501A (KPS)	A-0501A	KPS	2	8	0.002		
A-0103	Hydrocarbon gas to A-0503 (KPS)	A-0503	KPS	4	1.5	0.001		
	КА-08/18							
A-2863	Wet gas from KA-4/14	A-2165	KA-19	4	1.5	0.001		
A-2813	Dry gas to KA-4	A-0502D	KPS	2	1	0.0002		
A-2814	Dry gas to KA-4	A-2440	KA-4/14	4	1.5	0.001		
A-2864	Condensate to KA-1&7	A-0501B	KPS	4	7	0.003		
		KA-4/	14					
A-2440	Dry gas to KA-7	A-2167	KA-19	1	1	0.0001		
		KA-1	9					
A-2165	Wet gas to KA-8/18 via KA-4/14	A-2863	KA-8/18	4	1	0.0005		
A-2167	Dry gas from KA-4/14 wellsites	A-2440	KA-4/14	1	1	0.0001		
A-2163	Wet gas from A-5002	A-5002	KPS	4	0.5	0.0002		
A-2166	Dry gas to KPS A-502A	A-0502A	KPS	1	0.5	0.0001		
A-2164	Vector Treated Gas from KPS A-5004	A-5004	KPS	1	0.5	0.0001		
A-2169	(Hydrocarbon gas) To Kiwi Dairy Co. & Taranaki Byproducts Co.	N/A	Other	1	6	0.001		

Table 3-2: Pigging	Frequencies	and Modification	Factor [Ref 19]
TUDIE 5-2. Flygilly	riequencies		Fuctor [Rej. 19]

Note: No pig traps at KA-05 and KA-13.

# 3.3.3 Release Hole Sizes

For every component failure, there is a range of credible hole sizes ranging from pinhole leak to full bore rupture (FBR). The representative hole sizes to be used for process sites are as shown in Table 3-3.

The geometric mean for hole diameter will be used to represent a range in hole sizes as this approach has a mathematical basis that aligns with numbers that are exponential in nature, such as is the case for hole sizes where the consequence is dependent on the area of the hole size or square of the diameter. For example, the representative hole size for the range 10 - 50 mm is calculated as  $(10 \times 50)^{0.5} = 22$  mm. The use of geometric mean is also aligned with the recommendation in the latest IOGP Process Release Frequency [Ref. 7].





#### Table 3-3: Hole Size Distribution

IOGP Hole Size Group (mm)	Representative Hole Size (mm)
1 - 3	2
3 - 10	6
10 - 50	22
50 - 150	85
> 150	Range geometric mean

22 mm will be used as the maximum hole size for small bore fittings as per the Todd Energy's Methodology Guideline [Ref. 5].

The same approach will be taken to select the representative hole size for rupture cases (release > 150 mm). The selected hole size will be the geometric mean of 150 and the largest line size in the section. This is consistent with the approach used for other release size categories and may be appropriate given the limited FBR base data that is used by the algorithm to calculate frequency.

It is noted for methanol tanks that will reference to TNO Purple Book [Ref. 23] failure data, actual hole sizes following the failure data will be used as there are no sufficient leak size distribution data in Purple Book to calculate the geometric mean.

#### 3.3.4 Leak Frequency Modification Factor

Several leak frequency modification factors will be applied to the release frequency database as per the Todd Energy's Methodology Guideline [Ref. 5]. These are listed below:

- Piping Release Frequency
  - Pipework will be split into categories: process (on skid) piping and interskid piping as described in the definition for equipment type 1: steel process pipes of IOGP Process Release Frequencies [Ref. 7].
  - For interskid piping, the modification factor for "inter-unit piping" (section 3.3.3 of IOGP Process Release Frequencies) which is 0.9 will be applied, i.e. there will be a 90% reduction in frequencies.
- Rupture Release Frequency
  - A review of the UK HSE Hydrocarbon Release Database (HCRD) from 1992 to 2015 has been performed and it was determined that there were 31 incidents in the full-bore release category within 24 years. These were reviewed by Todd to determine the applicability of these cases in comparison with Todd Energy facilities. For wellsites, 22 of the incidents can be discounted on the basis that the release scenarios cannot occur on an onshore wellsite. The frequency for rupture release will be reduced by 65%.

The maximum flange release hole size will also be limited to 22 mm as a release from a flange is normally limited to a segment of a gasket between bolts [Ref. 5].





# 3.4 Blowout Events

For normal operations, it is assumed that a blowout may occur during either production, well workover or well wireline activities. The categories applied for classifying the incidents [Ref. 11 and 12] are shown in Table 3-4.

Main	Category	Description
Blowout and well release	Blowout (surface flow)	• Uncontrolled incidents with surface flow, including subsea releases, e.g., from topside or subsea wellhead, drill floor or Christmas tree.
		<ul> <li>Considered as a full blowout event from the full well bore size. This will be modelled based on the expected maximum well fluid flowrate that the reservoir can supply to the wellbore instead of the wellhead pressure to avoid over-estimating the release rate and creating unrealistic results.</li> </ul>
	Blowout (underground flow)	• Underground flow only or with limited surface flow where minor flow occurred and typically the Blowout Preventer (BOP) has been activated.
		• Considered to have no consequences on the surface and will therefore not considered in this study.
	Diverted well release	• An incident where the diverter system functioned as intended.
		• Assumed to be a well release that can be shut-in or diverted to flare in a short period of time. This event will not be included as the event frequency as given in Table 3-4 is equal to zero.
	Well release	• An incident where hydrocarbons (oil or gas) flow from the well at some point where flow was not intended, and the flow was stopped by use of the barrier system that was available on the well at the time the incident started.
		• Assumed to be release from the wellhead and Christmas trees. It will be modelled as a horizontal well fluid release at well pressures. Release sizes will be based on the same hole size distribution used for other release cases.

Table 3-4:	Categories	of Blowo	ut Incidents
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The blowout likelihood from the IOGP Blowout Frequencies [Ref. 11] will be used, specifically data for offshore operations in areas not operating according to North Sea Standard (Table 2-3 in the IOGP). It is noted that the Kapuni wellsites are located onshore, however, IOGP recommends the use of offshore data presented in Section 2 in the IOGP but noted that there will be a greater degree of uncertainty. The frequency for well wirelining considered in the KA-4/14 and KA-13 QRA [Ref. 1] is once per well per year, and no workover will be performed in the wells' life time. These assumptions will be used in this QRA as well.

Operation	Category	Frequency
Production (Excluding	Blowout (surface flow)	3.3E-05 per well year
external causes Note 1)	Diverted well release	0 per well year
	Well release	2.9E-05 per well year
Wireline	Blowout (surface flow)	9.0E-06 per well year
	Diverted well release	0 per well year
	Well release	2.6E-05 per well year

Note 1: External causes are external loads such as storms or fire leading to blowout or well release.





# 3.5 Ignition Probabilities

The probability of ignition of a release is a function of the release rate, the nature of the material being released and the conditions of the surrounding plant. For this QRA, The Energy Institute (EI) ignition probability model referenced in IOGP Ignition Probabilities [Ref. 8] will be used for the estimation of overall ignition probability of loss of containment scenarios.

For wellsite, ignition probabilities should be taken from Scenarios 5 and 6 and they are assumed to particularly apply to a 'plant' where processing takes place. This is considered conservative for use at wellsites as not much processing takes place.

The scenarios are described as:

- Scenario 5 Small Plant Gas LPG (Gas or LPG release from small onshore plant) Releases of flammable gases, vapour or liquids significantly above their normal boiling point from small onshore plants (plant area up to 1200 m<sup>2</sup>, site area up to 35,000 m<sup>2</sup>).
- Scenario 6 Small Plant Liquid (Liquid release from small onshore plant) Releases of flammable liquids that do not have any significant flash fraction (10% or less) if released from small onshore plants (plant area up to 1200 m<sup>2</sup>, site area up to 35,000 m<sup>2</sup>) and which are not bunded or otherwise contained.

The graphs of ignition probabilities as a function of mass release rate are shown in Figure 3-1.

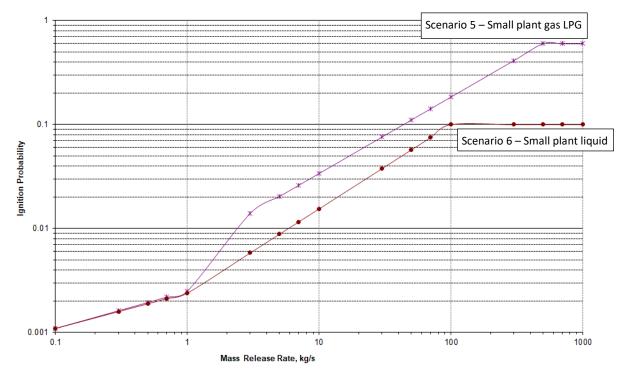


Figure 3-1: Ignition Probability

#### **Early and Delayed Ignition Probabilities**

The graph represents the total ignition probability. An overall distribution for early to delayed ignition ratio of 30:70 to 50:50 split is considered reasonable. The timing of ignition is used as a means to predict the nature of the ignited event. Early ignition is taken to indicate a jet fire or pool fire depending on the material released. Delayed ignition is taken to indicate that the ignition would initially result in a flash fire or explosion.





For this study, a 30:70 split for early to delayed ignition probability will be used. Given the maturity of the hazardous area for all wellsites, it can be assumed that probability of early ignition would be low.

# 3.6 Material Composition

The Heat and Material Balances (HMBs) will be provided by Todd Energy's process engineer [Ref. 9]. The wellstream fluid from each well have different flowrates, material compositions and operating conditions. Any stream that has unique consequences will be represented by dedicated sections. For sections with similar operating conditions or fluid composition that have similar consequence results, the worst-case scenario will be selected as representative, to rationalise the number of scenarios performed. This is to avoid the averaging out of inputs of different wellstreams, as it may create a stream with 'brand new' operating conditions, material compositions and flowrates which does not represent the actual release conditions.

As far as is reasonable, the compositions in each stream are simplified, i.e. isomers are summed together and the C6+ hypothetical materials (KP01, up to KP30) are represented by different heavy alkanes. The following alkanes are selected to represent different ranges of hypothetical materials found in the streams based on their properties:

- KP01 to KP10 are assumed to be C7;
- KP11 to KP20 are assumed to be C10; and
- KP21 to KP30 are assumed to be C20.

Note that the hypothetical materials in the Todd Energy's Methodology Guideline are represented in ST01 to ST30; whereas the hypothetical materials in the HMB provided by the process engineer are represented in KP01 to KP30. The hypotheticals STXX are the same as KPXX [Ref. 19].

The important characteristic of molecular weight is kept close to the actual value to ensure the release rate is representative.

The effects of water cut of the hydrocarbon on fire hazards will be considered to identify the streams that are considered not flammable due to high water content. According to Oil and Gas UK Fire and Explosion Guidance [Ref. 10], for water cuts under 50%, no significant reduction in heat fluxes to engulfed objects can be expected (<10%). However, for water cuts over 50%, the flames are significantly less radiative, and the overall heat flux to an obstacle can be reduced by 40% or more. To be in line with Oil and Gas UK Fire and Explosion Guidance, it is assumed that a mixture remains flammable if it has a water cut of up to 125% (defined as mass of water/ mass of fuel x 100%), although not necessarily capable of supporting a stable flame in the absence of some other supporting mechanisms.

Similarly, increasing concentrations of  $CO_2$  were found to reduce the likelihood of ignition of a methane jet release. At  $CO_2$  concentrations of 22–40% (v/v) it was possible for a self-sustaining flame to exist, but beyond these concentrations a pilot flame was required to aid combustion. Beyond 60%  $CO_2$  the pilot flame had no effect and the mixture was completely inert [Ref. 22].

The average flammability of the mixtures will be calculated by Safeti software, considering the effects of the inert components (e.g.,  $CO_2$ ,  $N_2$  and  $H_2O$ ).

# **3.7** Release Scenarios

Release rates will be calculated based on the release hole size and operating pressure. All releases will be modelled at initial process conditions until the entire isolatable inventory has been depleted and will not take account of the depressurisation that occurs over time.

All wellsites have automated ESD on fire detection, and KA-8/18 has automatic ESD on gas detection as well. Hydrocarbon leaks at the wellsites or along the pipelines (other than minor leaks) will lead to pressure and/or liquid level drop at KPS, which will alert the operators to perform a check at the wellsite(s).





Given the proximity to the KPS, operators can generally arrive at the wellsites within 15 minutes. As such, 15 minutes delayed detection will be assumed, and 15 minutes of released inventory will be added. Full bore rupture cases are only considered credible when there is major work on site, and the wellsite would be manned to detect the leak immediately. Hence undetected full bore rupture is not considered credible.

The inventory for well blowout and well release events will be considered as unlimited because they can be supplied from the downhole reservoirs.

The wellsites bunding and drainage systems are designed to contain hazardous materials within the boundaries of the wellsite. Therefore, condensate pools are assumed to remain confined within the site.

Other assumptions to be applied in the QRA include:

- The height of release from all scenarios will be assumed to be at 1 m above ground, although some equipment may be located at the elevation higher than the ground level.
- For wellsite releases, 70% of the releases should be modelled as horizontal releases and 30% of the releases as vertical releases. Well blowout will be modelled as 100% vertical release.
- All outdoor releases are modelled as non-impinged (free) releases and are monitored at the downwind direction.
- A free-field condition is assumed although in real facility situations, multiple obstructions beyond the leak source could shield or deflect the jet fire. Obstructions in the path of the vapour cloud could also alter the concentration of gas in the cloud
- Fire durations are estimated based on the assumption that isolation and shutdown are immediate.
- In estimating piping length, a safety factor of 1.25 will be applied to all lengths measured from the map to account for bends and elevations which could not be determined from the 2D map.
- For liquid releases from pressurised sources, if the rainout is significant then a pool fire will result. If not, a spray fire (equivalent to a jet fire) will result. It is suggested in the Oil and Gas UK Fire and Explosion Guidance [Ref. 10] that for ignited two-phase releases:
  - If the Gas Oil Ratio (GOR) is low, at drive pressures above 10 bar(abs) a spray fire will result;
  - If the GOR is high, at drive pressures above 5 bar(abs) a spray fire will result.

Note: Gas oil ratio is the ratio of gas to oil within the hydrocarbon fluid. A high GOR indicates a high gas content which has implications for the potential for gas fires from a depressurisation and release [Ref. 10].

# 3.8 Congested Area

A flammable vapour cloud accumulation at congested area(s) is the prerequisite to a vapour cloud explosion (VCE). There is limited equipment at the wellsites, and these areas are generally open with good ventilation expected throughout the year. The possibility of flammable vapour accumulating and developing into subsequent vapour cloud explosions, are considered not credible. Hence, VCE modelling will not be carried out.

# 3.9 Atmospheric Conditions for Modelling

Meteorological conditions impact the outcomes of release modelling, including downwind flammable and toxic vapour cloud dispersion distance (influenced by atmospheric stability and wind speed), rate of pool vaporisation (ambient temperature), and atmospheric attenuation of radiant heat (temperature and relative humidity).





# 3.9.1 Wind Speed and Direction

Wind speed and direction data are taken from NIWA's CliFlo database [Ref. 16] for the Hawera Automatic Weather Station (AWS) to represent the atmospheric conditions at Kapuni. Data for 5-year period from January 2008 to December 2012 are taken, with wind speed and direction measurements taken every hour. The wind rose is shown in Figure 3-2.

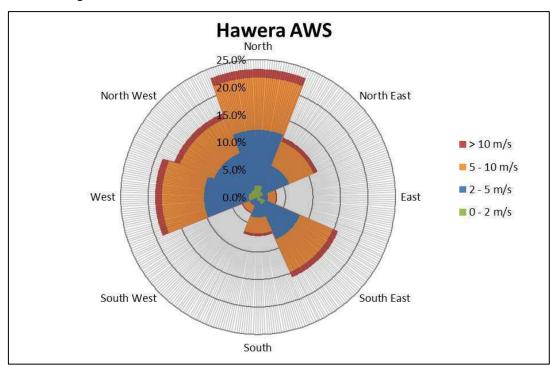


Figure 3-2: Hawera AWS Windrose

The following combinations of wind speed and atmospheric stability will be considered in the QRA that represents the typical wind speed conditions around the wellsites:

- 2/F wind speed of 2 m/s with Pasquill Stability class F stable, night with moderate clouds and light/moderate wind
- 5/D wind speed of 5 m/s with Pasquill Stability class D neutral, little sun and high wind or overcast/windy night
- 10/D wind speed of 10 m/s with Pasquill Stability class D

For the modelling, wind speed reference height (the height at which the wind impacts a release) will be set at 1 m (i.e., so as to match the release height). The Power Law wind profile will be applied where the wind speed varies with height according to power-law profile.

By consideration of the Pasquill Stability class relationship with day and night and wind speeds, the wind data for use in the QRA model is calculated as shown in Table 3-6.

Wind Speed / Pasquill Stability	North	North East	East	South East	South	South West	West	North West	Total
0 - 2 m/s / F	2.1%	1.1%	0.3%	1.4%	0.6%	0.3%	1.7%	1.5%	9.0%





Wind Speed / Pasquill Stability	North	North East	East	South East	South	South West	West	North West	Total
2 - 5 m/s / D	10.1%	5.1%	1.5%	6.9%	3.1%	1.4%	8.2%	7.2%	43.5%
> 5 m/s / D	11.1%	5.6%	1.7%	7.5%	3.4%	1.5%	8.9%	7.9%	47.5%
Total	23.3%	11.8%	3.5%	15.9%	7.1%	3.2%	18.7%	16.5%	100.0%

# 3.9.2 Ambient Temperature and Relative Humidity

The following ambient temperature and relative humidity as consistent with those used in the KPS QRA [Ref. 18] will be used in the QRA:

- Ambient temperature: 14°C
- Relative humidity: 83%

#### 3.9.3 Solar Radiation

The allowance for solar radiation will not be included in the thermal radiation effects consideration.

# 3.9.4 Surface Roughness

Safeti cannot take into account the effects of the local undulating topography for the gas dispersion. The surface roughness of 30 mm will be applied, which generally represents an area of "open flat terrain; grass, few isolated objects" to represent the open area of the wellsites.

# 3.10 Fatality Criteria

The physical effects from these consequences can have different impacts on humans. The variation of harm from different effects is reflected in a parameter known as the harm probability. In this study, human harm relates to high potential for fatality.

# 3.10.1 Heat Radiation

The method of calculating the probability of fatality for an individual, given known exposure duration and thermal heat radiation levels, is undertaken by using a Probit function. The Probit function is a general formula which takes the same form, but with various constants used. The Probit used for lethality calculations is taken from the TNO Green Book [Ref. 17]. The Probit function is defined as follows:

Probit =  $-36.38 + 2.56 \ln (t \times q^{4/3})$ 

Where:

t = exposure duration in seconds

q = thermal radiation level in W/m<sup>2</sup>

Safeti calculates the Probit values during the analysis.

An exposure duration of 20 seconds has been used as a base case, although it is noted that personnel are likely to find some form of shielding protection within this time frame.

# 3.10.2 Flash Fire

If personnel are within the 100% lower flammable limit (LFL) of the gas plume, 100% fatality is assumed. LFL is the lower end of the concentration range over which the flammable mixture of vapour in air can be ignited.





A flash fire occurs when a dispersed cloud of flammable vapour and air mixture is ignited within its flammable regions, causing a wall of flame to spread throughout the flammable region and back to the release point. The flame propagates through the cloud in a manner such that negligible or no damaging overpressure is generated. This flash is almost instantaneous as the flame propagates at high speed through the cloud and back to the source.

An assumption of 100% fatality rate within the footprint of the cloud is conservative and does not allow for potential risk reducing considerations such as:

- uneven mixing of flammable vapour and air in the cloud resulting in uneven propagation of the flame,
- topography,
- sparsely populated rural land use adjoining the site,
- availability of shelter,
- opportunity for escape, and
- clothing worn by persons exposed to the flash fire.

Thermal radiation outside of the flash fire footprint, reduces rapidly and is not sustained due to the instantaneous nature of the event. The potential for fatality outside the flash fire footprint is not considered credible.

# 3.10.3 BLEVE

Boiling Liquid Expanding Vapour Explosion (BLEVE) is an escalation scenario that occurs as a result of prolonged flame impingement on above ground pressurised vessels containing materials such as liquefied petroleum gas (LPG) or light end hydrocarbon. BLEVE would result in an explosion overpressure together with a fireball and missile generation over some distance. As the fireball tends to drift upward and to avoid double counting, only fatalities from the explosion overpressure effects are considered in this risk assessment. The probability of BLEVE depends on various factors, including the types of flammable material and liquid inventory in the vessel, material of construction of the vessel, types and number of fire protection systems (e.g. relief valves, cooling systems), mechanism of vessel failure (external impact, jet fire impingement or pool fire impingement), etc. Passive Fire Protection (PFP) can be provided on pressurised vessels to minimise the probability of BLEVE. There is no clear guideline or criteria to determine the likelihood of a BLEVE on a pressurised vessel. For this risk assessment, BLEVE will be considered credible if a pressurised vessel containing at least 4 m<sup>3</sup> of volatile hydrocarbon (liquid butane or lighter) is exposed to direct flame impingement for 5 minutes or longer.

Liquid volume calculation for the vessels at the wellsites are shown in Table 3-7.

Тад	Description	Diameter (m)	Length / Height (m)	Volume (m³)	Liquid Level (mm)	Liquid Volume (m³)		
	КА-02							
V-201A	HP Knockout	0.686	4.572	1.69	343	0.84		
V-204A	Secondary Knockout	0.914	3.048	2.00	457	1.00		
V-0202A	LT Separator	1.219	3.810	4.45	1905	2.22		
КА-05								
V-0516	KA-5 Desander	0.406	4.572	0.59	406	0.59		

Table 3-7: Kapuni Wellsites Vessels Liquid Volume Estimation





Тад	Description	Diameter (m)	Length / Height (m)	Volume (m³)	Liquid Level (mm)	Liquid Volume (m³)	
		KA-1	9				
V-2154	Wellhead Knockout	1.068	4.572	4.10	534	2.05	
	KA-8/18						
V-2803	HP Knockout Drum	0.685	4.570	1.68	342.5	0.84	
V-9010	Wellstream Separator (2 phase)	1.600	4.500	9.05	800	4.52	
V-9020	Wellstream Separator (2 phase)	1.600	4.500	9.05	800	4.52	
V-2808	LT Separator	1.830	5.640	14.83	915	7.42	
V-2804	Low Temperature Separator	1.220	3.810	4.45	1905	2.23	
V-2805	Secondary Knockout	915	3.050	2.01	457.5	1.00	

Based on the table, the liquid volume for the KA-8/18 Wellstream Separators (V-9010 & V-9020) and LT Separator (V-2808) might be greater than 4 m<sup>3</sup>. However, based on the Heat and Material Balance, the composition of the liquid sections from the Wellstream Separators is mainly water (approx. 88 vol%), and the liquid from the LT Separator is mostly heavy hydrocarbons with volatile hydrocarbons making up only 15 vol% of the total composition. Therefore, it is considered that all vessels in Kapuni Wellsite do not have BLEVE potential.

# 3.10.4 Toxic Effects

Fatality probability when exposed to toxic gas as a function of exposure concentration and duration can be calculated by using a probit function of the form given below:

Probit =  $a + b \ln (C^n \times t)$ 

where:

t = exposure duration in minutes

C = concentration in ppm

a, b and n = material specific probit constants

Toxic effect from methanol will be considered in the QRA. UK HSE gives the following toxic load values for methanol:

- SLOT =  $8.02 \times 10^5$  ppm<sup>n</sup> · min (1% fatality probability)
- SLOD =  $2.67 \times 10^6$  ppm<sup>n</sup> · min (50% fatality probability)

By solving the simultaneous equation, the other constants a and b can be calculated. The probit constants for methanol are:

a = -23.67 b = 1.94 n = 1





# 3.11 Risk Criteria

Risk is the combination of the likelihood and consequence of such accidents. It is defined as the probability of a specific adverse event occurring in a specific period or in specified circumstances. The likelihood may be expressed either as a frequency (i.e. the rate of events per unit time) or a probability (i.e. the chance of the event occurring in specified circumstances). The consequence is the degree of harm caused by the event.

Escape and evacuation fatalities are generally not considered for an onshore plant due to the open site layout and personnel's ready accessibility to the muster area. Hence, only immediate fatalities will be taken into account when performing the risk analysis to onsite workers.

Key deliverable for this study is the location specific individual risk (LSIR) in the form of risk contour. LSIR is the risk of fatality at a point in space to a hypothetical individual at a location for 365 days per year, 24 hours a day, unprotected and unable to escape. In real situation, people do not constantly remain in one location, so this risk value does not provide a realistic representation of the true level of risk.

However, this value allows different areas to be compared on the same basis and is a useful measure for establishing the most hazardous areas of the plant, or for the comparison of facility risk profiles against standard criteria. The LSIR can be expressed as follows:

$$LSIR = \Sigma F \times P$$

Where:

F = Frequency of an event outcome per year

P = Probability of death due to the event at the location

 $\Sigma$  = Sum over all modelled events

LSIR is usually presented as risk contours or by defining risks at selected locations (e.g. site boundary).

As there are no standard risk criteria which have been developed for the NZ context, this deliverable will be assessed against the suggested risk criteria in the NSW Hazardous Industry Planning Advisory Paper No. 4 (HIPAP4) "Risk Criteria for Land Use Planning" as shown in Table 3-8.

Land Use	Risk Criteria Adopted (per annum)	Interpretation for QRA				
Hospitals, schools, childcare facilities, old age housing	0.5 × 10 <sup>-6</sup> (or 5 × 10 <sup>-7</sup> ) (1 in 2 million)	$5 \times 10^{-7}$ risk contour should not extend to these areas				
Residential, hotels, motels, tourist resorts	1 × 10 <sup>-6</sup> (1 in 1 million)	1 × 10 <sup>-6</sup> risk contour should not extend to these areas				
Commercial developments including retail centres, offices and entertainment centres	5 × 10 <sup>-6</sup> (1 in 200,000)	5 × 10 <sup>-6</sup> risk contour should not extend to these areas				
Sporting complexes and active open space	10 × 10 <sup>-6</sup> (or 1 × 10 <sup>-5</sup> ) (1 in 100,000)	1 × 10 <sup>-5</sup> risk contour should not extend to these areas				
Industrial	50 × 10 <sup>-6</sup> (or 5 × 10 <sup>-5</sup> ) (1 in 20,000)	$5 \times 10^{-5}$ risk contour should, as a target, be contained within the				

Table 3-8: HIPAP	4 Individual	Fatality	Risk criteria
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boundaries of the industrial site

where applicable





NSW HIPAP 4 states that where these criteria are initially exceeded, commercial and industrial land development may be appropriate where mitigating measures can be implemented to reduce risk exposure to less than the target individual fatality risk level.





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